

Supporting Information for:
Microalgal biomass production pathways: Evaluation of life cycle environmental impacts

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1. MODEL OVERVIEW:

1.1. Research Objectives

The goal of this study is to create an LCA open pond cultivation model to evaluate the direct Water Demands (WD), Fossil Energy Return on Investment ($EROI_{\text{fossil}}$), and net life cycle Green House Gas (GHG) emissions for the cultivation of microalgae in open raceway ponds. This study examines multiple cultivation locations as well as cultivation and harvesting options to see if variation in these parameters affects the overall viability of biomass production.

1.2. Reactor Configuration:

Previous studies have shown that the cultivation and harvesting of microalgae is energy intensive and is a major bottleneck in algae-to-biofuel production[1-3]. Reactor configuration is an important parameter that can influence the overall viability of biomass production. While a consensus on the optimal industrial reactor configuration has yet to be established, studies have shown that open raceway pond (ORP) configurations have lower environmental and operating costs than photobioreactors (PBRs)[4, 5]. Past research has also indicated that closed PBR systems have high capital costs, and may not scale efficiently to a commercial level [5, 6]. For these reason's only ORPs were examined in this study.

1.3. Methodology

Life Cycle Analysis (LCA) is utilized as a tool to quantify the environmental and energetic impacts of microalgae biomass production. Energetic Return on investment ($EROI_{\text{fossil}}$), which is traditionally used to evaluate fuel types, is implemented as a metric to evaluate the various biomass production pathways.

1.3.1. Fossil Energy Return on Investment ($EROI_{\text{fossil}}$)

As the primary motivation for microalgae production (and subsequent downstream processing) is its potential to displace fossil derived fuels, a fossil energy centered metric was chosen to assess the sustainability of microalgae production. In this analysis, the fossil energy return on investment ($EROI_{\text{fossil}}$) is defined as the ratio of the amount of energy stored in algal biomass (biomass energy density x mass of feedstock) to the amount of embedded non-renewable fossil energy required to produce algal biomass. $EROI_{\text{fossil}}$ (equivalent to the fossil energy ratio[7, 8]) is related to the net energy balance,

which is defined as the difference between the amount of energy stored in biomass to the amount of embedded nonrenewable-fossil energy required to produce biomass. This relationship is highlighted in the following cases:

| | |
|---------------------|----------------------------|
| $EROI_{fossil} > 1$ | Energy Balance is Positive |
| $EROI_{fossil} = 1$ | Energy Balance is Zero |
| $EROI_{fossil} < 1$ | Energy Balance is Negative |

$EROI_{fossil}$ has distinct significant advantages over contemporary economic analysis. These include: $EROI_{fossil}$ is not affected by market imperfections as is economic analysis, and $EROI_{fossil}$ can be used as a metric to rank the “renewability” of various energy technologies.

1.3.2. Life Cycle Assessment (LCA)

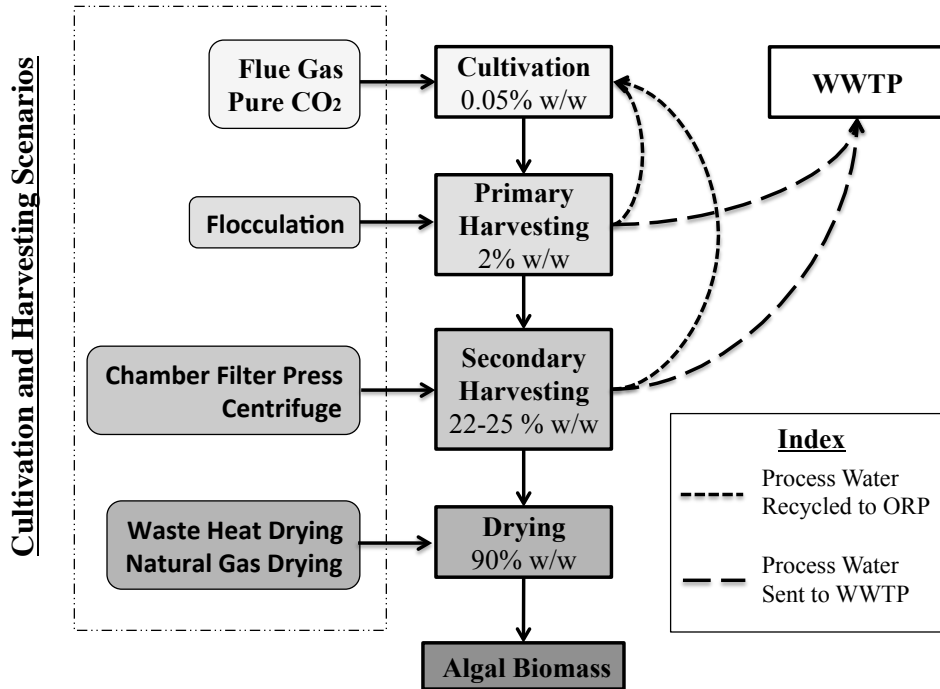
Life Cycle Assessment allows for the quantification of the environmental impacts of a product or service, incorporating the related resource consumption, emissions, and impacts across the various stages of the products life. LCA follows ISO 14040 standards [9].

1.4. Functional Unit and System Boundary

The scope of this LCA is cradle to gate, in which all processes upstream of dried biomass are evaluated. With the exception of PVC lining, previous LCA’s have shown that algae infrastructure related impacts are negligible as compared to other system processes[1], and were thus excluded from the scope of this study. The functional unit was chosen as one Mega-Joule (MJ) of dried biomass.

1.5. Production Chain Overview

Figure S1: Microalgal biomass production chain



1.6. Cultivation Locations

1.6.1. Electricity Mix

Data concerning the regional electricity mix for the cultivation locations was gathered from the EPA’s “Power Profiler”, based off the 2007 Emissions and Generation Resource Integrated Database (eGRID), and is presented in Table S1[10]. Life cycle impact factors for regional electricity generation were constructed using the SimaPro software package and eGRID database. Existing USLCI data for electricity generation was modified for each location based on the electricity generation mix (% Coal, Gas, Oil, Nuclear, Hydro, Ren, etc). Impact factors for regional electricity generation were created using the Tool for the Reduction and Assessment of Chemical and other environmental Impacts (TRACI) and cumulative energy demand (CED) methods. Furthermore, electricity distribution losses were accounted for in SimaPro.

Table S1 – Electricity Mix

| Resource Mix (%) | | | | | | | |
|------------------|-----------------|------|------|-----|---------|-------|----------------------|
| State | City | Coal | Gas | Oil | Nuclear | Hydro | Non-Hydro Renewables |
| AL | Mobile | 52.2 | 22.3 | 0.3 | 18.1 | 4.1 | 2.9 |
| AZ | Phoenix | 38.6 | 35.7 | 0.1 | 16.5 | 6.1 | 3.1 |
| CA | San Diego | 7.3 | 53 | 1.4 | 14.9 | 12.7 | 10.1 |
| FL | Daytona Beach | 23.7 | 54.8 | 4.4 | 14 | 0 | 1.7 |
| FL | Jacksonville | 23.7 | 54.8 | 4.4 | 14 | 0 | 1.7 |
| FL | Key West | 23.7 | 54.8 | 4.4 | 14 | 0 | 1.7 |
| FL | Miami | 23.7 | 54.8 | 4.4 | 14 | 0 | 1.7 |
| FL | Tallahassee | 23.7 | 54.8 | 4.4 | 14 | 0 | 1.7 |
| FL | Tampa | 23.7 | 54.8 | 4.4 | 14 | 0 | 1.7 |
| FL | West Palm Beach | 23.7 | 54.8 | 4.4 | 14 | 0 | 1.7 |
| GA | Savannah | 52.2 | 22.3 | 0.3 | 18.1 | 4.1 | 2.9 |
| LA | Baton Rouge | 22.7 | 45.1 | 1.5 | 26 | 1.7 | 1.9 |
| LA | Lake Charles | 22.7 | 45.1 | 1.5 | 26 | 1.7 | 1.9 |
| LA | New Orleans | 22.7 | 45.1 | 1.5 | 26 | 1.7 | 1.9 |
| TX | Austin | 33 | 47.8 | 1.1 | 12.3 | 0.2 | 5.5 |
| TX | Brownsville | 33 | 47.8 | 1.1 | 12.3 | 0.2 | 5.5 |
| TX | Corpus Christi | 33 | 47.8 | 1.1 | 12.3 | 0.2 | 5.5 |
| TX | Houston | 33 | 47.8 | 1.1 | 12.3 | 0.2 | 5.5 |
| TX | Lufkin | 33 | 47.8 | 1.1 | 12.3 | 0.2 | 5.5 |
| TX | Port Arthur | 22.7 | 45.1 | 1.5 | 26 | 1.7 | 1.9 |
| TX | San Antonio | 33 | 47.8 | 1.1 | 12.3 | 0.2 | 5.5 |
| TX | Victoria | 33 | 47.8 | 1.1 | 12.3 | 0.2 | 5.5 |

2. SOLAR INSOLATION AND CLIMATOLOGICAL DATA

2.1. Solar Insolation

Data concerning solar insolation for the cultivation locations was gathered from the National Solar Radiation Database (NSRD); this data set contains the average values of solar insolation over a thirty-year period (1961-1990)[11], summarized in

Table S2.

Table S2 - Average Solar Insolation (kWh/m²-day)

| State | City | March | April | May | June | July | Aug | Sept | Oct | Average |
|-------|-----------------|-------|-------|-----|------|------|-----|------|-----|---------|
| AL | Mobile | 4.4 | 5.4 | 5.9 | 5.9 | 5.6 | 5.2 | 4.7 | 4.2 | 5.2 |
| AZ | Phoenix | 5.5 | 7.1 | 8.0 | 8.4 | 7.6 | 7.1 | 6.1 | 4.9 | 6.8 |
| CA | San Diego | 4.9 | 6.1 | 6.3 | 6.5 | 6.9 | 6.5 | 5.4 | 4.4 | 5.9 |
| FL | Daytona Beach | 5.0 | 6.2 | 6.4 | 6.1 | 6.0 | 5.7 | 4.9 | 4.2 | 5.6 |
| FL | Jacksonville | 4.7 | 5.9 | 6.1 | 6.0 | 5.8 | 5.4 | 4.6 | 4.0 | 5.3 |
| FL | Key West | 5.5 | 6.3 | 6.3 | 6.1 | 6.1 | 5.8 | 5.2 | 4.6 | 5.7 |
| FL | Miami | 5.2 | 6.0 | 6.0 | 5.6 | 5.8 | 5.6 | 4.9 | 4.4 | 5.4 |
| FL | Tallahassee | 4.7 | 5.9 | 6.3 | 6.1 | 5.8 | 5.5 | 4.9 | 4.3 | 5.4 |
| FL | Tampa | 5.1 | 6.2 | 6.4 | 6.1 | 5.8 | 5.5 | 4.9 | 4.4 | 5.6 |
| FL | West Palm Beach | 5.0 | 5.9 | 6.0 | 5.7 | 5.9 | 5.6 | 4.8 | 4.2 | 5.4 |
| GA | Savannah | 4.7 | 5.8 | 6.2 | 6.3 | 6.1 | 5.5 | 4.7 | 4.1 | 5.4 |
| LA | Baton Rouge | 4.4 | 5.4 | 5.9 | 6.0 | 5.7 | 5.4 | 4.8 | 4.3 | 5.2 |
| LA | Lake Charles | 4.5 | 5.4 | 6.0 | 6.3 | 6.0 | 5.6 | 5.0 | 4.3 | 5.4 |
| LA | New Orleans | 4.5 | 5.5 | 6.1 | 6.1 | 5.7 | 5.5 | 4.9 | 4.3 | 5.3 |
| TX | Austin | 4.7 | 5.4 | 5.9 | 6.6 | 6.8 | 6.3 | 5.2 | 4.4 | 5.7 |
| TX | Brownsville | 4.6 | 5.3 | 5.8 | 6.4 | 6.5 | 6.0 | 5.2 | 4.5 | 5.5 |
| TX | Corpus Christi | 4.4 | 5.0 | 5.5 | 6.1 | 6.3 | 5.8 | 5.0 | 4.3 | 5.3 |
| TX | Houston | 4.2 | 5.0 | 5.6 | 6.0 | 5.9 | 5.6 | 4.9 | 4.2 | 5.2 |
| TX | Lufkin | 4.5 | 5.3 | 5.9 | 6.4 | 6.4 | 6.0 | 5.1 | 4.3 | 5.5 |
| TX | Port Arthur | 4.3 | 5.2 | 5.8 | 6.3 | 6.1 | 5.7 | 5.0 | 4.3 | 5.3 |
| TX | San Antonio | 4.8 | 5.5 | 6.0 | 6.7 | 6.9 | 6.4 | 5.4 | 4.5 | 5.8 |
| TX | Victoria | 4.4 | 5.1 | 5.7 | 6.2 | 6.2 | 5.8 | 5.0 | 4.3 | 5.3 |

2.1.1. Photo-synthetically Active Radiation (PAR) Energy

The %PAR (Percent Photo-synthetically Active Radiation) is defined as the ratio of the amount of solar energy that can be utilized in photosynthesis to the full spectrum solar energy, and as such is unit-less. The %PAR was assumed to be 46%, which agrees with previous studies[12], and was assumed to be the same for all examined locations.

Average PAR energy values (kWh/m²-day) were constructed by multiplying average values of solar insolation (kWh/m²-day), denoted as I_{avg}, by the %PAR. This is highlighted below, in Equation 1.

Equation 1
$$PAR_{avg} = \%PAR * I_{avg}$$

Substituting in the value for %PAR into Equation 1 yields:

Equation 2
$$PAR_{avg} = \left(\frac{46}{100}\right) * I_{avg}$$

Wherein, PAR_{avg} is the average PAR energy (kWh/m²-day) and I_{avg} is the value of average solar insolation for the given location and month in units of (kWh/m²-day). Note: to convert from kWh to MJ multiply by 3.6. The values for average PAR energy (MJ/m²-day) for various months and locations are presented in Table S3.

Table S3 - Average PAR Energy (MJ/m²-day)

| State | City | March | April | May | June | July | Aug | Sept | Oct | Average |
|-------|-----------------|-------|-------|------|------|------|------|------|-----|---------|
| AL | Mobile | 7.3 | 8.9 | 9.8 | 9.8 | 9.3 | 8.6 | 7.8 | 7.0 | 8.5 |
| AZ | Phoenix | 9.1 | 11.8 | 13.2 | 13.9 | 12.6 | 11.8 | 10.1 | 8.1 | 11.3 |
| CA | San Diego | 8.1 | 10.1 | 10.4 | 10.8 | 11.4 | 10.8 | 8.9 | 7.3 | 9.7 |
| FL | Daytona Beach | 8.3 | 10.3 | 10.6 | 10.1 | 9.9 | 9.4 | 8.1 | 7.0 | 9.2 |
| FL | Jacksonville | 7.8 | 9.8 | 10.1 | 9.9 | 9.6 | 8.9 | 7.6 | 6.6 | 8.8 |
| FL | Key West | 9.1 | 10.4 | 10.4 | 10.1 | 10.1 | 9.6 | 8.6 | 7.6 | 9.5 |
| FL | Miami | 8.6 | 9.9 | 9.9 | 9.3 | 9.6 | 9.3 | 8.1 | 7.3 | 9.0 |
| FL | Tallahassee | 7.8 | 9.8 | 10.4 | 10.1 | 9.6 | 9.1 | 8.1 | 7.1 | 9.0 |
| FL | Tampa | 8.4 | 10.3 | 10.6 | 10.1 | 9.6 | 9.1 | 8.1 | 7.3 | 9.2 |
| FL | West Palm Beach | 8.3 | 9.8 | 9.9 | 9.4 | 9.8 | 9.3 | 7.9 | 7.0 | 8.9 |
| GA | Savannah | 7.8 | 9.6 | 10.3 | 10.4 | 10.1 | 9.1 | 7.8 | 6.8 | 9.0 |
| LA | Baton Rouge | 7.3 | 8.9 | 9.8 | 9.9 | 9.4 | 8.9 | 7.9 | 7.1 | 8.7 |
| LA | Lake Charles | 7.5 | 8.9 | 9.9 | 10.4 | 9.9 | 9.3 | 8.3 | 7.1 | 8.9 |
| LA | New Orleans | 7.5 | 9.1 | 10.1 | 10.1 | 9.4 | 9.1 | 8.1 | 7.1 | 8.8 |
| TX | Austin | 7.8 | 8.9 | 9.8 | 10.9 | 11.3 | 10.4 | 8.6 | 7.3 | 9.4 |
| TX | Brownsville | 7.6 | 8.8 | 9.6 | 10.6 | 10.8 | 9.9 | 8.6 | 7.5 | 9.2 |
| TX | Corpus Christi | 7.3 | 8.3 | 9.1 | 10.1 | 10.4 | 9.6 | 8.3 | 7.1 | 8.8 |
| TX | Houston | 7.0 | 8.3 | 9.3 | 9.9 | 9.8 | 9.3 | 8.1 | 7.0 | 8.6 |
| TX | Lufkin | 7.5 | 8.8 | 9.8 | 10.6 | 10.6 | 9.9 | 8.4 | 7.1 | 9.1 |
| TX | Port Arthur | 7.1 | 8.6 | 9.6 | 10.4 | 10.1 | 9.4 | 8.3 | 7.1 | 8.8 |
| TX | San Antonio | 7.9 | 9.1 | 9.9 | 11.1 | 11.4 | 10.6 | 8.9 | 7.5 | 9.6 |
| TX | Victoria | 7.3 | 8.4 | 9.4 | 10.3 | 10.3 | 9.6 | 8.3 | 7.1 | 8.8 |

2.2. Auxiliary Climatological Parameters

Data for average wind speed (m/s), average temperature (C), average pressure (kPa), and relative humidity (%) was gathered from the National Solar Radiation Database (NSRD)[11], and are presented in Table S4 to Table S7.

Table S4: Average Pressure

| State | City | Pressure (mb) | Pressure (kPa) |
|-------|-----------------|---------------|----------------|
| AL | Mobile | 1010 | 101 |
| AZ | Phoenix | 974 | 97.4 |
| CA | San Diego | 1014 | 101.4 |
| FL | Daytona Beach | 1017 | 101.7 |
| FL | Jacksonville | 1017 | 101.7 |
| FL | Key West | 1016 | 101.6 |
| FL | Miami | 1017 | 101.7 |
| FL | Tallahassee | 1016 | 101.6 |
| FL | Tampa | 1018 | 101.8 |
| FL | West Palm Beach | 1017 | 101.7 |
| GA | Savannah | 1017 | 101.7 |
| LA | Baton Rouge | 1015 | 101.5 |
| LA | Lake Charles | 1016 | 101.6 |
| LA | New Orleans | 1017 | 101.7 |
| TX | Austin | 994 | 99.4 |
| TX | Brownsville | 1015 | 101.5 |
| TX | Corpus Christi | 1014 | 101.4 |
| TX | Houston | 1014 | 101.4 |
| TX | Lufkin | 1006 | 100.6 |
| TX | Port Arthur | 1017 | 101.7 |
| TX | San Antonio | 988 | 98.8 |
| TX | Victoria | 1012 | 101.2 |

Table S5: Average Wind Speed (m/s)

| State | City | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Average |
|-------|-----------------|-----|-----|-----|-----|-----|-----|-----|-----|---------|
| AL | Mobile | 4.7 | 4.6 | 3.9 | 3.4 | 3 | 2.9 | 3.4 | 3.6 | 3.7 |
| AZ | Phoenix | 3.2 | 3.4 | 3.4 | 3.2 | 3.4 | 3.2 | 3 | 2.8 | 3.2 |
| CA | San Diego | 3.5 | 3.7 | 3.7 | 3.6 | 3.5 | 3.5 | 3.4 | 3.1 | 3.5 |
| FL | Daytona Beach | 4.2 | 4.1 | 3.8 | 3.4 | 3.2 | 3 | 3.5 | 4 | 3.7 |
| FL | Jacksonville | 3.9 | 3.7 | 3.4 | 3.2 | 3 | 2.8 | 3.1 | 3.4 | 3.3 |
| FL | Key West | 5.5 | 5.3 | 4.8 | 4.5 | 4.3 | 4.1 | 4.3 | 5.2 | 4.8 |
| FL | Miami | 4.9 | 4.8 | 4.4 | 3.8 | 3.7 | 3.7 | 3.8 | 4.4 | 4.2 |
| FL | Tallahassee | 3.4 | 3.2 | 2.9 | 2.5 | 2.3 | 2.3 | 2.7 | 2.9 | 2.8 |
| FL | Tampa | 4.2 | 4.1 | 3.9 | 3.6 | 3.3 | 3.1 | 3.4 | 3.8 | 3.7 |
| FL | West Palm Beach | 5.1 | 4.9 | 4.6 | 3.9 | 3.7 | 3.7 | 3.9 | 4.8 | 4.3 |
| GA | Savannah | 4.1 | 3.9 | 3.4 | 3.3 | 3.2 | 2.9 | 3.2 | 3.3 | 3.4 |
| LA | Baton Rouge | 4.1 | 3.9 | 3.4 | 2.9 | 2.6 | 2.4 | 2.9 | 2.9 | 3.1 |
| LA | Lake Charles | 4.6 | 4.5 | 3.9 | 3.4 | 2.9 | 2.7 | 3.2 | 3.4 | 3.6 |
| LA | New Orleans | 4.2 | 4.1 | 3.6 | 3 | 2.6 | 2.6 | 3.1 | 3.3 | 3.3 |
| TX | Austin | 4.7 | 4.5 | 4.2 | 3.8 | 3.5 | 3.4 | 3.5 | 3.5 | 3.9 |
| TX | Brownsville | 5.9 | 6 | 5.7 | 5.1 | 5 | 4.6 | 4.2 | 4.1 | 5.1 |
| TX | Corpus Christi | 6.4 | 6.4 | 5.7 | 5 | 5.1 | 5 | 4.9 | 4.8 | 5.4 |
| TX | Houston | 4.4 | 4.4 | 3.9 | 3.6 | 3.2 | 3 | 3.3 | 3.4 | 3.7 |
| TX | Lufkin | 3.6 | 3.5 | 3.1 | 2.6 | 2.4 | 2.4 | 2.6 | 2.6 | 2.9 |
| TX | Port Arthur | 5 | 5.1 | 4.4 | 3.8 | 3.2 | 3.1 | 3.6 | 3.8 | 4.0 |
| TX | San Antonio | 4.5 | 4.4 | 4.4 | 4.3 | 4.2 | 3.8 | 3.8 | 3.8 | 4.2 |
| TX | Victoria | 5.3 | 5.2 | 4.9 | 4.3 | 4.1 | 3.8 | 4 | 4.1 | 4.5 |

Table S6: Average Temperature (°C)

| State | City | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Average |
|-------|---------------|------|------|------|------|------|------|------|------|---------|
| AL | Mobile | 15.8 | 19.9 | 23.6 | 26.9 | 27.9 | 27.7 | 25.5 | 20.2 | 23.4 |
| AZ | Phoenix | 16.8 | 21.1 | 26.0 | 31.2 | 34.2 | 33.1 | 29.8 | 23.6 | 27.0 |
| CA | San Diego | 15.3 | 16.7 | 17.8 | 19.3 | 21.7 | 22.6 | 21.9 | 19.8 | 19.4 |
| FL | Daytona Beach | 17.9 | 20.7 | 23.7 | 26.3 | 27.3 | 27.2 | 26.3 | 23.0 | 24.1 |
| FL | Jacksonville | 16.2 | 19.4 | 23.0 | 26.2 | 27.6 | 27.3 | 25.6 | 21.0 | 23.3 |
| FL | Key West | 23.2 | 25.0 | 27.0 | 28.4 | 29.1 | 29.1 | 28.5 | 26.7 | 27.1 |
| FL | Miami | 22.1 | 24.0 | 25.9 | 27.4 | 28.1 | 28.2 | 27.7 | 25.7 | 26.1 |
| FL | Tallahassee | 15.7 | 19.1 | 23.1 | 26.4 | 27.4 | 27.4 | 25.7 | 20.4 | 23.2 |

| | | | | | | | | | | |
|----|-----------------|------|------|------|------|------|------|------|------|------|
| FL | Tampa | 19.1 | 21.8 | 25.1 | 27.2 | 27.8 | 27.8 | 27.2 | 23.8 | 25.0 |
| FL | West Palm Beach | 21.1 | 23.0 | 25.3 | 27.0 | 27.9 | 28.1 | 27.6 | 25.4 | 25.7 |
| GA | Savannah | 15.1 | 18.9 | 23.1 | 26.2 | 27.7 | 27.2 | 24.8 | 19.6 | 22.8 |
| LA | Baton Rouge | 16.3 | 20.5 | 24.1 | 26.9 | 27.9 | 27.7 | 25.6 | 20.3 | 23.7 |
| LA | Lake Charles | 15.9 | 20.2 | 23.8 | 26.8 | 27.9 | 27.7 | 25.4 | 20.6 | 23.5 |
| LA | New Orleans | 16.4 | 20.3 | 23.8 | 26.7 | 27.7 | 27.5 | 25.6 | 20.6 | 23.6 |
| TX | Austin | 16.4 | 20.9 | 24.2 | 27.4 | 29.2 | 29.3 | 26.8 | 21.7 | 24.5 |
| TX | Brownsville | 20.4 | 24.1 | 26.6 | 28.3 | 29.2 | 29.2 | 27.7 | 24.3 | 26.2 |
| TX | Corpus Christi | 18.7 | 22.5 | 25.5 | 27.7 | 28.9 | 29.0 | 27.2 | 23.3 | 25.4 |
| TX | Houston | 15.9 | 20.2 | 23.6 | 26.9 | 28.1 | 27.9 | 25.7 | 20.9 | 23.7 |
| TX | Lufkin | 15.3 | 19.7 | 23.3 | 26.6 | 28.2 | 28.1 | 25.2 | 19.8 | 23.3 |
| TX | Port Arthur | 16.3 | 20.5 | 24.0 | 27.1 | 28.2 | 28.1 | 25.9 | 20.9 | 23.9 |
| TX | San Antonio | 16.5 | 20.7 | 24.2 | 27.9 | 29.4 | 29.4 | 26.3 | 21.2 | 24.5 |
| TX | Victoria | 17.4 | 21.4 | 24.8 | 27.6 | 28.9 | 28.9 | 26.4 | 22.1 | 24.7 |

Table S7: Relative Humidity (%)

| State | City | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Average |
|-------|-----------------|-----|-----|-----|-----|-----|-----|-----|-----|---------|
| AL | Mobile | 71 | 70 | 71 | 73 | 76 | 78 | 75 | 71 | 73 |
| AZ | Phoenix | 39 | 28 | 22 | 19 | 32 | 36 | 36 | 37 | 31 |
| CA | San Diego | 67 | 67 | 71 | 74 | 75 | 74 | 73 | 69 | 71 |
| FL | Daytona Beach | 71 | 69 | 72 | 77 | 78 | 80 | 79 | 75 | 75 |
| FL | Jacksonville | 71 | 69 | 73 | 77 | 78 | 80 | 81 | 79 | 76 |
| FL | Key West | 73 | 70 | 72 | 74 | 72 | 73 | 75 | 75 | 73 |
| FL | Miami | 69 | 67 | 72 | 76 | 75 | 76 | 78 | 75 | 74 |
| FL | Tallahassee | 72 | 70 | 72 | 76 | 80 | 81 | 78 | 74 | 75 |
| FL | Tampa | 72 | 69 | 70 | 74 | 77 | 78 | 77 | 74 | 74 |
| FL | West Palm Beach | 70 | 67 | 71 | 77 | 77 | 76 | 77 | 74 | 74 |
| GA | Savannah | 67 | 65 | 70 | 74 | 76 | 79 | 78 | 73 | 73 |
| LA | Baton Rouge | 70 | 71 | 72 | 74 | 77 | 78 | 77 | 73 | 74 |
| LA | Lake Charles | 76 | 76 | 77 | 78 | 80 | 80 | 79 | 76 | 78 |
| LA | New Orleans | 73 | 73 | 74 | 76 | 79 | 79 | 78 | 75 | 76 |
| TX | Austin | 64 | 66 | 71 | 69 | 65 | 64 | 68 | 68 | 67 |
| TX | Brownsville | 75 | 75 | 77 | 75 | 73 | 74 | 76 | 75 | 75 |
| TX | Corpus Christi | 74 | 77 | 79 | 78 | 75 | 75 | 76 | 75 | 76 |
| TX | Houston | 73 | 74 | 75 | 75 | 75 | 75 | 76 | 74 | 75 |
| TX | Lufkin | 70 | 72 | 75 | 75 | 74 | 73 | 75 | 73 | 73 |
| TX | Port Arthur | 76 | 77 | 79 | 79 | 81 | 80 | 79 | 77 | 79 |
| TX | San Antonio | 63 | 66 | 71 | 69 | 65 | 65 | 68 | 67 | 67 |
| TX | Victoria | 72 | 74 | 76 | 76 | 74 | 74 | 76 | 74 | 75 |

2.3. Evaporation

Evaporations losses were constructed based on the Penman Equation, show in Equation 3 [13].

$$\text{Equation 3} \quad E_{mass} = \frac{mR_n + \gamma * 6.43 * (1 + 0.563 * U_m) * \delta e}{\lambda_v * (m + \gamma)}$$

Where:

E_{mass} = Evaporation rate (mm day⁻¹)

m = Slope of the saturation vapor pressure curve (kPa K⁻¹)

R_n = Net Solar radiation (MJ m⁻² day⁻¹)

γ = psychometric constant (kPa K⁻¹)

U_m = wind speed (m s⁻¹)

δe = vapor pressure deficit (kPa)

λ_v = latent heat of vaporization (MJ kg⁻¹)

For average solar insolation (I_{avg}) in units of (watts/m²), net solar radiation R_n in units of (MJ/m²-day) is computed using Equation 4 [1].

$$\text{Equation 4} \quad R_n = \left(I_{avg} * \left(\frac{63}{100} \right) - 40 \right) * \left(\frac{24}{1000} \right)$$

The latent heat of vaporization (MJ*kg⁻¹) is given by Equation 5 [13]

$$\text{Equation 5} \quad \lambda_v = (2.501 - 0.002361 * T_{avg_c})$$

Where: T_{avg_c} is the average temperature in Celsius

The slopes of the saturation vapor pressure curve in units of (kPa*K⁻¹) are presented in Equation 6.

$$\text{Equation 6} \quad m = \frac{711.5}{T_{avg_k}^2} * \exp \left(21.07 - \frac{5336}{T_{avg_k}} \right)$$

Where: T_{avg_k} is the average temperature in Kelvin

The psychometric constant in units of (kPa K⁻¹) is presented in Equation 7 [13].

Equation 7
$$\gamma = \frac{.0016286 * P_{avg_{kPa}}}{\lambda_v}$$

Where: $P_{avg_{kPa}}$ is the mean pressure for the given location in units of kPa. The vapor pressure deficit in units of (kPa), denoted δe , is given by Equation 8.

Equation 8
$$\delta e = (e_s - e_a) = (1 - \text{relative humidity}) * e_s$$

Where: e_s is the saturated vapor pressure of air (kPa), e_a is the vapor pressure of free flowing air (kPa), relative humidity (%).

The saturation vapor pressure of air in units of (kPa), denoted e_s , is approximated in Equation 9 [14].

Equation 9
$$e_s = \frac{1}{7.5} * \exp\left(21.07 - \frac{5336}{T_{avg_k}}\right)$$

Evaporative losses (mm/day) are presented in Table S8.

Table S8: Evaporative Losses (mm/day)

| State | City | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Average |
|-------|-----------------|-----|-----|-----|------|-----|-----|-----|-----|---------|
| AL | Mobile | 3.5 | 4.5 | 4.9 | 4.9 | 4.4 | 4.0 | 3.8 | 3.4 | 4.2 |
| AZ | Phoenix | 5.4 | 7.7 | 9.5 | 10.6 | 9.7 | 8.7 | 7.4 | 5.6 | 8.1 |
| CA | San Diego | 3.6 | 4.5 | 4.5 | 4.6 | 5.0 | 4.9 | 4.1 | 3.5 | 4.3 |
| FL | Daytona Beach | 3.9 | 5.0 | 5.2 | 4.7 | 4.6 | 4.2 | 3.8 | 3.5 | 4.4 |
| FL | Jacksonville | 3.5 | 4.6 | 4.7 | 4.6 | 4.4 | 3.9 | 3.3 | 2.8 | 4.0 |
| FL | Key West | 5.0 | 5.9 | 5.7 | 5.5 | 5.6 | 5.2 | 4.7 | 4.4 | 5.2 |
| FL | Miami | 4.8 | 5.6 | 5.3 | 4.6 | 4.9 | 4.7 | 4.0 | 3.9 | 4.7 |
| FL | Tallahassee | 3.3 | 4.3 | 4.7 | 4.5 | 4.1 | 3.8 | 3.6 | 3.1 | 3.9 |
| FL | Tampa | 4.0 | 5.1 | 5.5 | 5.0 | 4.6 | 4.2 | 3.9 | 3.7 | 4.5 |
| FL | West Palm Beach | 4.6 | 5.5 | 5.4 | 4.6 | 4.8 | 4.7 | 4.0 | 4.0 | 4.7 |
| GA | Savannah | 3.7 | 4.8 | 5.0 | 5.0 | 4.8 | 4.1 | 3.5 | 3.1 | 4.2 |
| LA | Baton Rouge | 3.4 | 4.3 | 4.7 | 4.7 | 4.3 | 4.0 | 3.6 | 3.2 | 4.0 |
| LA | Lake Charles | 3.2 | 4.1 | 4.6 | 4.8 | 4.4 | 4.1 | 3.7 | 3.2 | 4.0 |
| LA | New Orleans | 3.4 | 4.3 | 4.8 | 4.7 | 4.2 | 4.0 | 3.7 | 3.2 | 4.0 |
| TX | Austin | 4.2 | 4.9 | 5.1 | 5.8 | 6.3 | 6.0 | 4.7 | 3.8 | 5.1 |
| TX | Brownsville | 4.1 | 4.9 | 5.2 | 5.8 | 6.1 | 5.5 | 4.5 | 3.8 | 5.0 |
| TX | Corpus Christi | 4.0 | 4.5 | 4.7 | 5.2 | 5.8 | 5.4 | 4.5 | 3.8 | 4.7 |
| TX | Houston | 3.2 | 4.0 | 4.4 | 4.9 | 4.8 | 4.5 | 3.9 | 3.2 | 4.1 |
| TX | Lufkin | 3.3 | 4.0 | 4.4 | 4.8 | 4.9 | 4.7 | 3.8 | 3.0 | 4.1 |

| | | | | | | | | | | |
|----|-------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| TX | Port Arthur | 3.2 | 4.1 | 4.5 | 4.9 | 4.5 | 4.3 | 3.8 | 3.2 | 4.1 |
| TX | San Antonio | 4.2 | 4.9 | 5.2 | 6.1 | 6.7 | 6.2 | 4.9 | 4.0 | 5.3 |
| TX | Victoria | 3.7 | 4.4 | 4.8 | 5.2 | 5.4 | 5.0 | 4.2 | 3.6 | 4.6 |

2.4. Precipitation

Data concerning average rainfall for the various locations was taken from the National Oceanic and Atmospheric Administration (NOAA)[15], the average rainfall (mm/day) for the cultivation locations is presented in Table S9.

Table S9: Average Rainfall (mm/day)

| State | City | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Average |
|-------|-----------------|-----|-----|-----|-----|-----|-----|-----|-----|---------|
| AL | Mobile | 5.9 | 4.1 | 5.0 | 4.1 | 5.4 | 5.1 | 4.9 | 2.7 | 4.6 |
| AZ | Phoenix | 0.9 | 0.2 | 0.1 | 0.1 | 0.8 | 0.8 | 0.6 | 0.6 | 0.5 |
| CA | San Diego | 1.9 | 0.6 | 0.2 | 0.1 | 0.0 | 0.1 | 0.2 | 0.4 | 0.4 |
| FL | Daytona Beach | 3.1 | 2.1 | 2.7 | 4.7 | 4.2 | 5.0 | 5.4 | 3.7 | 3.9 |
| FL | Jacksonville | 3.2 | 2.6 | 2.9 | 4.4 | 4.9 | 5.6 | 6.5 | 3.2 | 4.2 |
| FL | Key West | 1.5 | 1.7 | 2.9 | 3.7 | 2.7 | 4.4 | 4.5 | 3.6 | 3.1 |
| FL | Miami | 2.1 | 2.8 | 4.5 | 7.0 | 4.7 | 7.1 | 6.9 | 5.1 | 5.0 |
| FL | Tallahassee | 5.3 | 2.9 | 4.1 | 5.7 | 6.6 | 5.8 | 4.1 | 2.7 | 4.6 |
| FL | Tampa | 2.3 | 1.5 | 2.3 | 4.5 | 5.3 | 6.2 | 5.4 | 1.9 | 3.7 |
| FL | West Palm Beach | 3.0 | 2.9 | 4.4 | 6.2 | 4.9 | 5.4 | 6.6 | 4.5 | 4.8 |
| GA | Savannah | 3.0 | 2.7 | 3.0 | 4.5 | 4.9 | 5.9 | 4.2 | 2.6 | 3.8 |
| LA | Baton Rouge | 4.2 | 4.6 | 4.4 | 4.4 | 4.9 | 4.8 | 4.0 | 3.1 | 4.3 |
| LA | Lake Charles | 2.9 | 3.0 | 5.0 | 5.0 | 4.2 | 4.0 | 4.9 | 3.2 | 4.0 |
| LA | New Orleans | 4.3 | 4.1 | 3.8 | 5.6 | 5.1 | 5.0 | 4.5 | 2.5 | 4.4 |
| TX | Austin | 1.8 | 2.1 | 4.1 | 3.1 | 1.6 | 1.9 | 2.4 | 3.3 | 2.5 |
| TX | Brownsville | 0.8 | 1.6 | 2.0 | 2.4 | 1.5 | 2.4 | 4.4 | 3.1 | 2.3 |
| TX | Corpus Christi | 1.4 | 1.7 | 2.9 | 2.9 | 1.6 | 2.9 | 4.1 | 3.2 | 2.6 |
| TX | Houston | 2.8 | 2.9 | 4.2 | 4.4 | 2.6 | 3.1 | 3.5 | 3.7 | 3.4 |
| TX | Lufkin | 3.0 | 3.2 | 4.0 | 3.1 | 2.6 | 2.5 | 2.8 | 2.7 | 3.0 |
| TX | Port Arthur | 3.1 | 3.1 | 4.8 | 5.4 | 4.3 | 4.0 | 5.0 | 3.8 | 4.2 |
| TX | San Antonio | 1.5 | 2.1 | 3.9 | 3.5 | 1.7 | 2.1 | 2.5 | 3.2 | 2.6 |
| TX | Victoria | 1.8 | 2.4 | 4.2 | 4.1 | 2.4 | 2.5 | 4.1 | 3.5 | 3.1 |

2.5. Net Water Accumulation

The net water accumulation (mm/day) was calculated as the difference between the average rainfall (mm/day) and evaporative losses (mm/day), as shown in Equation 10.

Equation 10 $NetWaterAccum = AvgRainfall - EvapLoss$

Negative values signify a net negative water accumulation, indicating that additional water must be pumped into the ponds. The values for net water accumulation for the various locations are shown in Table S10.

Table S10: Net Water Accumulation (mm/day)

| State | City | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Average |
|-------|-----------------|------|------|------|-------|------|------|------|------|---------|
| AL | Mobile | 2.4 | -0.2 | 0.1 | -0.6 | 0.9 | 1.1 | 1.3 | -0.7 | 0.5 |
| AZ | Phoenix | -4.5 | -7.5 | -9.4 | -10.5 | -8.9 | -8.0 | -6.8 | -5.0 | -7.6 |
| CA | San Diego | -1.8 | -3.9 | -4.4 | -4.5 | -5.0 | -4.8 | -4.0 | -3.1 | -3.9 |
| FL | Daytona Beach | -0.8 | -2.9 | -2.5 | 0.1 | -0.4 | 0.8 | 1.8 | 0.2 | -0.4 |
| FL | Jacksonville | -0.3 | -1.9 | -1.8 | 0.0 | 0.5 | 1.7 | 3.4 | 0.3 | 0.2 |
| FL | Key West | -3.5 | -4.2 | -2.9 | -1.6 | -2.9 | -0.8 | -0.1 | -0.8 | -2.1 |
| FL | Miami | -2.7 | -2.8 | -0.8 | 2.6 | -0.1 | 2.4 | 3.1 | 1.1 | 0.4 |
| FL | Tallahassee | 2.0 | -1.3 | -0.7 | 1.4 | 2.5 | 1.9 | 0.7 | -0.4 | 0.8 |
| FL | Tampa | -1.7 | -3.6 | -3.1 | -0.4 | 0.7 | 2.0 | 1.6 | -1.8 | -0.8 |
| FL | West Palm Beach | -1.5 | -2.5 | -1.0 | 1.8 | 0.1 | 0.8 | 2.8 | 0.5 | 0.1 |
| GA | Savannah | -0.7 | -2.0 | -2.0 | -0.4 | 0.1 | 1.8 | 0.8 | -0.5 | -0.4 |
| LA | Baton Rouge | 0.7 | 0.4 | -0.3 | -0.2 | 0.6 | 0.8 | 0.5 | 0.0 | 0.3 |
| LA | Lake Charles | -0.3 | -1.0 | 0.4 | 0.3 | -0.2 | -0.1 | 1.3 | 0.1 | 0.1 |
| LA | New Orleans | 0.9 | 0.0 | -1.0 | 1.1 | 0.9 | 1.0 | 1.0 | -0.7 | 0.4 |
| TX | Austin | -2.4 | -2.7 | -0.9 | -2.6 | -4.7 | -4.1 | -2.3 | -0.5 | -2.5 |
| TX | Brownsville | -3.3 | -3.2 | -3.2 | -3.3 | -4.6 | -3.0 | 0.0 | -0.7 | -2.7 |
| TX | Corpus Christi | -2.6 | -2.7 | -1.9 | -2.2 | -4.1 | -2.5 | -0.3 | -0.6 | -2.1 |
| TX | Houston | -0.4 | -0.9 | -0.2 | -0.4 | -2.2 | -1.3 | -0.2 | 0.5 | -0.6 |
| TX | Lufkin | -0.2 | -0.7 | -0.4 | -1.6 | -2.3 | -2.2 | -0.9 | -0.3 | -1.1 |
| TX | Port Arthur | -0.2 | -0.8 | 0.3 | 0.7 | -0.2 | -0.3 | 1.3 | 0.6 | 0.2 |
| TX | San Antonio | -2.7 | -2.7 | -1.3 | -2.5 | -5.0 | -4.0 | -2.4 | -0.8 | -2.7 |
| TX | Victoria | -1.9 | -1.9 | -0.6 | -1.0 | -3.0 | -2.5 | 0.0 | -0.1 | -1.4 |

3. ALGAL BIOMASS

3.1. Fractionated Biomass Composition

The composition and net calorific value of the biomass fractions were taken from Lardon et al. 2009, and are presented in Table S11[16].

Table S11: Biomass Content

| | Fraction | Composition | Molar Mass (g*mole ⁻¹) | Net Calorific Value (MJ/g- biomass) |
|---|--------------|--|------------------------------------|-------------------------------------|
| 1 | Protein | C _{4.43} H ₇ O _{1.44} N _{1.16} | 100.1 | 15.5*10 ⁻³ |
| 2 | Carbohydrate | C ₆ H ₁₂ O ₆ | 180 | 13*10 ⁻³ |
| 3 | Lipid | C ₄₀ H ₇₄ O ₅ | 634 | 38.3*10 ⁻³ |

3.2. Algal Composition

The algae composition was assumed to be 50% proteins, 25% carbohydrates, 20% lipids, and 5% other organic material, which correlates with previous studies [17, 18]. It was assumed that the values of P, K, Mg, and S vary linearly with the protein content; a proportionality constant was constructed based on a reference composition of *Chlorella vulgaris*, obtained from Lardon et al. 2009[16]. The algae compositional parameters are provided in Table S12, additionally information on reported algal composition, lipid content, and productivities are provided in Table S13 and Table S14.

Table S12: Algae Composition

| | Parameters | Reference Composition (g/kg-biomass) | Composition assumed in this study (g/kg-biomass) |
|---|--------------|--------------------------------------|--|
| 1 | Protein | 282 | 500 |
| 2 | Carbohydrate | 495 | 250 |
| 3 | Lipid | 175 | 200 |
| 4 | C | 480 | 517 |
| 5 | N | 46 | 81.2 |
| 6 | P | 9.9 | 17.6 |
| 7 | K | 8.2 | 14.5 |
| 8 | Mg | 3.8 | 6.7 |
| 9 | S | 2.2 | 3.9 |

Table S13 – Fractionated Biomass composition for different algal biomass strains (% dry matter)

| Parameters | Protein | Carbohydrates | Lipids | Nucleic acid |
|----------------------------------|---------|---------------|--------|--------------|
| <i>Aphanizomenon flos-aquae</i> | 62 | 23 | 3 | - |
| <i>Anabaena cylindrica</i> | 43-56 | 25-30 | 4-7 | - |
| <i>Arthrospira maxima</i> | 60-71 | 13-16 | 6-7 | - |
| <i>Chlamydomonas reinhardtii</i> | 48 | 17 | 21 | - |
| <i>Chlorella pyrenoidosa</i> | 57 | 26 | 2 | - |
| <i>Chlorella vulgaris</i> | 51-58 | 12-17 | 14-22 | 4-5 |
| <i>Dunaliella bioculata</i> | 49 | 4 | 8 | - |
| <i>Dunaliella salina</i> | 57 | 32 | 6 | - |
| <i>Euglena gracilis</i> | 39-61 | 14-18 | 14-20 | - |
| <i>Porphyridium cruentum</i> | 28-39 | 40-57 | 9-14 | - |
| <i>Prymnesium parvum</i> | 28-45 | 25-33 | 22-38 | 1-2 |
| <i>Scenedesmus dimorphus</i> | 8-18 | 21-52 | 16-40 | - |
| <i>Scenedesmus obliquus</i> | 50-56 | 10-17 | 12-14 | 3-6 |
| <i>Scenedesmus quadricauda</i> | 47 | - | 1.9 | - |
| <i>Spirogyra sp.</i> | 6-20 | 33-64 | 11-21 | - |
| <i>Spirulina maxima</i> | 60-71 | 13-16 | 6-7 | 3-4.5 |
| <i>Spirulina platensis</i> | 46-63 | 8-14 | 4-9 | 2-5 |
| <i>Synechococcus sp.</i> | 63 | 15 | 11 | 5 |
| <i>Tetraselmis maculata</i> | 52 | 15 | 3 | - |

Adopted from: ref[18, 19]

Table S14 – Lipid content and productivity for select microalgae strains

| Microalgae species | Marine or Freshwater | Lipid content (% dry weight) | Lipid productivity (mg/L/day) | Volumetric productivity (g/L/day) |
|---------------------------------|----------------------|------------------------------|-------------------------------|-----------------------------------|
| <i>Ankistrodesmus sp.</i> | Freshwater | 24.0-31.0 | - | - |
| <i>Botryococcus braunii</i> | Freshwater | 25.0-75.0 | - | 0.02 |
| <i>Chaetoceros muelleri</i> | Marine | 33.6 | 21.8 | 0.07 |
| <i>Chaetoceros calcitrans</i> | Marine | 14.6-16.4/39.8 | 17.6 | 0.04 |
| <i>Chlorella emersonii</i> | Freshwater | 25.0-63.0 | 10.3-50.0 | 0.036-0.041 |
| <i>Chlorella protothecoides</i> | Freshwater | 14.6-57.8 | 1214 | 2.00-7.70 |
| <i>Chlorella sorokiniana</i> | Freshwater | 19.0-22.0 | 44.7 | 0.23-1.47 |
| <i>Chlorella vulgaris</i> | Freshwater | 5.0-58.0 | 11.2-40.0 | 0.02-0.20 |
| <i>Chlorella sp.</i> | Freshwater | 10.0-48.0 | 42.1 | 0.02-2.5 |
| <i>Chlorella pyrenoidosa</i> | Freshwater | 2 | - | 2.90-3.64 |
| <i>Chlorella</i> | Freshwater | 18.0-57.0 | 18.7 | - |
| <i>Chlorococcum sp.</i> | Freshwater | 19.3 | 53.7 | 0.28 |
| <i>Cryptocodinium cohnii</i> | Marine | 20.0-51.1 | - | 10 |
| <i>Dunaliella salina</i> | Marine | 6.0-25.0 | 116 | 0.22-0.34 |
| <i>Dunaliella primolecta</i> | Marine | 23.1 | - | 0.09 |
| <i>Dunaliella tertiolecta</i> | Marine | 16.7-71.0 | - | 0.12 |
| <i>Dunaliella sp.</i> | Marine | 17.5-67.0 | 33.5 | - |
| <i>Ellipsoidion sp.</i> | Freshwater | 27.4 | 47.3 | 0.17 |
| <i>Euglena gracilis</i> | Freshwater | 14.0-20.0 | - | 7.7 |
| <i>Haematococcus pluvialis</i> | Freshwater | 25 | - | 0.05-0.06 |
| <i>Isochrysis galbana</i> | Marine | 7.0-40.0 | - | 0.32-1.60 |
| <i>Isochrysis sp.</i> | Marine | 7.1-33 | 37.8 | 0.08-0.17 |

| | | | | |
|----------------------------------|------------|---------------|------------|------------|
| <i>Monodus subterraneus</i> | Freshwater | 16 | 30.4 | 0.19 |
| <i>Monallanthus salina</i> | Marine | 20.0-22.0 | - | 0.08 |
| <i>Nannochloris sp.</i> | Freshwater | 20.0-56.0 | 60.9-76.5 | 0.17-0.51 |
| <i>Nannochloropsis oculata.</i> | Freshwater | 22.7-29.7 | 84.0-142.0 | 0.37-0.48 |
| <i>Nannochloropsis sp.</i> | Freshwater | 12.0-53.0 | 37.6-90.0 | 0.17-1.43 |
| <i>Neochloris oleoabundans</i> | Freshwater | 29.0-65.0 | 90.0-134.0 | - |
| <i>Nitzschia sp.</i> | Freshwater | 16.0-47.0 | - | - |
| <i>Oocystis pusilla</i> | Freshwater | 10.5 | - | - |
| <i>Pavlova salina</i> | Marine | 30.9 | 49.4 | 0.16 |
| <i>Pavlova lutheri</i> | Marine | 35.5 | 40.2 | 0.14 |
| <i>Phaeodactylum tricornutum</i> | Marine | 18.0-57.0 | 44.8 | 0.003-1.9 |
| <i>Porphyridium cruentum</i> | Marine | 9.0-18.8/60.7 | 34.8 | 0.36-1.50 |
| <i>Scenedesmus obliquus</i> | Freshwater | 11.0-55.0 | - | 0.004-0.74 |
| <i>Scenedesmus quadricauda</i> | Freshwater | 1.9-18.4 | 35.1 | 0.19 |
| <i>Scenedesmus sp.</i> | Freshwater | 19.6-21.1 | 40.8-53.9 | 0.03-0.26 |
| <i>Skeletonema sp.</i> | Marine | 13.3-31.8 | 27.3 | 0.09 |
| <i>Skeletonema costatum</i> | Marine | 13.5-51.3 | 17.4 | 0.08 |
| <i>Spirulina platensis</i> | Freshwater | 4.0-16.6 | - | 0.06-4.3 |
| <i>Spirulina maxima</i> | Freshwater | 4.0-9.0 | - | 0.21-0.25 |
| <i>Thalassiosira pseudonana</i> | Marine | 20.6 | 17.4 | 0.08 |
| <i>Tetraselmis suecica</i> | Marine | 8.5-23.0 | 27.0-36.4 | 0.12-0.32 |
| <i>Tetraselmis sp.</i> | Marine | 12.6-14.7 | 43.4 | 0.3 |

Adopted from: ref[20]

3.3. Algal Lower Heating Value

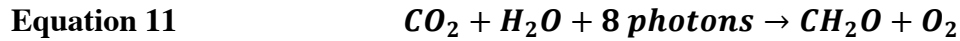
The energetic content of the algae in units of MJ/kg-biomass, denoted as β , was calculated as the sum of the individual biomass fractions (g/kg biomass) multiplied by their respective energetic content (MJ/g). The biomass Lower Heating Value (LHV) was computed to be 18.66 MJ/kg-biomass.

4. Algal Growth Rates

Algae growth rates were calculated based on the amount of PAR energy a region receives as well as efficiency terms determined by both pond design and characteristics of the algae culture.

4.1 Efficiency Terms

Photosynthetic Efficiency: accounts for the efficiency of converting solar energy into chemical energy by the process of photosynthesis. The equation governing photosynthesis is presented in Equation 11. The photosynthetic efficiency is determined by the quantum requirement, average photon energy, and carbohydrate energy content, and is presented in Equation 12. Values for quantum requirement, average photon energy, and carbohydrate energy content were taken from Weyer et al. 2010[12].



- a. *Quantum Requirement* (Mole Photons/Mole CH₂O): represents the number of photons needed to produce a photosynthetic reaction, this value was assumed to be 8 moles of photons per mole of CH₂O. [12]
- b. *Average Photon Energy* (MJ/Mole Photons): corresponds to the average photonic energy of solar radiation, this value was assumed to be 225.3×10^{-3} MJ per mole of photons. [12]
- c. *Carbohydrate Energy Content* (MJ/Mole CH₂O): represents the energetic content of CH₂O formed in photosynthesis, this value was taken to be 482.5×10^{-3} MJ per mole of CH₂O. [12]

Equation 12
$$\text{Photosynthetic Efficiency (\%)} = \left(\frac{\text{Carbohydrate Energy Content}}{\text{Average Photon Energy} \times \text{Quantum Requirement}} \right) \times 100$$

Values for photosynthetic efficiency, quantum requirement, average photon energy, and carbohydrate energy content are presented in Table S15.

Table S15: Photosynthetic Efficiency Terms

| Term | Value |
|---|------------------------|
| Photosynthetic Efficiency (%) | 26.8 |
| Quantum Requirement (Moles Photons/Moles CH ₂ O): | 8 |
| Average Photon Energy (MJ/Mole Photons): | 225.3×10^{-3} |
| Carbohydrate Energy Content (MJ/Mole CH ₂ O): | 482.5×10^{-3} |

Losses due to Reflection: accounts for solar radiation reflected off of the pond surface. For the months of March through October, and for regions between 20-30 degrees latitude, the percent of solar radiation reflected off of the pond surface ranges between 6-8%[21]. This corresponds to an average efficiency value of 93%.

Losses due to sub-optimal environmental conditions: accounts for losses in photon absorption due to temperature and environmental conditions, this value was taken to be 95%. [12]

Photon Utilization Efficiency: accounts for losses in photon absorption in the algal culture due to high or low light levels. For low light levels, photon utilization typically varies between 50-90%, for high light levels 10-30% [22]. For the open pond system, the photon utilization efficiency was taken to be 25%.

Biomass accumulation efficiency: Energy that is available to the algae culture will be used either in cellular respiration or will be stored as biomass. The biomass accumulation efficiency is the ratio of the amount of energy stored in the biomass to the total energy available to the algal culture, and thus shows the efficiency at which algae convert available energy into biomass, this value was taken to be 72%[23].

The values for the efficiency terms are shown in Table S16.

Table S16: Efficiency Factors

| | Efficiency Factors | Value (%) |
|----------|---|------------------|
| 1 | Photosynthetic efficiency: | 26.8 |
| 2 | Losses due to reflection: | 93 |
| 3 | Losses due to sub-optimal environmental conditions: | 95 |
| 4 | Photon utilization efficiency: | 25 |
| 5 | Biomass accumulation efficiency: | 72 |

Let α denote the product of the five efficiency terms, highlighted in Equation 13.

Equation 13 $\alpha = \prod_{i=1}^{i=5} \text{EfficiencyFactors}_i$

Computing this value, we find that

Equation 14 $\alpha = 4.262 * 10^{-2}$

Let us denote another quantity, δ (g/MJ), equal to the ratio of α (unit-less) to the lower heating value β (MJ/g), given by Equation 15.

Equation 15

$$\delta = \frac{\alpha}{\beta}$$

4.2. Algal Growth Rates

The growth rates in units of (g/m²-day) of the algae culture were calculated as the product of the average PAR energy (MJ/m²-day) and δ (g/MJ), expressed in Equation 16.

Equation 16

$$\text{Growth Rates} = \text{PAR}_{\text{avg}} * \delta$$

Monthly average micro-algal growth rates for all examined locations are presented in Table S17

Table S17: Algae Growth Rates (g/m²-day)

| State | City | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Average |
|-------|-----------------|------|------|------|------|------|------|------|------|---------|
| AL | Mobile | 16.6 | 20.4 | 22.3 | 22.3 | 21.2 | 19.6 | 17.8 | 15.9 | 19.5 |
| AZ | Phoenix | 20.8 | 26.8 | 30.2 | 31.7 | 28.7 | 26.8 | 23.0 | 18.5 | 25.8 |
| CA | San Diego | 18.5 | 23.0 | 23.8 | 24.6 | 26.1 | 24.6 | 20.4 | 16.6 | 22.2 |
| FL | Daytona Beach | 18.9 | 23.4 | 24.2 | 23.0 | 22.7 | 21.5 | 18.5 | 15.9 | 21.0 |
| FL | Jacksonville | 17.8 | 22.3 | 23.0 | 22.7 | 21.9 | 20.4 | 17.4 | 15.1 | 20.1 |
| FL | Key West | 20.8 | 23.8 | 23.8 | 23.0 | 23.0 | 21.9 | 19.6 | 17.4 | 21.7 |
| FL | Miami | 19.6 | 22.7 | 22.7 | 21.2 | 21.9 | 21.2 | 18.5 | 16.6 | 20.5 |
| FL | Tallahassee | 17.8 | 22.3 | 23.8 | 23.0 | 21.9 | 20.8 | 18.5 | 16.2 | 20.5 |
| FL | Tampa | 19.3 | 23.4 | 24.2 | 23.0 | 21.9 | 20.8 | 18.5 | 16.6 | 21.0 |
| FL | West Palm Beach | 18.9 | 22.3 | 22.7 | 21.5 | 22.3 | 21.2 | 18.1 | 15.9 | 20.4 |
| GA | Savannah | 17.8 | 21.9 | 23.4 | 23.8 | 23.0 | 20.8 | 17.8 | 15.5 | 20.5 |
| LA | Baton Rouge | 16.6 | 20.4 | 22.3 | 22.7 | 21.5 | 20.4 | 18.1 | 16.2 | 19.8 |
| LA | Lake Charles | 17.0 | 20.4 | 22.7 | 23.8 | 22.7 | 21.2 | 18.9 | 16.2 | 20.4 |
| LA | New Orleans | 17.0 | 20.8 | 23.0 | 23.0 | 21.5 | 20.8 | 18.5 | 16.2 | 20.1 |
| TX | Austin | 17.8 | 20.4 | 22.3 | 24.9 | 25.7 | 23.8 | 19.6 | 16.6 | 21.4 |
| TX | Brownsville | 17.4 | 20.0 | 21.9 | 24.2 | 24.6 | 22.7 | 19.6 | 17.0 | 20.9 |
| TX | Corpus Christi | 16.6 | 18.9 | 20.8 | 23.0 | 23.8 | 21.9 | 18.9 | 16.2 | 20.0 |
| TX | Houston | 15.9 | 18.9 | 21.2 | 22.7 | 22.3 | 21.2 | 18.5 | 15.9 | 19.6 |
| TX | Lufkin | 17.0 | 20.0 | 22.3 | 24.2 | 24.2 | 22.7 | 19.3 | 16.2 | 20.7 |
| TX | Port Arthur | 16.2 | 19.6 | 21.9 | 23.8 | 23.0 | 21.5 | 18.9 | 16.2 | 20.2 |
| TX | San Antonio | 18.1 | 20.8 | 22.7 | 25.3 | 26.1 | 24.2 | 20.4 | 17.0 | 21.8 |
| TX | Victoria | 16.6 | 19.3 | 21.5 | 23.4 | 23.4 | 21.9 | 18.9 | 16.2 | 20.2 |

5. Cultivation

5.1 CO₂ Procurement

CO₂ from a nearby natural gas fired power plant is supplied to the ponds in two ways:

5.1.1 Direct Injection of Flue Gas

(i) Flue gas is transported via lower pressure blowers and delivered to the algae ponds, evaluated at 22.2×10^{-3} kilowatt hours (kWh) per kg CO₂ [24]. While microalgae's potential to utilize flue gas as a source of CO₂ has been extensively cited in the literature [25, 26], it remains uncertain if the presence of flue gas will have detrimental effects upon the algae culture [27, 28]. More so, there is potential concern that industrial flue gases may contain heavy metals, which may decrease the quality of algal derived fuels. In this study, it is assumed that the Direct Injection (DI) of flue gas has no negative impacts upon the algae culture. While the utilization of industrial flue gas has the potential to decrease the high energetic cost associated with CO₂, the feasibility of direct injection of flue gas on an industrial scale remains questionable.

5.1.2 Monoethanolamine Scrubbing and Injection of Pure CO₂

(ii) Flue gas is separated into pure CO₂ via Monoethanolamine (MEA) scrubbing; this pure CO₂ is then delivered to the ponds via low-pressure blowers. Kadam et al. 2002 estimated that 1 kg of CO₂ from MEA extraction would require approximately 2.01 kg of steam and 32.65×10^{-3} kWh of electricity [24]. The energy required to transform water to steam was based on the enthalpy of steam, evaluated at 2.6 MJ/kg-steam. It was assumed that natural gas would be burned to generate steam; the energetic content of natural gas was taken to be 39 MJ/m³-natural gas and a boiler efficiency of 80% was assumed[29]. While MEA scrubbing is the more energy intensive of the two options, it insures that the algal culture does not experience the possible negative effects as associated with the direct injection of flue gas.

In this study, it was assumed that the microalgae culture captures only 70% of the injected CO₂ [4].

5.2. Paddlewheels

During cultivation, the algal growth medium is circulated by paddlewheels, consistent with current reactor configurations [1, 5, 30]. While other medium circulation configurations have been proposed, paddlewheels are a proven technology, and appear to be the most effective method of circulating the algal growth medium. For a mixing velocity of 15 cm/second and a pond depth of 0.3 m, the energetic cost of the paddlewheels was evaluated at 18 kWh/ha-day[5]. Existing studies have produced a wide

range of values for paddlewheel energetic consumption [1, 4, 29, 30], due to variations in pond depth, mixing velocity, and process assumptions. Deviations in paddlewheel energetic consumption were included as a parameter in the sensitivity analysis.

5.3. PVC Liner

A 0.75 mm thick PVC membrane was assumed to line the ORPs with an average lifetime of 5 years[4]. The mass of PVC required to line the ORPs was calculated as the product of the surface area, thickness of the PVC membrane, and density of the PVC liner. The required surface area of the PVC liner was assumed to be 120% times the surface area of the cultivation ponds (500 ha)[3]. The density of the PVC membrane was taken to be 950 kg/m³. The impacts of the PVC liner were normalized over the total amount of biomass produced over the lifetime of the PVC liner.

5.4. Freshwater Sourcing

The energy required to source freshwater to the ORPs was evaluated based off of conventional crop irrigation. It was assumed that electric pumps would bring surface and groundwater to the ORPs. The amount of energy required to source ground and surface water was based off of the 2008 Farm and ranch Irrigation survey[31], and the cost of electricity was assumed to be \$0.10 kWh [3]

6. HARVESTING

6.1. Flocculation

Algae are pumped into post-cultivation holding tanks in which a coagulant, aluminum sulfate, is injected at a rate of 100 g/m³ [32]. Aluminum sulfate was chosen for this study because it has been shown to be an effective coagulant for *Chlorella* algae [33]. Flocculation was assumed to concentrate the algal culture to a concentration of 2% (w/w). It was assumed that 90% of the medium from flocculation is recycled back to the cultivation ponds.

6.2. Pumping Requirements

Pumping power requirements (kWh/day) were constructed based on pipe flowrate (l/s), pipe diameter (m), pipe length (m), pipeline roughness (m), fluid velocity (m/s), pipe head-loss (m), Reynolds number (unit-less), and pump and motor efficiency (%).

The power requirement for pond pumping (J/s) is dependent on: g the gravitational acceleration (m/s²), total lift (m), flow rate (m³/s), density of fluid (kg/m³), and motor efficiency (%) and is presented in Equation 17.

$$\text{Equation 17} \quad \mathbf{Power}_{\text{pump}} = \frac{\mathbf{g} * (\mathbf{Total\ Lift}) * (\mathbf{Flowrate}) * (\mathbf{density\ of\ fluid})}{\mathbf{Motor\ Efficiency}}$$

The Total Lift (m) is calculated as the sum of the Static Lift (m) and Pipe Head loss (m), shown in Equation 18.

$$\text{Equation 18} \quad \mathbf{Total\ Lift} = \mathbf{Static\ Lift} + \mathbf{Pipe\ Head\ loss}$$

Pipe head loss was based on the Darcy–Weisbach equation and is presented in Equation 19.

$$\text{Equation 19} \quad \frac{\mathbf{f} * \mathbf{L} * \mathbf{V}^2}{\mathbf{2} * \mathbf{g} * \mathbf{D}} = \mathbf{h}_f$$

Where h_f is head loss due to friction (m), L is the length of the pipe (m), V is the mean velocity of the flow (m/s), g is the acceleration due to gravity (m/s²), D is the pipe diameter (m), and f is the Darcy-Weisbach friction factor.

The Swamee–Jain equation is used to solve for the Darcy-Weisbach friction factor f , and is presented in Equation 20 [34].

Equation 20

$$f = \frac{0.25}{[\text{Log}_{10}(\frac{\varepsilon}{3.7 * D} + \frac{5.74}{Re^{0.9}})]^2}$$

Where ε is the pipeline roughness (m), Re is the Reynolds number for fluid flow in a pipe (unitless), and D is the diameter of the pipe (m)

The Reynolds number (Re) for fluid flow in a pipe is defined as:

Equation 21

$$Re = \frac{Q * D_H}{A * v}$$

Wherein Q is the volumetric flowrate (m^3/s), D_H is the hydraulic diameter of the pipe (m), A is the pipe cross sectional area (m^2), and v is the kinematic viscosity (m^2/s).

The mean velocity of the flow (m/s) is expressed in Equation 22.

Equation 22

$$V = \frac{Q}{A}$$

Where A is the pipe cross sectional area (m^2), and Q is the volumetric flow rate (m^3/s).

The cross sectional area of a circular pipe is expressed in Equation 23

Equation 23

$$A = \pi * (\frac{D}{2})^2$$

Where D is the diameter of the pipe (m)

6.3. Centrifugation

After flocculation, algae are pumped to an industrial Centrifuge (CF) for dewatering. Decanter centrifuges were chosen as a means to concentrate the algae culture, as they are both a proven and reliable technology, and have the ability to significantly increase the concentration (% w/w) of the culture as compared to other centrifuge types. For centrifugation, the electrical consumption was evaluated at $8 \text{ kWh}/m^3$ consistent with centrifuges of this type[35]. Centrifugation was assumed to increase the algal concentration to 22% (w/w)[35]. In addition, it was assumed that 5% of the input culture would be lost during centrifugation, and that 90% of process medium would be recycled back into the ponds.

6.4. Chamber Filter Press

For Chamber Filter Presses (CFP), the electrical consumption per unit throughput was evaluated at 0.88 kWh/m³ [35]. It was assumed that the chamber filter press would increase the algal concentration to 25% (w/w)[35]. It was assumed that 5% of the input culture would be lost during dewatering, and that 90% of the process medium would be recycled back into the ponds. The energetic and environmental costs associated with replacing the filter press membranes were not considered in this study.

6.5. Algal Drying

After dewatering, algae must undergo additional drying to achieve a final concentration of 90% (w/w). Two production scenarios were examined for drying: (i) natural gas based drying and (ii) waste heat drying

6.5.1. Natural Gas based Drying

(i): Algae from dewatering process are sent to an industrial boiler in which natural gas is burned to dry the algae. The amount of heat energy needed to dry the algae was based on the amount of water extracted from the system, latent heat of evaporation of water, and boiler efficiency. The boiler efficiency was assumed to be 75%, and it was assumed that 5% of the input algal biomass would be lost in this process.

The energy (kJ) required for Natural Gas based Drying (NGD) is dependent on: m the mass of water needed to be extracted from the system (kg), C_w the latent heat of evaporation of water (kJ/kg), C_v the specific heat of water (kJ/kg-C), ΔT the change in temperature of the water (C), and boiler efficiency ϵ_{NG} (%), expressed in Equation 24.

Equation 24
$$Energy_{heat} = m * (C_w + C_v * \Delta T)$$

6.5.2. Waste Heat Drying

(ii): Studies have suggested that it may be possible to recover waste heat contained in the exhaust gases from power plants, and therefore utilize these exhaust streams to offset a portion of the energy required to dry the algal biomass[36]. Prior studies have estimated that a 500 MW power plant could generate up to $4.4 * 10^9$ MJ of “waste” heat energy per year[36], which greatly exceeds the heat energy required to dry the biomass. For Waste Heat Drying (WHD) scenarios it was assumed that all of the heat energy required to dry the biomass could be met using waste heat from a co-located power plant.

7. Life Cycle Inventory

The Life Cycle Inventory [LCI], normalized to 1 kg of biomass, for all production pathways are provided in the tables below. To avoid redundancy, the LCI of the following cultivation locations are provided: Mobile AL; Phoenix, AZ; San Diego, CA; Tallahassee, FL; Savannah, GA; Baton Rouge, LA; Brownsville, TX. In the following LCI tables these locations are referred to by state only. The sources of life cycle data are provided in the table below.

Table 18 – Sources of life cycle data

| Input | Life Cycle Database |
|--------------------|----------------------------|
| Aluminum Sulfate | Ecoinvent Database |
| PVC Liner | Ecoinvent Database |
| Wastewater | Ecoinvent Database |
| Urea | Ecoinvent Database |
| Superphosphate | Ecoinvent Database |
| Potassium Chloride | Ecoinvent Database |
| Electricity | USLCI Database |
| Natural Gas | USLCI Database |

Table S19 – LCI normalized per kg biomass for MEA/CF/NGD production pathway for select locations

| MEA/Centrifugation/Natural Gas Based Drying | | | | | | | | | | | | | | |
|---|---------------------------|------------------------------|--------------------------|--------|----------------|---------|--------|--------|--|----------------|----------------------------|---------------------------------|----------------|----------------------------|
| | Freshwater Requirement | Wastewater Treatment | CO ₂ Injected | PVC | Paddlewheels | Urea | SSP | KCL | Flocculation | MEA | | Pumping and Sourcing Freshwater | CF | NGD |
| State | m ³ Freshwater | m ³ Process Water | kg CO ₂ | kg PVC | MJ Electricity | kg Urea | kg SSP | kg KCL | Kg Al ₂ (SO ₄) ₃ | MJ Electricity | m ³ Natural gas | MJ Electricity | MJ Electricity | m ³ Natural Gas |
| AL | 0.42 | 0.36 | 3.00 | 0.03 | 0.37 | 0.26 | 0.10 | 0.04 | 0.25 | 0.35 | 0.50 | 1.34 | 1.56 | 0.38 |
| AZ | 0.72 | 0.33 | 3.00 | 0.02 | 0.28 | 0.26 | 0.10 | 0.04 | 0.25 | 0.35 | 0.50 | 2.42 | 1.56 | 0.38 |
| CA | 0.62 | 0.34 | 3.00 | 0.03 | 0.32 | 0.26 | 0.10 | 0.04 | 0.25 | 0.35 | 0.50 | 1.85 | 1.56 | 0.38 |
| FL | 0.39 | 0.35 | 3.00 | 0.03 | 0.35 | 0.26 | 0.10 | 0.04 | 0.25 | 0.35 | 0.50 | 1.61 | 1.56 | 0.38 |
| GA | 0.45 | 0.35 | 3.00 | 0.03 | 0.35 | 0.26 | 0.10 | 0.04 | 0.25 | 0.35 | 0.50 | 1.46 | 1.56 | 0.38 |
| LA | 0.43 | 0.36 | 3.00 | 0.03 | 0.36 | 0.26 | 0.10 | 0.04 | 0.25 | 0.35 | 0.50 | 1.77 | 1.56 | 0.38 |
| TX | 0.58 | 0.35 | 3.00 | 0.03 | 0.34 | 0.26 | 0.10 | 0.04 | 0.25 | 0.35 | 0.50 | 1.38 | 1.56 | 0.38 |

Table S20 – LCI normalized per kg biomass for MEA/CF/WHD production pathway for select locations

| MEA/Centrifugation/Waste Heat Drying | | | | | | | | | | | | | | |
|--------------------------------------|---------------------------|------------------------------|--------------------------|--------|----------------|---------|--------|--------|--|----------------|----------------------------|---------------------------------|----------------|----------------------------|
| | Freshwater Requirement | Wastewater Treatment | CO ₂ Injected | PVC | Paddlewheels | Urea | SSP | KCL | Flocculation | MEA | | Pumping and Sourcing Freshwater | CF | WHD |
| State | m ³ Freshwater | m ³ Process Water | kg CO ₂ | kg PVC | MJ Electricity | kg Urea | kg SSP | kg KCL | Kg Al ₂ (SO ₄) ₃ | MJ Electricity | m ³ Natural gas | MJ Electricity | MJ Electricity | m ³ Natural Gas |
| AL | 0.42 | 0.36 | 3.00 | 0.03 | 0.37 | 0.26 | 0.10 | 0.04 | 0.25 | 0.35 | 0.50 | 1.34 | 1.56 | 0 |
| AZ | 0.72 | 0.33 | 3.00 | 0.02 | 0.28 | 0.26 | 0.10 | 0.04 | 0.25 | 0.35 | 0.50 | 2.42 | 1.56 | 0 |
| CA | 0.62 | 0.34 | 3.00 | 0.03 | 0.32 | 0.26 | 0.10 | 0.04 | 0.25 | 0.35 | 0.50 | 1.85 | 1.56 | 0 |
| FL | 0.39 | 0.35 | 3.00 | 0.03 | 0.35 | 0.26 | 0.10 | 0.04 | 0.25 | 0.35 | 0.50 | 1.61 | 1.56 | 0 |
| GA | 0.45 | 0.35 | 3.00 | 0.03 | 0.35 | 0.26 | 0.10 | 0.04 | 0.25 | 0.35 | 0.50 | 1.46 | 1.56 | 0 |
| LA | 0.43 | 0.36 | 3.00 | 0.03 | 0.36 | 0.26 | 0.10 | 0.04 | 0.25 | 0.35 | 0.50 | 1.77 | 1.56 | 0 |
| TX | 0.58 | 0.35 | 3.00 | 0.03 | 0.34 | 0.26 | 0.10 | 0.04 | 0.25 | 0.35 | 0.50 | 1.38 | 1.56 | 0 |

Table S21 – LCI normalized per kg biomass for DI/CF/NGD production pathway for select locations

| Direct Injection/Centrifugation/Natural Gas Based Drying | | | | | | | | | | | | | |
|--|---------------------------|------------------------------|--------------------------|--------|----------------|---------|--------|--------|--|----------------|---------------------------------|----------------|----------------------------|
| | Freshwater Requirement | Wastewater Treatment | CO ₂ Injected | PVC | Paddlewheels | Urea | SSP | KCL | Flocculation | DI | Pumping and Sourcing Freshwater | CF | NGD |
| State | m ³ Freshwater | m ³ Process Water | kg CO ₂ | kg PVC | MJ Electricity | kg Urea | kg SSP | kg KCL | kg Al ₂ (SO ₄) ₃ | MJ Electricity | MJ Electricity | MJ Electricity | m ³ Natural Gas |
| AL | 0.42 | 0.36 | 3.00 | 0.03 | 0.37 | 0.26 | 0.10 | 0.04 | 0.25 | 0.24 | 1.34 | 1.56 | 0.38 |
| AZ | 0.72 | 0.33 | 3.00 | 0.02 | 0.28 | 0.26 | 0.10 | 0.04 | 0.25 | 0.24 | 2.42 | 1.56 | 0.38 |
| CA | 0.62 | 0.34 | 3.00 | 0.03 | 0.32 | 0.26 | 0.10 | 0.04 | 0.25 | 0.24 | 1.85 | 1.56 | 0.38 |
| FL | 0.39 | 0.35 | 3.00 | 0.03 | 0.35 | 0.26 | 0.10 | 0.04 | 0.25 | 0.24 | 1.61 | 1.56 | 0.38 |
| GA | 0.45 | 0.35 | 3.00 | 0.03 | 0.35 | 0.26 | 0.10 | 0.04 | 0.25 | 0.24 | 1.46 | 1.56 | 0.38 |
| LA | 0.43 | 0.36 | 3.00 | 0.03 | 0.36 | 0.26 | 0.10 | 0.04 | 0.25 | 0.24 | 1.77 | 1.56 | 0.38 |
| TX | 0.58 | 0.35 | 3.00 | 0.03 | 0.34 | 0.26 | 0.10 | 0.04 | 0.25 | 0.24 | 1.38 | 1.56 | 0.38 |

Table S22 – LCI normalized per kg biomass for DI/CF/WHD production pathway for select locations

| Direct Injection/Centrifugation/Waste Heat Drying | | | | | | | | | | | | | |
|---|---------------------------|------------------------------|--------------------------|--------|----------------|---------|--------|--------|--|----------------|---------------------------------|----------------|----------------------------|
| | Freshwater Requirement | Wastewater Treatment | CO ₂ Injected | PVC | Paddlewheels | Urea | SSP | KCL | Flocculation | DI | Pumping and Sourcing Freshwater | CF | WHD |
| State | m ³ Freshwater | m ³ Process Water | kg CO ₂ | kg PVC | MJ Electricity | kg Urea | kg SSP | kg KCL | kg Al ₂ (SO ₄) ₃ | MJ Electricity | MJ Electricity | MJ Electricity | m ³ Natural Gas |
| AL | 0.42 | 0.36 | 3.00 | 0.03 | 0.37 | 0.26 | 0.10 | 0.04 | 0.25 | 0.24 | 1.34 | 1.56 | 0 |
| AZ | 0.72 | 0.33 | 3.00 | 0.02 | 0.28 | 0.26 | 0.10 | 0.04 | 0.25 | 0.24 | 2.42 | 1.56 | 0 |
| CA | 0.62 | 0.34 | 3.00 | 0.03 | 0.32 | 0.26 | 0.10 | 0.04 | 0.25 | 0.24 | 1.85 | 1.56 | 0 |
| FL | 0.39 | 0.35 | 3.00 | 0.03 | 0.35 | 0.26 | 0.10 | 0.04 | 0.25 | 0.24 | 1.61 | 1.56 | 0 |
| GA | 0.45 | 0.35 | 3.00 | 0.03 | 0.35 | 0.26 | 0.10 | 0.04 | 0.25 | 0.24 | 1.46 | 1.56 | 0 |
| LA | 0.43 | 0.36 | 3.00 | 0.03 | 0.36 | 0.26 | 0.10 | 0.04 | 0.25 | 0.24 | 1.77 | 1.56 | 0 |
| TX | 0.58 | 0.35 | 3.00 | 0.03 | 0.34 | 0.26 | 0.10 | 0.04 | 0.25 | 0.24 | 1.38 | 1.56 | 0 |

Table S23 – LCI normalized per kg biomass for MEA/CFP/NGD production pathway for select locations

| MEA/Chamber Filter Press/Natural Gas Based Drying | | | | | | | | | | | | | | |
|---|---------------------------|------------------------------|--------------------------|--------|----------------|---------|--------|--------|--|----------------|----------------------------|---------------------------------|----------------|----------------------------|
| | Freshwater Requirement | Wastewater Treatment | CO ₂ Injected | PVC | Paddlewheels | Urea | SSP | KCL | Flocculation | MEA | | Pumping and Sourcing Freshwater | CFP | NGD |
| State | m ³ Freshwater | m ³ Process Water | kg CO ₂ | kg PVC | MJ Electricity | kg Urea | kg SSP | kg KCL | kg Al ₂ (SO ₄) ₃ | MJ Electricity | m ³ natural gas | MJ Electricity | MJ Electricity | m ³ Natural Gas |
| AL | 0.41 | 0.36 | 3.00 | 0.03 | 0.37 | 0.26 | 0.10 | 0.04 | 0.25 | 0.35 | 0.50 | 1.34 | 0.17 | 0.32 |
| AZ | 0.72 | 0.33 | 3.00 | 0.02 | 0.28 | 0.26 | 0.10 | 0.04 | 0.25 | 0.35 | 0.50 | 2.42 | 0.17 | 0.32 |
| CA | 0.61 | 0.34 | 3.00 | 0.03 | 0.32 | 0.26 | 0.10 | 0.04 | 0.25 | 0.35 | 0.50 | 1.85 | 0.17 | 0.32 |
| FL | 0.39 | 0.35 | 3.00 | 0.03 | 0.35 | 0.26 | 0.10 | 0.04 | 0.25 | 0.35 | 0.50 | 1.61 | 0.17 | 0.32 |
| GA | 0.45 | 0.35 | 3.00 | 0.03 | 0.35 | 0.26 | 0.10 | 0.04 | 0.25 | 0.35 | 0.50 | 1.46 | 0.17 | 0.32 |
| LA | 0.42 | 0.36 | 3.00 | 0.03 | 0.36 | 0.26 | 0.10 | 0.04 | 0.25 | 0.35 | 0.50 | 1.77 | 0.17 | 0.32 |
| TX | 0.57 | 0.35 | 3.00 | 0.03 | 0.34 | 0.26 | 0.10 | 0.04 | 0.25 | 0.35 | 0.50 | 1.38 | 0.17 | 0.32 |

Table S24 – LCI normalized per kg biomass for MEA/CFP/WHD production pathway for select locations

| MEA/Chamber Filter Press/Waste Heat Drying | | | | | | | | | | | | | | |
|--|---------------------------|------------------------------|--------------------------|--------|----------------|---------|--------|--------|--|----------------|----------------------------|---------------------------------|----------------|----------------------------|
| | Freshwater Requirement | Wastewater Treatment | CO ₂ Injected | PVC | Paddlewheels | Urea | SSP | KCL | Flocculation | MEA | | Pumping and Sourcing Freshwater | CFP | WHD |
| State | m ³ Freshwater | m ³ Process Water | kg CO ₂ | kg PVC | MJ Electricity | kg Urea | kg SSP | kg KCL | kg Al ₂ (SO ₄) ₃ | MJ Electricity | m ³ natural gas | MJ Electricity | MJ Electricity | m ³ Natural Gas |
| AL | 0.41 | 0.36 | 3.00 | 0.03 | 0.37 | 0.26 | 0.10 | 0.04 | 0.25 | 0.35 | 0.50 | 1.34 | 0.17 | 0 |
| AZ | 0.72 | 0.33 | 3.00 | 0.02 | 0.28 | 0.26 | 0.10 | 0.04 | 0.25 | 0.35 | 0.50 | 2.42 | 0.17 | 0 |
| CA | 0.61 | 0.34 | 3.00 | 0.03 | 0.32 | 0.26 | 0.10 | 0.04 | 0.25 | 0.35 | 0.50 | 1.85 | 0.17 | 0 |
| FL | 0.39 | 0.35 | 3.00 | 0.03 | 0.35 | 0.26 | 0.10 | 0.04 | 0.25 | 0.35 | 0.50 | 1.61 | 0.17 | 0 |
| GA | 0.45 | 0.35 | 3.00 | 0.03 | 0.35 | 0.26 | 0.10 | 0.04 | 0.25 | 0.35 | 0.50 | 1.46 | 0.17 | 0 |
| LA | 0.42 | 0.36 | 3.00 | 0.03 | 0.36 | 0.26 | 0.10 | 0.04 | 0.25 | 0.35 | 0.50 | 1.77 | 0.17 | 0 |
| TX | 0.57 | 0.35 | 3.00 | 0.03 | 0.34 | 0.26 | 0.10 | 0.04 | 0.25 | 0.35 | 0.50 | 1.38 | 0.17 | 0 |

Table S25 – LCI normalized per kg biomass for DI/CFP/NGD production pathway for select locations

| Direct Injection/Chamber Filter Press/Natural Gas Based Drying | | | | | | | | | | | | | |
|--|---------------------------|------------------------------|--------------------------|--------|----------------|---------|--------|--------|--|----------------|---------------------------------|----------------|----------------------------|
| | Freshwater Requirement | Wastewater Treatment | CO ₂ Injected | PVC | Paddlewheels | Urea | SSP | KCL | Flocculation | DI | Pumping and Sourcing Freshwater | CFP | NGD |
| State | m ³ Freshwater | m ³ Process Water | kg CO ₂ | kg PVC | MJ Electricity | kg Urea | kg SSP | kg KCL | kg Al ₂ (SO ₄) ₃ | MJ Electricity | MJ Electricity | MJ Electricity | m ³ Natural Gas |
| AL | 0.41 | 0.36 | 3.00 | 0.03 | 0.37 | 0.26 | 0.10 | 0.04 | 0.25 | 0.24 | 1.34 | 0.17 | 0.32 |
| AZ | 0.72 | 0.33 | 3.00 | 0.02 | 0.28 | 0.26 | 0.10 | 0.04 | 0.25 | 0.24 | 2.42 | 0.17 | 0.32 |
| CA | 0.61 | 0.34 | 3.00 | 0.03 | 0.32 | 0.26 | 0.10 | 0.04 | 0.25 | 0.24 | 1.85 | 0.17 | 0.32 |
| FL | 0.39 | 0.35 | 3.00 | 0.03 | 0.35 | 0.26 | 0.10 | 0.04 | 0.25 | 0.24 | 1.61 | 0.17 | 0.32 |
| GA | 0.45 | 0.35 | 3.00 | 0.03 | 0.35 | 0.26 | 0.10 | 0.04 | 0.25 | 0.24 | 1.46 | 0.17 | 0.32 |
| LA | 0.42 | 0.36 | 3.00 | 0.03 | 0.36 | 0.26 | 0.10 | 0.04 | 0.25 | 0.24 | 1.77 | 0.17 | 0.32 |
| TX | 0.57 | 0.35 | 3.00 | 0.03 | 0.34 | 0.26 | 0.10 | 0.04 | 0.25 | 0.24 | 1.38 | 0.17 | 0.32 |

Table S26– LCI normalized per kg biomass for DI/CFP/WHD production pathway for select locations

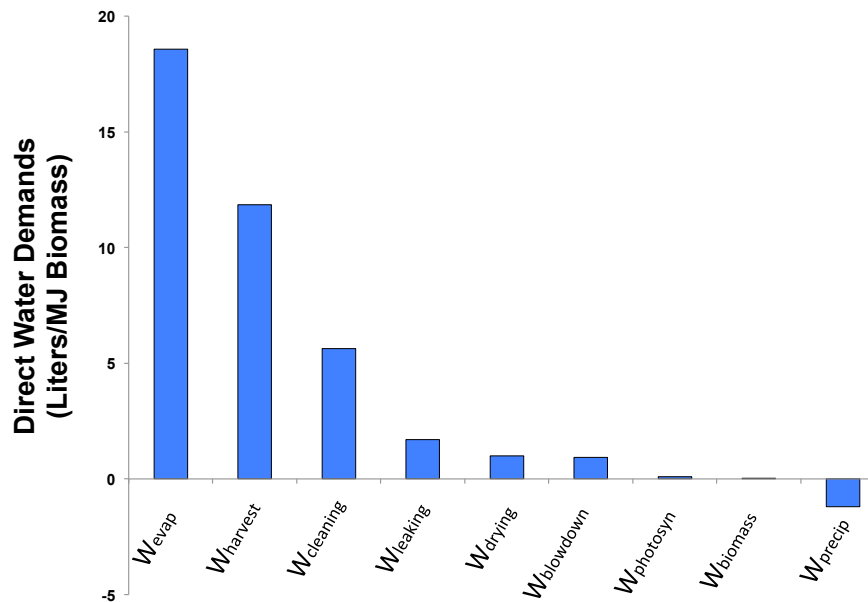
| Direct Injection/Chamber Filter Press/Waste Heat Drying | | | | | | | | | | | | | |
|---|---------------------------|------------------------------|--------------------------|--------|----------------|---------|--------|--------|--|----------------|---------------------------------|----------------|----------------------------|
| | Freshwater Requirement | Wastewater Treatment | CO ₂ Injected | PVC | Paddlewheels | Urea | SSP | KCL | Flocculation | DI | Pumping and Sourcing Freshwater | CFP | WHD |
| State | m ³ Freshwater | m ³ Process Water | kg CO ₂ | kg PVC | MJ Electricity | kg Urea | kg SSP | kg KCL | kg Al ₂ (SO ₄) ₃ | MJ Electricity | MJ Electricity | MJ Electricity | m ³ Natural Gas |
| AL | 0.41 | 0.36 | 3.00 | 0.03 | 0.37 | 0.26 | 0.10 | 0.04 | 0.25 | 0.24 | 1.34 | 0.17 | 0 |
| AZ | 0.72 | 0.33 | 3.00 | 0.02 | 0.28 | 0.26 | 0.10 | 0.04 | 0.25 | 0.24 | 2.42 | 0.17 | 0 |
| CA | 0.61 | 0.34 | 3.00 | 0.03 | 0.32 | 0.26 | 0.10 | 0.04 | 0.25 | 0.24 | 1.85 | 0.17 | 0 |
| FL | 0.39 | 0.35 | 3.00 | 0.03 | 0.35 | 0.26 | 0.10 | 0.04 | 0.25 | 0.24 | 1.61 | 0.17 | 0 |
| GA | 0.45 | 0.35 | 3.00 | 0.03 | 0.35 | 0.26 | 0.10 | 0.04 | 0.25 | 0.24 | 1.46 | 0.17 | 0 |
| LA | 0.42 | 0.36 | 3.00 | 0.03 | 0.36 | 0.26 | 0.10 | 0.04 | 0.25 | 0.24 | 1.77 | 0.17 | 0 |
| TX | 0.57 | 0.35 | 3.00 | 0.03 | 0.34 | 0.26 | 0.10 | 0.04 | 0.25 | 0.24 | 1.38 | 0.17 | 0 |

8. Direct Water Demands

The direct WDs for biomass production were calculated as the difference between the amount of make-up water required due to evaporation (W_{evap}), pond cleaning ($W_{cleaning}$), pond leaking ($W_{leaking}$), blowdown ($W_{blowdown}$), photosynthesis ($W_{photosyn}$), harvesting ($W_{harvest}$), algal drying (W_{drying}), water stored in the biomass that is transported offsite ($W_{biomass}$), and annual precipitation (W_{precip}), defined in Equation 25. A breakdown of the direct water demands for Chamber filter press based pathways for Phoenix, Arizona are provided in Figure 2.

$$\text{Equation 25 } \textit{Direct WD} = W_{evap} + W_{cleaning} + W_{leaking} + W_{blowdown} + W_{photosyn} + W_{harvest} + W_{drying} + W_{biomass} - W_{precip}$$

Figure 2 – Direct Water Demands for CFP Pathways for Phoenix, Arizona



9. Allocation

In this study the energetic and environmental impacts of obtaining pure CO₂ via MEA scrubbing are allocated between the algae cultivation facility and Natural Gas (NG) fired power plants on an energy basis. The allocation scheme is as follows: for every X MJ of electricity produced at a NG fired power plant, Y kg of CO₂ are emitted which in turn produces Z MJ of algal biomass. The percentage of environmental and energetic impacts that are allocated to algal cultivation is equal to $\frac{Z}{(Z+X)}$. To estimate the amount of CO₂ produced per MJ of electricity at a Natural Gas power plant, emissions data for over 450 NG fired power plants were acquired from the eGRID database. Analysis of this data indicates that on average NG fired power plant produce approximately 470 kg of CO₂ per MWh of electricity. Under this assumption, 44.8% of the environmental impacts due to MEA are allocated to algae cultivation. Additionally, unallocated values for EROI_{fossil} and life cycle GHG emissions are provided in summary tables in section 10.

10. Summary Tables

The following tables provide the direct WDs, $EROI_{fossil}$, and life cycle GHG emissions for biomass production with and without allocation.

Table S27 - Allocated $EROI_{fossil}$, net life cycle GHG emissions, and direct WDs for examined biomass production pathways & locations

| Parameters | | Cultivation and Harvesting Scenarios (Allocated) | | | | | | | | WD ¹ | |
|------------|-----------------|--|-------------|-------------|-------------|--------------|--------------|--------------|--------------|-----------------|------|
| State | City | MEA/CF/NGD | MEA/CFP/NGD | DI/CF/NGD | DI/CFP/NGD | MEA/CF/WHD | MEA/CFP/WHD | DI/CF/WHD | DI/CFP/WHD | CFP | CF |
| AL | Mobile | 0.40 (44.2) | 0.46 (22.5) | 0.49 (18.9) | 0.59 (-2.8) | 0.60 (-0.4) | 0.68 (-15.1) | 0.86 (-25.7) | 1.04 (-40.4) | 22.1 | 22.3 |
| AZ | Phoenix | 0.38 (48.9) | 0.43 (28.4) | 0.47 (23.5) | 0.56 (3.0) | 0.57 (4.2) | 0.64 (-9.2) | 0.79 (-21.2) | 0.94 (-34.6) | 38.6 | 38.8 |
| CA | San Diego | 0.41 (32.0) | 0.46 (16.0) | 0.51 (6.3) | 0.60 (-9.6) | 0.63 (-12.6) | 0.69 (-21.5) | 0.91 (-38.3) | 1.06 (-47.2) | 32.8 | 33.0 |
| FL | Daytona Beach | 0.38 (43.0) | 0.44 (22.7) | 0.47 (17.5) | 0.57 (-2.7) | 0.58 (-1.6) | 0.66 (-14.8) | 0.81 (-27.1) | 0.97 (-40.2) | 24.1 | 24.3 |
| FL | Jacksonville | 0.38 (43.1) | 0.44 (22.8) | 0.47 (17.7) | 0.57 (-2.6) | 0.58 (-1.5) | 0.66 (-14.7) | 0.81 (-27.0) | 0.97 (-40.1) | 22.6 | 22.9 |
| FL | Key West | 0.38 (43.6) | 0.44 (23.4) | 0.47 (18.2) | 0.57 (-2.1) | 0.57 (-1.0) | 0.65 (-14.2) | 0.80 (-26.4) | 0.97 (-39.6) | 28.4 | 28.6 |
| FL | Miami | 0.38 (42.7) | 0.44 (22.5) | 0.48 (17.3) | 0.57 (-3.0) | 0.58 (-1.9) | 0.66 (-15.1) | 0.81 (-27.3) | 0.98 (-40.5) | 22.1 | 22.4 |
| FL | Tallahassee | 0.39 (42.4) | 0.44 (22.2) | 0.48 (17.0) | 0.57 (-3.2) | 0.58 (-2.2) | 0.66 (-15.4) | 0.82 (-27.6) | 0.98 (-40.8) | 20.8 | 21.1 |
| FL | Tampa | 0.38 (43.2) | 0.44 (23.0) | 0.47 (17.8) | 0.57 (-2.5) | 0.58 (-1.4) | 0.65 (-14.6) | 0.81 (-26.8) | 0.97 (-40.0) | 25.1 | 25.4 |
| FL | West Palm Beach | 0.38 (43.0) | 0.44 (22.7) | 0.47 (17.6) | 0.57 (-2.7) | 0.58 (-1.6) | 0.66 (-14.8) | 0.81 (-27.0) | 0.97 (-40.2) | 22.9 | 23.1 |
| GA | Savannah | 0.39 (45.0) | 0.45 (23.2) | 0.49 (19.7) | 0.59 (-2.1) | 0.60 (0.4) | 0.68 (-14.3) | 0.86 (-24.9) | 1.03 (-39.6) | 24.1 | 24.4 |
| LA | Baton Rouge | 0.39 (39.2) | 0.45 (20.8) | 0.49 (13.6) | 0.58 (-4.7) | 0.60 (-5.4) | 0.67 (-16.8) | 0.86 (-31.0) | 1.01 (-42.3) | 22.6 | 22.8 |
| LA | Lake Charles | 0.39 (39.0) | 0.45 (20.6) | 0.49 (13.5) | 0.58 (-4.9) | 0.60 (-5.6) | 0.67 (-16.9) | 0.86 (-31.1) | 1.02 (-42.4) | 23.0 | 23.2 |
| LA | New Orleans | 0.40 (38.9) | 0.45 (20.5) | 0.49 (13.4) | 0.58 (-5.0) | 0.60 (-5.7) | 0.67 (-17.0) | 0.86 (-31.2) | 1.02 (-42.5) | 22.1 | 22.3 |
| TX | Austin | 0.39 (41.5) | 0.45 (20.6) | 0.49 (16.1) | 0.59 (-4.8) | 0.59 (-3.1) | 0.68 (-16.9) | 0.85 (-28.5) | 1.03 (-42.3) | 29.8 | 30.0 |
| TX | Brownsville | 0.39 (41.8) | 0.45 (20.9) | 0.49 (16.4) | 0.58 (-4.5) | 0.59 (-2.8) | 0.68 (-16.6) | 0.84 (-28.2) | 1.02 (-42.0) | 30.6 | 30.8 |
| TX | Corpus Christi | 0.39 (42.1) | 0.45 (21.3) | 0.48 (16.8) | 0.58 (-4.1) | 0.59 (-2.5) | 0.67 (-16.3) | 0.84 (-27.8) | 1.02 (-41.7) | 29.7 | 29.9 |
| TX | Houston | 0.39 (42.0) | 0.45 (21.1) | 0.49 (16.7) | 0.58 (-4.2) | 0.59 (-2.6) | 0.67 (-16.4) | 0.84 (-27.9) | 1.02 (-41.8) | 25.6 | 25.8 |
| TX | Lufkin | 0.39 (41.5) | 0.45 (20.6) | 0.49 (16.1) | 0.59 (-4.8) | 0.59 (-3.1) | 0.68 (-16.9) | 0.85 (-28.5) | 1.03 (-42.3) | 26.1 | 26.3 |
| TX | Port Arthur | 0.40 (35.2) | 0.46 (16.9) | 0.51 (9.7) | 0.60 (-8.6) | 0.62 (-9.4) | 0.70 (-20.6) | 0.91 (-34.9) | 1.08 (-46.2) | 22.8 | 23.0 |
| TX | San Antonio | 0.39 (41.3) | 0.45 (20.4) | 0.49 (16.0) | 0.59 (-4.9) | 0.60 (-3.3) | 0.68 (-17.1) | 0.85 (-28.6) | 1.03 (-42.5) | 29.9 | 30.1 |
| TX | Victoria | 0.39 (41.9) | 0.45 (21.0) | 0.49 (16.5) | 0.58 (-4.4) | 0.59 (-2.7) | 0.68 (-16.5) | 0.84 (-28.1) | 1.02 (-41.9) | 27.4 | 27.7 |

Table S28 - Unallocated EROI_{fossil}, net life cycle GHG emissions, and direct WDs for examined biomass production pathways & locations

| Parameters | | Cultivation and Harvesting Scenarios (Unallocated) | | | | | | | | WD ¹ | |
|------------|-----------------|--|-------------|-------------|-------------|-------------|-------------|--------------|--------------|-----------------|------|
| State | City | MEA/CF/NGD | MEA/CF/NGD | MEA/CF/WHD | MEA/CF/WHD | DI/CF/NGD | DI/CF/NGD | DI/CF/WHD | DI/CF/WHD | CFP | CF |
| AL | Mobile | 0.31 (78.6) | 0.35 (56.8) | 0.43 (33.9) | 0.47 (19.2) | 0.49 (18.9) | 0.59 (-2.8) | 0.86 (-25.7) | 1.04 (-40.4) | 22.1 | 22.3 |
| AZ | Phoenix | 0.30 (83.0) | 0.34 (62.5) | 0.41 (38.4) | 0.45 (25.0) | 0.47 (23.5) | 0.56 (3.0) | 0.79 (-21.2) | 0.94 (-34.6) | 38.6 | 38.8 |
| CA | San Diego | 0.32 (65.5) | 0.35 (49.5) | 0.44 (20.9) | 0.48 (12.0) | 0.51 (6.3) | 0.60 (-9.6) | 0.91 (-38.3) | 1.06 (-47.2) | 32.8 | 33.0 |
| FL | Daytona Beach | 0.31 (77.1) | 0.34 (56.8) | 0.42 (32.4) | 0.46 (19.3) | 0.47 (17.5) | 0.57 (-2.7) | 0.81 (-27.1) | 0.97 (-40.2) | 24.1 | 24.3 |
| FL | Jacksonville | 0.31 (77.2) | 0.34 (56.9) | 0.42 (32.6) | 0.46 (19.4) | 0.47 (17.7) | 0.57 (-2.6) | 0.81 (-27.0) | 0.97 (-40.1) | 22.6 | 22.9 |
| FL | Key West | 0.31 (77.7) | 0.34 (57.5) | 0.42 (33.1) | 0.46 (19.9) | 0.47 (18.2) | 0.57 (-2.1) | 0.80 (-26.4) | 0.97 (-39.6) | 28.4 | 28.6 |
| FL | Miami | 0.31 (76.8) | 0.34 (56.6) | 0.42 (32.2) | 0.46 (19.0) | 0.48 (17.3) | 0.57 (-3.0) | 0.81 (-27.3) | 0.98 (-40.5) | 22.1 | 22.4 |
| FL | Tallahassee | 0.31 (76.5) | 0.34 (56.3) | 0.42 (31.9) | 0.46 (18.7) | 0.48 (17.0) | 0.57 (-3.2) | 0.82 (-27.6) | 0.98 (-40.8) | 20.8 | 21.1 |
| FL | Tampa | 0.31 (77.3) | 0.34 (57.1) | 0.42 (32.7) | 0.46 (19.5) | 0.47 (17.8) | 0.57 (-2.5) | 0.81 (-26.8) | 0.97 (-40.0) | 25.1 | 25.4 |
| FL | West Palm Beach | 0.31 (77.1) | 0.34 (56.8) | 0.42 (32.5) | 0.46 (19.3) | 0.47 (17.6) | 0.57 (-2.7) | 0.81 (-27.0) | 0.97 (-40.2) | 22.9 | 23.1 |
| GA | Savannah | 0.31 (79.3) | 0.35 (57.5) | 0.43 (34.7) | 0.47 (20.0) | 0.49 (19.7) | 0.59 (-2.1) | 0.86 (-24.9) | 1.03 (-39.6) | 24.1 | 24.4 |
| LA | Baton Rouge | 0.31 (73.0) | 0.35 (54.6) | 0.43 (28.4) | 0.47 (17.1) | 0.49 (13.6) | 0.58 (-4.7) | 0.86 (-31.0) | 1.01 (-42.3) | 22.6 | 22.8 |
| LA | Lake Charles | 0.31 (72.8) | 0.35 (54.5) | 0.43 (28.2) | 0.47 (16.9) | 0.49 (13.5) | 0.58 (-4.9) | 0.86 (-31.1) | 1.02 (-42.4) | 23.0 | 23.2 |
| LA | New Orleans | 0.31 (72.7) | 0.35 (54.4) | 0.43 (28.1) | 0.47 (16.8) | 0.49 (13.4) | 0.58 (-5.0) | 0.86 (-31.2) | 1.02 (-42.5) | 22.1 | 22.3 |
| TX | Austin | 0.31 (75.7) | 0.35 (54.8) | 0.43 (31.1) | 0.47 (17.3) | 0.49 (16.1) | 0.59 (-4.8) | 0.85 (-28.5) | 1.03 (-42.3) | 29.8 | 30.0 |
| TX | Brownsville | 0.31 (76.0) | 0.35 (55.1) | 0.43 (31.4) | 0.47 (17.6) | 0.49 (16.4) | 0.58 (-4.5) | 0.84 (-28.2) | 1.02 (-42.0) | 30.6 | 30.8 |
| TX | Corpus Christi | 0.31 (76.3) | 0.35 (55.5) | 0.43 (31.7) | 0.47 (17.9) | 0.48 (16.8) | 0.58 (-4.1) | 0.84 (-27.8) | 1.02 (-41.7) | 29.7 | 29.9 |
| TX | Houston | 0.31 (76.2) | 0.35 (55.3) | 0.43 (31.6) | 0.47 (17.8) | 0.49 (16.7) | 0.58 (-4.2) | 0.84 (-27.9) | 1.02 (-41.8) | 25.6 | 25.8 |
| TX | Lufkin | 0.31 (75.7) | 0.35 (54.8) | 0.43 (31.1) | 0.47 (17.3) | 0.49 (16.1) | 0.59 (-4.8) | 0.85 (-28.5) | 1.03 (-42.3) | 26.1 | 26.3 |
| TX | Port Arthur | 0.32 (69.1) | 0.36 (50.7) | 0.44 (24.5) | 0.48 (13.2) | 0.51 (9.7) | 0.60 (-8.6) | 0.91 (-34.9) | 1.08 (-46.2) | 22.8 | 23.0 |
| TX | San Antonio | 0.31 (75.7) | 0.35 (54.6) | 0.43 (30.9) | 0.47 (17.1) | 0.49 (16.0) | 0.59 (-4.9) | 0.85 (-28.6) | 1.03 (-42.5) | 29.9 | 30.1 |
| TX | Victoria | 0.31 (76.1) | 0.35 (55.2) | 0.43 (31.5) | 0.47 (17.6) | 0.49 (16.5) | 0.58 (-4.4) | 0.84 (-28.1) | 1.02 (-41.9) | 27.4 | 27.7 |

* The results are presented in the following format: EROI_{fossil} (Net Life Cycle GHG Emissions) where Net life cycle GHG emissions are in units of (g CO₂ eq/MJ-Biomass)

¹ The results for the WD are presented in units of (liters/MJ-biomass)

11. Additional Scenarios

11.1. Low Nitrogen Scenario

Previous studies have suggested that cultivating algae in low-nitrogen conditions can substantially increase the lipid content of the biomass[37-39]. However, nitrogen deprivation may have adverse effects on the algae culture, and additional experimental data is required to validate the feasibility of this approach. A low-nitrogen scenario was considered in this analysis, the fractionalized composition of algae under nitrogen deprivation, taken from Lardon et al. 2009, was evaluated at 38.5% lipids, 52.9% carbohydrates, and 6.7% proteins[40]. The following tables provide the $EROI_{\text{fossil}}$ and life cycle GHG emissions for biomass production for the low-nitrogen scenario (with and without allocation).

Table S29 – Low Nitrogen Scenario: Allocated EROI_{fossil} & net life cycle GHG emissions for examined biomass production pathways & locations

| Parameters | | Cultivation and Harvesting Scenarios (Allocated) | | | | | | | |
|------------|-----------------|--|-------------|--------------|--------------|--------------|--------------|--------------|--------------|
| State | City | MEA/CF/NGD | MEA/CF/NGD | DI/CF/NGD | DI/CF/NGD | MEA/CF/WHD | MEA/CF/WHD | DI/CF/WHD | DI/CF/WHD |
| AL | Mobile | 0.54 (22.8) | 0.63 (4.8) | 0.72 (-1.6) | 0.90 (-19.5) | 0.87 (-14.0) | 1.02 (-26.1) | 1.50 (-38.3) | 1.97 (-50.4) |
| AZ | Phoenix | 0.51 (27.3) | 0.59 (10.5) | 0.68 (3.0) | 0.83 (-13.9) | 0.81 (-9.4) | 0.92 (-20.4) | 1.31 (-33.8) | 1.65 (-44.8) |
| CA | San Diego | 0.55 (12.4) | 0.64 (-0.7) | 0.75 (-12.1) | 0.92 (-25.2) | 0.91 (-24.3) | 1.03 (-31.6) | 1.62 (-48.8) | 2.04 (-56.1) |
| FL | Daytona Beach | 0.52 (21.8) | 0.61 (5.1) | 0.69 (-2.6) | 0.86 (-19.3) | 0.83 (-15.0) | 0.96 (-25.8) | 1.36 (-39.3) | 1.78 (-50.2) |
| FL | Jacksonville | 0.52 (21.9) | 0.61 (5.2) | 0.69 (-2.5) | 0.86 (-19.2) | 0.82 (-14.9) | 0.96 (-25.7) | 1.36 (-39.2) | 1.77 (-50.1) |
| FL | Key West | 0.52 (22.4) | 0.60 (5.7) | 0.68 (-2.0) | 0.85 (-18.6) | 0.82 (-14.3) | 0.95 (-25.2) | 1.34 (-38.7) | 1.75 (-49.6) |
| FL | Miami | 0.52 (21.5) | 0.61 (4.8) | 0.69 (-2.9) | 0.86 (-19.5) | 0.83 (-15.2) | 0.97 (-26.1) | 1.37 (-39.6) | 1.79 (-50.4) |
| FL | Tallahassee | 0.52 (21.2) | 0.61 (4.6) | 0.69 (-3.1) | 0.86 (-19.8) | 0.83 (-15.5) | 0.97 (-26.4) | 1.38 (-39.9) | 1.81 (-50.7) |
| FL | Tampa | 0.52 (22.0) | 0.61 (5.3) | 0.69 (-2.4) | 0.86 (-19.0) | 0.82 (-14.7) | 0.96 (-25.6) | 1.35 (-39.1) | 1.77 (-50.0) |
| FL | West Palm Beach | 0.52 (21.8) | 0.61 (5.1) | 0.69 (-2.6) | 0.86 (-19.3) | 0.82 (-14.9) | 0.96 (-25.8) | 1.36 (-39.3) | 1.78 (-50.2) |
| GA | Savannah | 0.53 (23.4) | 0.63 (5.5) | 0.72 (-0.9) | 0.89 (-18.8) | 0.87 (-13.3) | 1.01 (-25.4) | 1.48 (-37.6) | 1.94 (-49.7) |
| LA | Baton Rouge | 0.53 (18.6) | 0.62 (3.5) | 0.72 (-5.8) | 0.88 (-21.0) | 0.87 (-18.1) | 0.99 (-27.5) | 1.48 (-42.6) | 1.89 (-51.9) |
| LA | Lake Charles | 0.54 (18.4) | 0.62 (3.3) | 0.72 (-6.0) | 0.88 (-21.1) | 0.87 (-18.3) | 0.99 (-27.6) | 1.49 (-42.7) | 1.90 (-52.1) |
| LA | New Orleans | 0.54 (18.3) | 0.62 (3.2) | 0.72 (-6.1) | 0.89 (-21.3) | 0.87 (-18.4) | 1.00 (-27.7) | 1.49 (-42.8) | 1.90 (-52.2) |
| TX | Austin | 0.53 (20.4) | 0.63 (3.2) | 0.71 (-4.0) | 0.89 (-21.2) | 0.86 (-16.3) | 1.01 (-27.7) | 1.46 (-40.7) | 1.94 (-52.1) |
| TX | Brownsville | 0.53 (20.7) | 0.62 (3.5) | 0.71 (-3.7) | 0.89 (-20.9) | 0.86 (-16.1) | 1.00 (-27.4) | 1.45 (-40.4) | 1.92 (-51.8) |
| TX | Corpus Christi | 0.53 (21.0) | 0.62 (3.8) | 0.71 (-3.3) | 0.89 (-20.5) | 0.85 (-15.7) | 1.00 (-27.1) | 1.44 (-40.1) | 1.90 (-51.4) |
| TX | Houston | 0.53 (20.9) | 0.62 (3.7) | 0.71 (-3.4) | 0.89 (-20.6) | 0.85 (-15.8) | 1.00 (-27.2) | 1.44 (-40.2) | 1.91 (-51.6) |
| TX | Lufkin | 0.53 (20.4) | 0.63 (3.2) | 0.71 (-4.0) | 0.89 (-21.2) | 0.86 (-16.4) | 1.01 (-27.8) | 1.46 (-40.7) | 1.94 (-52.1) |
| TX | Port Arthur | 0.55 (15.0) | 0.64 (-0.1) | 0.75 (-9.4) | 0.93 (-24.5) | 0.91 (-21.7) | 1.05 (-31.0) | 1.62 (-46.1) | 2.11 (-55.4) |
| TX | San Antonio | 0.53 (20.2) | 0.63 (3.0) | 0.71 (-4.1) | 0.90 (-21.3) | 0.86 (-16.5) | 1.01 (-27.9) | 1.46 (-40.9) | 1.95 (-52.3) |
| TX | Victoria | 0.53 (20.7) | 0.62 (3.5) | 0.71 (-3.6) | 0.89 (-20.8) | 0.85 (-16.0) | 1.00 (-27.4) | 1.44 (-40.3) | 1.92 (-51.7) |

Table S30 - Low Nitrogen Scenario: Unlocated EROI_{fossil} & net life cycle GHG emissions for examined biomass production pathways & locations

| Parameters | | Cultivation and Harvesting Scenarios (Unallocated) | | | | | | | |
|------------|-----------------|--|-------------|-------------|-------------|--------------|--------------|--------------|--------------|
| State | City | MEA/CF/NGD | MEA/CF/NGD | MEA/CF/WHD | MEA/CF/WHD | DI/CF/NGD | DI/CF/NGD | DI/CF/WHD | DI/CF/WHD |
| AL | Mobile | 0.42 (49.6) | 0.48 (31.7) | 0.60 (12.9) | 0.67 (0.8) | 0.72 (-1.6) | 0.90 (-19.5) | 1.50 (-38.3) | 1.97 (-50.4) |
| AZ | Phoenix | 0.40 (54.0) | 0.45 (37.2) | 0.57 (17.3) | 0.63 (6.3) | 0.68 (2.9) | 0.83 (-13.9) | 1.31 (-33.8) | 1.65 (-44.8) |
| CA | San Diego | 0.43 (38.6) | 0.48 (25.5) | 0.62 (1.9) | 0.68 (-5.4) | 0.75 (-12.1) | 0.92 (-25.2) | 1.62 (-48.8) | 2.04 (-56.1) |
| FL | Daytona Beach | 0.41 (48.4) | 0.46 (31.8) | 0.58 (11.7) | 0.64 (0.9) | 0.69 (-2.7) | 0.86 (-19.3) | 1.36 (-39.3) | 1.78 (-50.2) |
| FL | Jacksonville | 0.41 (48.5) | 0.46 (31.9) | 0.58 (11.8) | 0.64 (1.0) | 0.69 (-2.5) | 0.86 (-19.2) | 1.36 (-39.2) | 1.77 (-50.1) |
| FL | Key West | 0.41 (49.1) | 0.46 (32.4) | 0.58 (12.4) | 0.64 (1.5) | 0.68 (-2.0) | 0.85 (-18.6) | 1.34 (-38.7) | 1.75 (-49.6) |
| FL | Miami | 0.41 (48.2) | 0.46 (31.5) | 0.58 (11.5) | 0.64 (0.6) | 0.69 (-2.9) | 0.86 (-19.5) | 1.37 (-39.6) | 1.79 (-50.4) |
| FL | Tallahassee | 0.41 (47.9) | 0.46 (31.2) | 0.58 (11.2) | 0.65 (0.3) | 0.69 (-3.2) | 0.86 (-19.8) | 1.38 (-39.9) | 1.81 (-50.7) |
| FL | Tampa | 0.41 (48.7) | 0.46 (32.0) | 0.58 (12.0) | 0.64 (1.1) | 0.69 (-2.4) | 0.86 (-19.0) | 1.35 (-39.1) | 1.77 (-50.0) |
| FL | West Palm Beach | 0.41 (48.4) | 0.46 (31.8) | 0.58 (11.7) | 0.64 (0.9) | 0.69 (-2.6) | 0.86 (-19.3) | 1.36 (-39.3) | 1.78 (-50.2) |
| GA | Savannah | 0.42 (50.2) | 0.47 (32.3) | 0.60 (13.5) | 0.66 (1.4) | 0.72 (-0.9) | 0.89 (-18.8) | 1.48 (-37.6) | 1.94(-49.7) |
| LA | Baton Rouge | 0.42 (45.0) | 0.47 (29.9) | 0.60 (8.4) | 0.66 (-1.0) | 0.72 (-5.9) | 0.88 (-21.0) | 1.48 (-42.6) | 1.89 (-51.9) |
| LA | Lake Charles | 0.42 (44.9) | 0.47 (29.8) | 0.60 (8.2) | 0.66 (-1.1) | 0.72 (-6.0) | 0.88 (-21.1) | 1.49 (-42.7) | 1.90 (-52.1) |
| LA | New Orleans | 0.42 (44.8) | 0.47 (29.7) | 0.60 (8.1) | 0.66 (-1.2) | 0.72 (-6.1) | 0.89 (-21.3) | 1.49 (-42.8) | 1.90 (-52.2) |
| TX | Austin | 0.42 (47.1) | 0.47 (29.9) | 0.60 (10.4) | 0.66 (-1.0) | 0.71 (-4.0) | 0.89 (-21.2) | 1.46 (-40.7) | 1.94 (-52.1) |
| TX | Brownsville | 0.42 (47.4) | 0.47 (30.2) | 0.59 (10.7) | 0.66 (-0.7) | 0.71 (-3.7) | 0.89 (-20.9) | 1.45 (-40.4) | 1.92 (-51.8) |
| TX | Corpus Christi | 0.42 (47.7) | 0.47 (30.6) | 0.59 (11.1) | 0.66 (-0.3) | 0.71 (-3.4) | 0.89 (-20.5) | 1.44 (-40.1) | 1.90 (-51.4) |
| TX | Houston | 0.42 (47.6) | 0.47 (30.5) | 0.59 (10.9) | 0.66 (-0.4) | 0.71 (-3.5) | 0.89 (-20.6) | 1.44 (-40.2) | 1.91 (-51.6) |
| TX | Lufkin | 0.42 (47.1) | 0.47 (29.9) | 0.60 (10.4) | 0.66 (-1.0) | 0.71 (-4.0) | 0.89 (-21.2) | 1.46 (-40.7) | 1.94 (-52.1) |
| TX | Port Arthur | 0.43 (41.5) | 0.48 (26.4) | 0.62 (4.8) | 0.68 (-4.5) | 0.75 (-9.5) | 0.93 (-24.5) | 1.62 (-46.1) | 2.11 (-55.4) |
| TX | San Antonio | 0.42 (46.9) | 0.47 (29.8) | 0.60 (10.2) | 0.66 (-1.1) | 0.71 (-4.2) | 0.90 (-21.3) | 1.46 (-40.9) | 1.95 (-52.3) |
| TX | Victoria | 0.42 (47.5) | 0.47 (30.3) | 0.59 (10.8) | 0.66 (-0.6) | 0.71 (-3.6) | 0.89 (-20.8) | 1.44 (-40.3) | 1.92 (-51.7) |

* The results are presented in the following format: EROI_{fossil} (Net Life Cycle GHG Emissions) where Net life cycle GHG emissions are in units of (g CO₂ eq/MJ-Biomass)

11.2. Alternative Production Scenario

An alternate technological route was considered in this work. This production pathway assumes that algae undergo auto-flocculation (AF) to concentrate the biomass to .25% (w/w) [41]. Recent studies have suggested that cross flow filtration (CFF) is a low-energy intensive technology that can be used to dewater the algae culture, and has many advantages over conventional centrifugation, pressure filtration, and dissolved air and/or froth flotation[42]. Therefore, post auto-flocculation biomass is then sent to a cross-flow filtration unit for further dewatering to 16% (w/w); the electrical consumption for cross flow filtration was evaluated at .5 kWh/m³ [42]. A chamber filter press (CFP) is then used to further concentrate the algae to 25% (w/w), and both natural gas (NG) and waste heat (WHD) are evaluated as processing options for drying the biomass to 90% (w/w). This technological route may be favorable, as it does not rely on a coagulant for biomass production and uses low-energy dewatering strategies. The results are presented in Tables S31 and Table S32.

Table S31 – Alternate Biomass Production Scenario: Allocated EROI_{fossil} & net life cycle GHG emissions for examined biomass production pathways & locations

| Parameters | | Cultivation and Harvesting Scenarios (Allocated) | | | | | | | |
|-------------------|-----------------|--|----------------------|------------------------|------------------------|-----------------------|----------------------|------------------------|------------------------|
| Growth Conditions | | Normal Growth Conditions | | | | Low Nitrogen Scenario | | | |
| State | City | MEA/AF/CFE/ CFP/NG | DI/AF/CFE/ CFP/NG | MEA/AF/CFE/ CFP/WHD | DI/AF/CFE/ CFP/ WHD | MEA/AF/CFE/ CFP/NG | DI/AF/CFE/ CFP/NG | MEA/AF/CFE/ CFP/WHD | DI/AF/CFE/ CFP/ WHD |
| AL | Mobile | 0.45 (14.6) | 0.59 (-10.7) | 0.68 (-22.9) | 1.04 (-48.2) | 0.63 (-1.6) | 0.90 (-25.9) | 1.01 (-32.5) | 1.96 (-56.8) |
| AZ | Phoenix | 0.43 (20.7) | 0.56 (-4.7) | 0.64 (-16.8) | 0.94 (-42.2) | 0.59 (4.2) | 0.83 (-20.2) | 0.92 (-26.7) | 1.65 (-51.1) |
| CA | San Diego | 0.46 (9.0) | 0.60 (-16.7) | 0.70 (-28.6) | 1.08 (-54.2) | 0.64 (-6.5) | 0.93 (-31.1) | 1.05 (-37.4) | 2.10 (-61.9) |
| FL | Daytona Beach | 0.44 (15.1) | 0.57 (-10.3) | 0.65 (-22.5) | 0.97 (-47.9) | 0.61 (-1.2) | 0.85 (-25.6) | 0.95 (-32.1) | 1.76 (-56.5) |
| FL | Jacksonville | 0.44 (15.2) | 0.57 (-10.2) | 0.65 (-22.3) | 0.96 (-47.8) | 0.61 (-1.1) | 0.85 (-25.5) | 0.95 (-32.0) | 1.75 (-56.4) |
| FL | Key West | 0.44 (15.7) | 0.56 (-9.7) | 0.65 (-21.8) | 0.96 (-47.2) | 0.60 (-0.6) | 0.85 (-24.9) | 0.95 (-31.5) | 1.72 (-55.8) |
| FL | Miami | 0.44 (14.8) | 0.57 (-10.6) | 0.65 (-22.7) | 0.97 (-48.1) | 0.61 (-1.5) | 0.86 (-25.8) | 0.96 (-32.3) | 1.77 (-56.7) |
| FL | Tallahassee | 0.44 (14.5) | 0.57 (-10.9) | 0.66 (-23.0) | 0.97 (-48.4) | 0.61 (-1.7) | 0.86 (-26.1) | 0.96 (-32.6) | 1.78 (-57.0) |
| FL | Tampa | 0.44 (15.3) | 0.56 (-10.1) | 0.65 (-22.2) | 0.96 (-47.6) | 0.60 (-1.0) | 0.85 (-25.3) | 0.95 (-31.9) | 1.74 (-56.2) |
| FL | West Palm Beach | 0.44 (15.1) | 0.57 (-10.3) | 0.65 (-22.4) | 0.97 (-47.8) | 0.61 (-1.2) | 0.85 (-25.6) | 0.95 (-32.1) | 1.75 (-56.5) |
| GA | Savannah | 0.45 (15.4) | 0.59 (-9.9) | 0.68 (-22.1) | 1.03 (-47.5) | 0.63 (-1.0) | 0.89 (-25.3) | 1.00 (-31.9) | 1.93 (-56.2) |
| LA | Baton Rouge | 0.45 (13.4) | 0.58 (-12.1) | 0.67 (-24.1) | 1.02 (-49.6) | 0.62 (-2.6) | 0.89 (-27.1) | 1.00 (-33.5) | 1.91 (-58.0) |
| LA | Lake Charles | 0.45 (13.2) | 0.58 (-12.3) | 0.68 (-24.3) | 1.02 (-49.8) | 0.62 (-2.8) | 0.89 (-27.2) | 1.00 (-33.7) | 1.92 (-58.1) |
| LA | New Orleans | 0.45 (13.1) | 0.58 (-12.4) | 0.68 (-24.4) | 1.02 (-49.9) | 0.62 (-2.9) | 0.89 (-27.3) | 1.00 (-33.8) | 1.92 (-58.2) |
| TX | Austin | 0.45 (12.9) | 0.58 (-12.5) | 0.67 (-24.6) | 1.02 (-50.0) | 0.62 (-3.2) | 0.89 (-27.5) | 1.00 (-34.1) | 1.91 (-58.4) |
| TX | Brownsville | 0.45 (13.2) | 0.58(-12.2) | 0.67 (-24.3) | 1.01 (-49.7) | 0.62 (-2.9) | 0.88 (-27.2) | 0.99 (-33.8) | 1.89 (-58.1) |
| TX | Corpus Christi | 0.45 (13.5) | 0.58 (-11.9) | 0.67 (-24.0) | 1.01 (-49.4) | 0.62 (-2.6) | 0.88 (-26.9) | 0.99 (-33.4) | 1.88 (-57.8) |
| TX | Houston | 0.45 (13.4) | 0.58 (-12.0) | 0.67 (-24.1) | 1.01 (-49.5) | 0.62 (-2.7) | 0.88 (-27.0) | 0.99 (-33.6) | 1.88 (-57.9) |
| TX | Lufkin | 0.45 (12.9) | 0.58 (-12.5) | 0.67 (-24.6) | 1.02 (-50.0) | 0.62 (-3.2) | 0.89 (-27.6) | 1.00 (-34.1) | 1.91 (-58.4) |
| TX | Port Arthur | 0.46 (9.5) | 0.60 (-16.0) | 0.70 (-28.0) | 1.09 (-53.5) | 0.64 (-6.2) | 0.93 (-30.6) | 1.05 (-37.0) | 2.13 (-61.5) |
| TX | San Antonio | 0.45 (12.7) | 0.58 (-12.7) | 0.68 (-24.8) | 1.02 (-50.2) | 0.62 (-3.4) | 0.89 (-27.7) | 1.00 (-34.3) | 1.92 (-58.6) |
| TX | Victoria | 0.45 (13.3) | 0.58 (-12.1) | 0.67 (-24.3) | 1.01 (-49.6) | 0.62 (-2.8) | 0.88 (-27.2) | 0.99 (-33.7) | 1.89 (-58.1) |

*The results are presented in the following format: EROI_{fossil} (Net Life Cycle GHG Emissions) where Net life cycle GHG emissions are in units of (g CO₂ eq/MJ Biomass)

Table S32 – Alternate Biomass Production Scenario: Allocated EROI_{fossil} & net life cycle GHG emissions for examined biomass production pathways & locations

| Parameters | | Cultivation and Harvesting Scenarios (Unallocated) | | | | | | | |
|-------------------|-----------------|--|--------------------|------------------|-------------------|-----------------------|--------------------|------------------|-------------------|
| Growth Conditions | | Normal Growth Conditions | | | | Low Nitrogen Scenario | | | |
| State | City | MEA/AF/CFE/CFP/NG | MEA/AF/CFE/CFP/WHD | DI/AF/CFE/CFP/NG | DI/AF/CFE/CFP/WHD | MEA/AF/CFE/CFP/NG | MEA/AF/CFE/CFP/WHD | DI/AF/CFE/CFP/NG | DI/AF/CFE/CFP/WHD |
| AL | Mobile | 0.35 (48.9) | 0.47 (11.4) | 0.59 (-10.7) | 1.04 (-48.2) | 0.48 (25.2) | 0.67 (-5.7) | 0.90 (-25.9) | 1.96 (-56.8) |
| AZ | Phoenix | 0.34 (54.9) | 0.45 (17.3) | 0.56 (-4.7) | 0.94 (-42.2) | 0.45 (30.9) | 0.63 (0.0) | 0.83 (-20.2) | 1.65 (-51.1) |
| CA | San Diego | 0.36 (42.5) | 0.48 (4.9) | 0.60 (-16.7) | 1.08 (-54.2) | 0.48 (19.7) | 0.68 (-11.2) | 0.93 (-31.1) | 2.10 (-61.9) |
| FL | Daytona Beach | 0.34 (49.2) | 0.46 (11.6) | 0.57 (-10.3) | 0.97 (-47.9) | 0.46 (25.5) | 0.64 (-5.4) | 0.85 (-25.6) | 1.76 (-56.5) |
| FL | Jacksonville | 0.34 (49.3) | 0.46 (11.7) | 0.57 (-10.2) | 0.96 (-47.8) | 0.46 (25.6) | 0.64 (-5.3) | 0.85 (-25.5) | 1.75 (-56.4) |
| FL | Key West | 0.34 (49.8) | 0.45 (12.3) | 0.56 (-9.7) | 0.96 (-47.2) | 0.46 (26.1) | 0.64 (-4.8) | 0.85 (-24.9) | 1.72 (-55.8) |
| FL | Miami | 0.34 (48.9) | 0.46 (11.4) | 0.57 (-10.6) | 0.97 (-48.1) | 0.46 (25.2) | 0.64 (-5.7) | 0.86 (-25.8) | 1.77 (-56.7) |
| FL | Tallahassee | 0.34 (48.6) | 0.46 (11.1) | 0.57 (-10.9) | 0.97 (-48.4) | 0.46 (25.0) | 0.64 (-5.9) | 0.86 (-26.1) | 1.78 (-57.0) |
| FL | Tampa | 0.34 (49.4) | 0.46 (11.9) | 0.56 (-10.1) | 0.96 (-47.6) | 0.46 (25.7) | 0.64 (-5.2) | 0.85 (-25.3) | 1.74 (-56.2) |
| FL | West Palm Beach | 0.34 (49.2) | 0.46 (11.7) | 0.57 (-10.3) | 0.97 (-47.8) | 0.46 (25.5) | 0.64 (-5.4) | 0.85 (-25.6) | 1.75 (-56.5) |
| GA | Savannah | 0.35 (49.7) | 0.47 (12.2) | 0.59 (-9.9) | 1.03 (-47.5) | 0.47 (25.9) | 0.66 (-5.0) | 0.89 (-25.3) | 1.93 (-56.2) |
| LA | Baton Rouge | 0.35 (47.2) | 0.47 (9.7) | 0.58 (-12.1) | 1.02 (-49.6) | 0.47 (23.9) | 0.66 (-7.0) | 0.89 (-27.1) | 1.91 (-58.0) |
| LA | Lake Charles | 0.35 (47.1) | 0.47 (9.5) | 0.58 (-12.3) | 1.02 (-49.8) | 0.47 (23.7) | 0.66 (-7.2) | 0.89 (-27.2) | 1.92 (-58.1) |
| LA | New Orleans | 0.35 (47.0) | 0.47 (9.4) | 0.58 (-12.4) | 1.02 (-49.9) | 0.47 (23.6) | 0.66 (-7.3) | 0.89 (-27.3) | 1.92 (-58.2) |
| TX | Austin | 0.35 (47.1) | 0.47 (9.6) | 0.58 (-12.5) | 1.02 (-50.0) | 0.47 (23.6) | 0.66 (-7.3) | 0.89 (-27.5) | 1.91 (-58.4) |
| TX | Brownsville | 0.35 (47.4) | 0.47 (9.9) | 0.58(-12.2) | 1.01 (-49.7) | 0.47 (23.9) | 0.66 (-7.0) | 0.88 (-27.2) | 1.89 (-58.1) |
| TX | Corpus Christi | 0.35 (47.7) | 0.46 (10.2) | 0.58 (-11.9) | 1.01 (-49.4) | 0.47 (24.2) | 0.65 (-6.7) | 0.88 (-26.9) | 1.88 (-57.8) |
| TX | Houston | 0.35 (47.6) | 0.47 (10.1) | 0.58 (-12.0) | 1.01 (-49.5) | 0.47 (24.1) | 0.66 (-6.8) | 0.88 (-27.0) | 1.88 (-57.9) |
| TX | Lufkin | 0.35 (47.1) | 0.47 (9.5) | 0.58 (-12.5) | 1.02 (-50.0) | 0.47 (23.6) | 0.66 (-7.3) | 0.89 (-27.6) | 1.91 (-58.4) |
| TX | Port Arthur | 0.36 (43.4) | 0.48 (5.8) | 0.60 (-16.0) | 1.09 (-53.5) | 0.48 (20.3) | 0.68 (-10.6) | 0.93 (-30.6) | 2.13 (-61.5) |
| TX | San Antonio | 0.35 (46.9) | 0.47 (9.4) | 0.58 (-12.7) | 1.02 (-50.2) | 0.47 (23.4) | 0.66 (-7.5) | 0.89 (-27.7) | 1.92 (-58.6) |
| TX | Victoria | 0.35 (47.4) | 0.47 (9.9) | 0.58 (-12.1) | 1.01 (-49.6) | 0.47 (23.9) | 0.66 (-6.9) | 0.88 (-27.2) | 1.89 (-58.1) |

* The results are presented in the following format: EROI_{fossil} (Net Life Cycle GHG Emissions) where Net life cycle GHG emissions are in units of (g CO₂ eq/MJ-Biomass)

12. Reference EROI_{fossil}

EROI_{fossil} for biofuels derived from various feedstock's are provided in the table below. As seen from Table S33, the EROI_{fossil} for algal biofuels can range from 0.29-2.49 depending on whether wet or dry extraction is implemented. The results presented in this work assume that algal biomass will have to be dried to 90% (w/w) before further downstream process of the biomass to biofuel is possible, and are comparable to the results found for producing biomass using the nominal dry route presented in ref[43].

Table S33 – Reference EROI_{fossil} for various biofuels

| Feedstock | Fuel Product | EROI _{fossil} | Source | Notes: |
|---------------------|----------------------|------------------------|------------|--|
| Rapeseed oil | Biodiesel | 2.29 | [44] | Study applicable to UK |
| Rapeseed oil | Biodiesel | 3.0 | [44] | Study applicable to Europe |
| Jatropha oil | Biodiesel | 1.9 | [44] | Study applicable to India |
| Palm oil | Biodiesel | 7.8-10.3 | [44] | Study applicable to Brazil |
| Palm oil | Biodiesel | 5.9-6.9 | [44] | Study applicable to Colombia |
| Recycled frying oil | Biodiesel | 5.51 | [44] | Study applicable to Germany |
| Waste vegetable oil | Biodiesel | 7.8 | [44] | Study applicable to USA |
| Waste vegetable oil | Biodiesel | 7.96 | [44] | Study applicable to Spain |
| Soybean | Biodiesel | 5.54 | [7] | Year: 2011 |
| Algae | Biodiesel | 1.87 | [4] | Assumes wet extraction |
| Algae | Biodiesel | 1.82 | [45] | Assumes wet extraction |
| Algae | Hydrocarbon biofuels | 2.49 | [43] | Nominal wet route |
| Algae | Hydrocarbon biofuels | 0.29 | [43] | Nominal dry route |
| Algae | Biomass | 0.86 | [43] | Nominal dry route |
| Algae | Biomass | 0.38 - 1.08 | This study | Normal Culture Conditions ¹ |
| Algae | Biomass | 0.43 – 2.13 | This study | Low N Scenario ¹ |

¹Allocation is performed

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