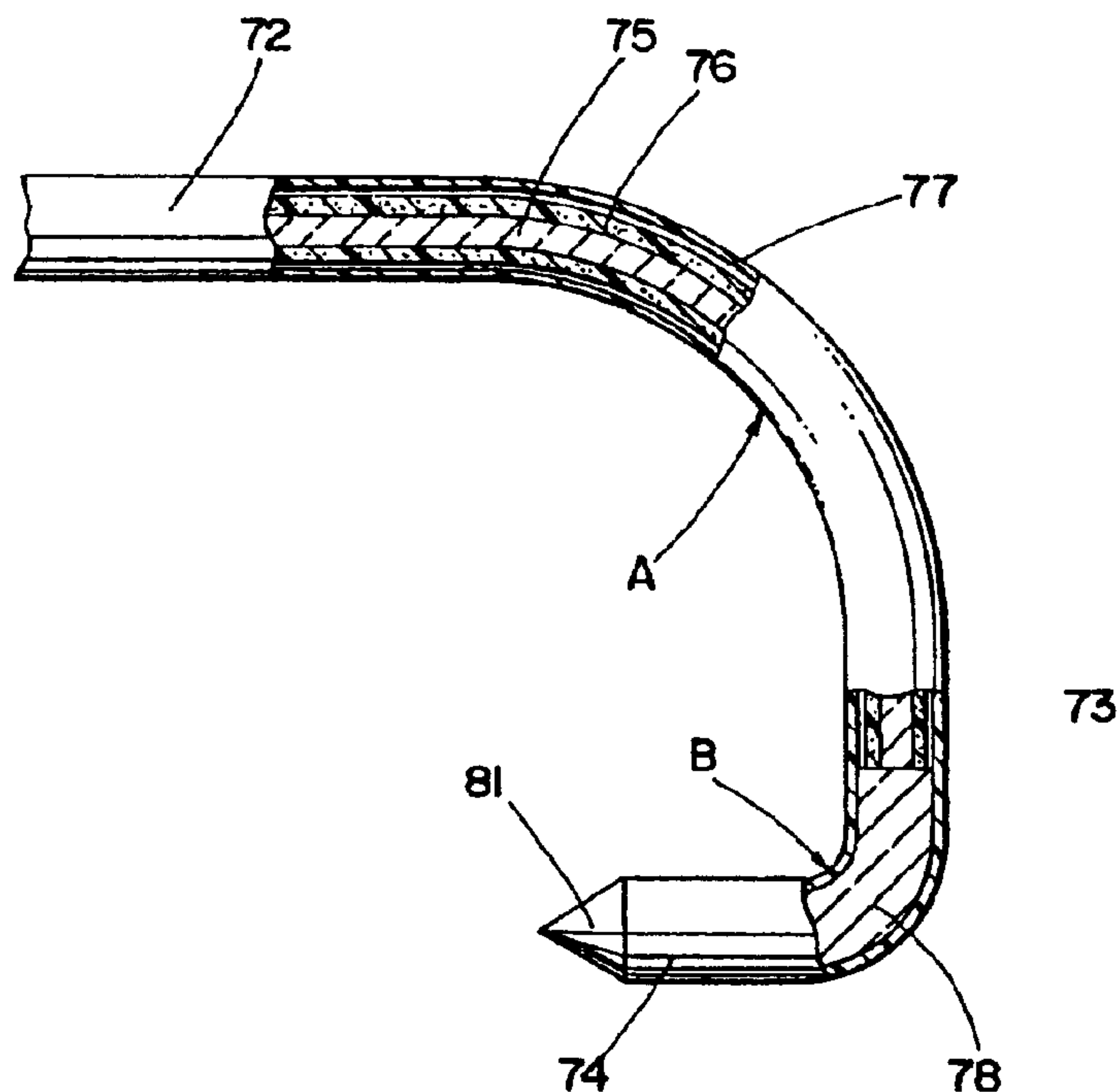




(86) Date de dépôt PCT/PCT Filing Date: 1993/10/07  
 (87) Date publication PCT/PCT Publication Date: 1995/04/13  
 (45) Date de délivrance/Issue Date: 2003/12/30  
 (85) Entrée phase nationale/National Entry: 1996/09/05  
 (86) N° demande PCT/PCT Application No.: US 1993/009656  
 (87) N° publication PCT/PCT Publication No.: 1995/009574

(51) Cl.Int.<sup>6</sup>/Int.Cl.<sup>6</sup> A61N 5/00, A61B 17/36, F21V 8/00,  
G02B 6/00  
 (72) Inventeurs/Inventors:  
DOIRON, DANIEL R., US;  
NARCISO, HUGH L., JR., US  
 (73) Propriétaire/Owner:  
PDT SYSTEMS, INC., US  
 (74) Agent: SMART & BIGGAR

(54) Titre : GUIDE D'ONDE OPTIQUE A POINTES FLEXIBLES  
 (54) Title: OPTICAL WAVEGUIDE WITH FLEXIBLE TIPS



(57) **Abrégé/Abstract:**

A flexible tip (10) for a medical catheter suitable for the transmission of light and dimensioned to pass through extremely small tubular members is described. The flexible tip, preferably made of optically transparent silicone elastomer (13), is affixed to the terminal end of a conventional optical fiber. In a preferred embodiment, the flexible tip comprises a central silicone core (11) surrounded by a cladding (12) having an index of refraction less than that of the core (11), permitting internal reflection. The flexible tip is provided with an outer jacket (13) which serves two purposes: (1) it provides structural integrity for the tip; and (2) it reinforces the union between the flexible tip and the optical fiber to which it is abutted. The tip (10) enables the delivery of a comparable amount of light as a large glass fiber of equal core diameter but possesses much greater flexibility. The tip (10) has the flexibility to be able to enter tortuous tubular members while retaining the light transmitting capabilities of relatively inflexible glass optical waveguides of the same diameter.



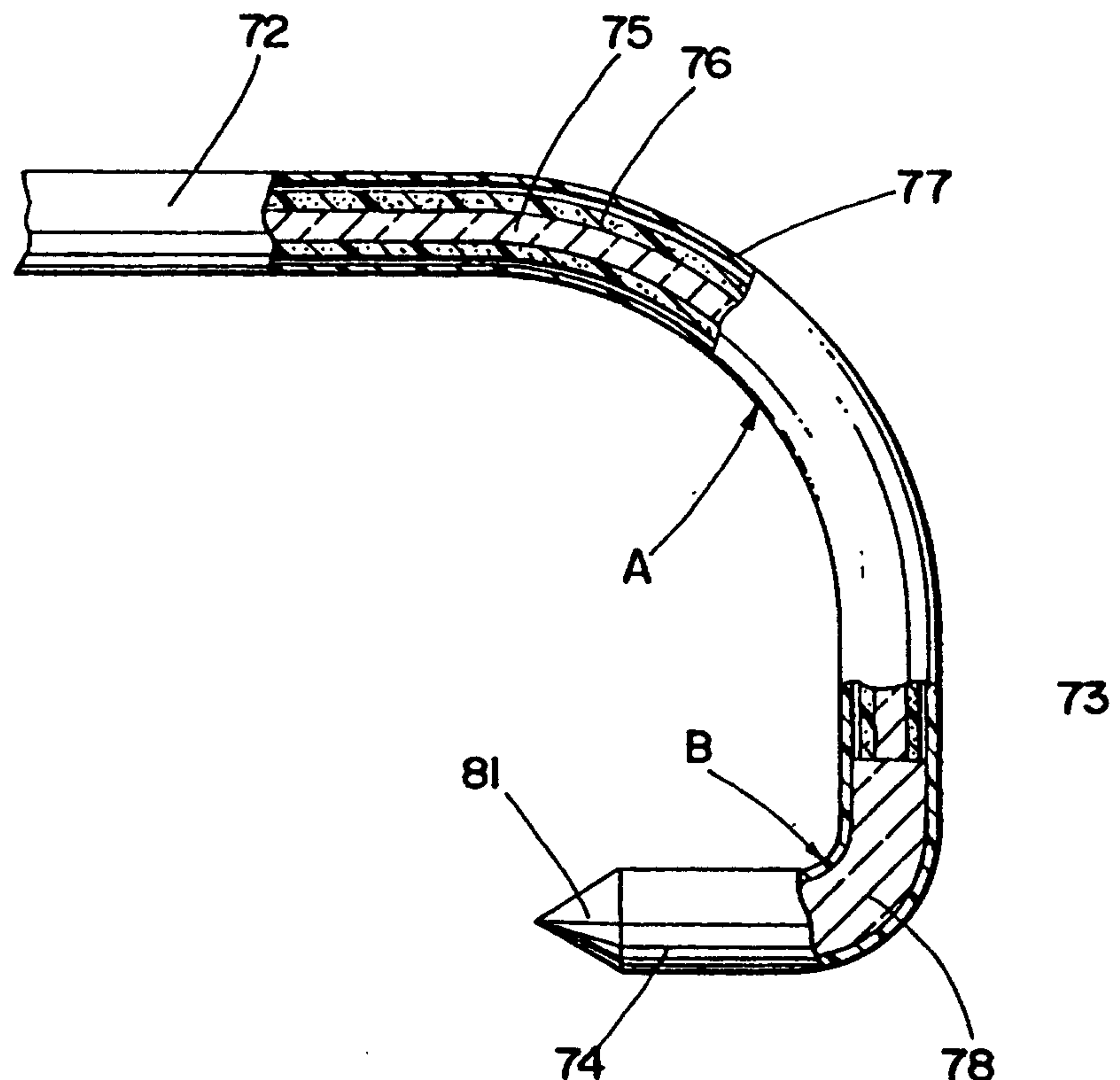
## INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

<p>(51) International Patent Classification<sup>5</sup> : A61B 17/36</p>	A1	<p>(11) International Publication Number: <b>WO 95/09574</b> (43) International Publication Date: 13 April 1995 (13.04.95)</p>
<p>(21) International Application Number: PCT/US93/09656 (22) International Filing Date: 7 October 1993 (07.10.93)</p> <p>(71) Applicant: PDT SYSTEMS, INC. [US/US]; 7408 Hollister Avenue, Goleta, CA 93117 (US).</p> <p>(72) Inventors: DOIRON, Daniel, R.; 3090 Calzada Ridge Road, Santa Ynez, CA 93460 (US). NARCISO, Hugh, L., Jr.; 990 Miramonte Drive #2, Santa Barbara, CA 93109 (US).</p> <p>(74) Agent: PETTIT, Michael, G.; 510 Castillo Street, Santa Barbara, CA 93101 (US).</p>		<p>(81) Designated States: AU, CA, JP, RU, European patent (AT, BE, CH, DE, DK, ES, FR, GB, GR, IE, IT, LU, MC, NL, PT, SE).</p> <p><b>Published</b> <i>With international search report.</i></p> <p style="text-align: center; font-size: 2em;">2184900</p>

(54) Title: OPTICAL WAVEGUIDE WITH FLEXIBLE TIPS

(57) Abstract

A flexible tip (10) for a medical catheter suitable for the transmission of light and dimensioned to pass through extremely small tubular members is described. The flexible tip, preferably made of optically transparent silicone elastomer (13), is affixed to the terminal end of a conventional optical fiber. In a preferred embodiment, the flexible tip comprises a central silicone core (11) surrounded by a cladding (12) having an index of refraction less than that of the core (11), permitting internal reflection. The flexible tip is provided with an outer jacket (13) which serves two purposes: (1) it provides structural integrity for the tip; and (2) it reinforces the union between the flexible tip and the optical fiber to which it is abutted. The tip (10) enables the delivery of a comparable amount of light as a large glass fiber of equal core diameter but possesses much greater flexibility. The tip (10) has the flexibility to be able to enter tortuous tubular members while retaining the light transmitting capabilities of relatively inflexible glass optical waveguides of the same diameter.





1 the difficulty of coupling. Energy density at the fiber optic  
2 tip is the total energy delivered divided by the cross sectional  
3 area of the optical fiber.

4 High energy densities cause undesired damage to the tip of  
5 the fiber. The solution to this problem, with present  
6 technology, is either using larger core diameter optical fibers,  
7 which while reducing the energy density, substantially reduces  
8 the flexibility (doubling the core size reduces the flexibility  
9 fourfold), or using a bundle of small core diameter fiber optics  
10 creating a large proportion of dead space. Dead space, as used  
11 herein, refers to the portion of the cross sectional area of a  
12 fiber optic catheter which does not transmit light energy.

13 Large core fiber optics permit the relatively efficient  
14 coupling of energy from an external source into the fiber; even  
15 if the source is divergent. This is not true of small core  
16 fibers. the coupling efficiency of large cores together with  
17 their rigidity enables them to be readily advanced through a  
18 straight lumen and conduct a large amount of light energy to the  
19 tip. The disadvantage is that the tip lacks the flexibility to  
20 follow a tortuous path.

21 With conventional laser catheter tips heat buildup is a  
22 significant problem. Sapphire or another expensive heat-stable  
23 material is frequently used at the tip of such catheters to  
24 prevent heat-induced fracturing and subsequent disintegration.  
25 Laser surgery is conveniently done by using a flexible quartz

1 fiber for transmitting the laser energy, usually from a Nd:YAG  
2 laser source, to the tissue undergoing treatment. In a typical  
3 laser surgery system the end or tip of the silica fiber optic  
4 serves as the probe for radiating the tissue to effect incision  
5 or coagulation thereof. With some fiber optic tips it is  
6 desirable to hold the tip away from direct contact with the  
7 tissue to avoid fouling of the fiber and, importantly, to avoid  
8 heat damage to the fiber end. Non-contact laser systems  
9 employing a light transmitting member at the output end of the  
10 fiber to focus or otherwise alter the radiation characteristics  
11 of the fiber have also been proposed, for example, by Enderly in  
12 U.S. Patent 4,273,109, and by Daikuzono in U.S. Patent 4,736,743.  
13 Microlenses may also be employed to distribute the light exiting  
14 the catheter. The problem with the foregoing termini for laser  
15 catheters is that they lack the flexibility to enter small  
16 tortuous tubular members such as blood vessels, vas deferens,  
17 ureters and so forth.

#### 18 SUMMARY OF THE INVENTION

19 It is an object of this invention to provide a minimally  
20 invasive medical, light transmitting catheter having the light  
21 transmitting capability of a large core conventional silica fiber  
22 dimensioned to fit within very small tubular members but having  
23 much greater flexibility at the distal end than a comparable  
24 silica fiber optic.

25 It is yet another object of this invention to provide a tip

1 having substantially the same light transmitting capabilities as  
2 silica tips having a much larger diameter while exhibiting  
3 greater flexibility at the tip than can be achieved with silica.

4 It is still another object of this invention to provide a  
5 transluminal catheter for conducting light from a source to a  
6 distal target which has the advantages of a large core silica  
7 fiber for coupling light from a source into the fiber and  
8 permitting advancement of the catheter through the lumen and  
9 having a tip which has the flexibility of a small core silica  
10 fiber.

11 It is yet another object of this invention to provide a  
12 flexible tip for a medical light delivery catheter of a  
13 composition amenable to being formed in many different geometries  
14 or configurations.

15 These and other objects of the invention will soon become  
16 apparent as we turn now to the descriptions of the preferred  
17 embodiment.

#### 18 BRIEF DESCRIPTION OF THE DRAWINGS

19 Figure 1 is a perspective view of the tip of the catheter  
20 of the present invention.

21 Figure 2 is a partially cutaway view of the tip of Figure  
22 1.

23 Figure 3 is a longitudinal cutaway view of the catheter of  
24 the present invention with a first preferred embodiment of the  
25 tip in place.

1           Figure 4 is a longitudinal cutaway view of the catheter of  
2 the present invention with a second preferred embodiment of the  
3 diffuser tip in place.

4           Figure 5 is another longitudinal, cross sectional view of  
5 an embodiment of the catheter of the current invention with the  
6 core of the flexible tip spaced from the core of the optical  
7 fiber.

8           Figure 6 is the same as Figure 5 except a cladding surrounds  
9 the core material of the tip.

10          Figure 7 is a partially cutaway schematic view of an  
11 embodiment of the invention used with a divergent light source.

12          Figure 8 shows the embodiment of Figure 7 with the flexible  
13 tip fitted with a terminus configured as (a) a pointed probe, (b)  
14 a rounded smooth terminus, and (c) a focusing lens.

#### 15                           DESCRIPTION OF THE PREFERRED EMBODIMENT

16          A flexible tip for use with the invasive catheter of the  
17 present invention is shown in Figure 1, generally indicated at  
18 10. The central core 11 of the flexible tip 10 is made from an  
19 optically transmissive material such as silicone, silicone  
20 copolymer, or any variety of elastomers. Surrounding the central  
21 core 11 is a cladding layer 12, again fabricated from silicone,  
22 silicone copolymer or elastomer. The cladding layer 12 and the  
23 core 11 are specifically chosen for their refractive indices.  
24 The refractive index of the cladding 12, which may be a length  
25 of tubing, is preferably less than the refractive index of the

1 core 11. Correctly choosing the refractive indices of the  
2 materials will insure total internal reflection of the light  
3 energy while also controlling the solid angle of the exiting  
4 light energy (not shown). The tip 10 shown in Figure 1 is  
5 abutted to a single fiber (not shown) or fiber bundle (not shown)  
6 to receive the light from the optical fiber(s) (not shown) and  
7 ultimately to deliver the light energy to the treatment site.  
8 The tip core 11 and the cladding 12 are held in position relative  
9 to the fiber optic (not shown) by a structural tube 13 made with  
10 flexible elastomeric material such as Teflon™ or polyurethane.

11  
12 Figure 2 is a cut away view of the tip of Figure 1. It is  
13 clear that the optically transmissive tip core 11 is surrounded  
14 by a cladding layer 12 which in turn is surrounded by a  
15 structural tube 13 made of flexible elastomeric material. The  
16 outer tube 13 may, of course, be made from a variety of flexible  
17 elastomers including Teflon™ and polyethylene. The catheter of  
18 the present invention, showing the flexible tip abutted to the  
19 terminus of the fiber optic is shown in Figure 3. The catheter,  
20 generally indicated at numeral 30, has a fiber optic portion 34  
21 abutted to the flexible tip portion 10. The fiber optic portion  
22 34 of the catheter 30 comprises a fiber central core 31  
23 surrounded by a cladding 32. The core 31 and cladding 32 are  
24 enclosed in a jacket 33. The distal tip, or terminus, 35 of the  
25 optical fiber portion 34 is abutted against the tip core 11 of



1 the flexible tip 10. The tip core 11 is surrounded by tip an  
2 outer sheath 13. Treatment light (not shown) exits the tip of  
3 the catheter 30 in Figure 3 in the forward direction towards the  
4 right. The flexible tip 10 may also include a cladding 12  
5 surrounding the tip core 11 as shown in embodiment 40 in Figure  
6 4.

7 A second preferred embodiment of the catheter of the present  
8 is generally indicated at 50 in Figure 5. In this embodiment the  
9 distal tip 35 of the optical fiber portion 34 is spaced from the  
10 flexible tip core 11 of the tip portion 10 by means of a liquid  
11 or gas-filled space 51. The fluid gap 51 allows greater power  
12 handling capabilities by substantially reducing the power density  
13 of the transmissive core 11/fluid gap 51 interface compared to  
14 the transmissive core 11/fiber optic 31 interface. The fluid  
15 space 51 may be filled with a gas or a fluid.

16 Figure 6 shows yet another embodiment 60 of the catheter  
17 shown in Figure 5 except that the flexible tip has a cladding  
18 material 12 surrounding the flexible tip core 11 of the flexible  
19 tip 10.

20 It is important that the fiber optic core 31 retain its  
21 cladding 32 during fabrication of the catheter. If the cladding  
22 32 is stripped from around the core 31 of the fiber optic 34, the  
23 catheter will be vulnerable to breakage at the point where the  
24 cladding has been stripped from the core. The material chosen  
25 for the fiber optic core is less elastic of flexible than the

1 material chosen for the core of the flexible tip.

2 The advantage of combining a large core silica fiber with  
3 an elastomer tip is seen by looking now to Figure 7. Divergent  
4 light 70 from a divergent source such as a diode laser 71 readily  
5 enters the large core 75 of the silica fiber 72 which conducts  
6 the light to the core 78 of the flexible elastomeric tip 74.  
7 Optically transparent silicone rubber is preferably employed as  
8 a material of choice for the tip 74 due to its biocompatibility.  
9 The index of refraction of the material comprising the flexible  
10 tip 74 is preferably close to that of the core 75 of the fiber  
11 optic. Alternatively, the space 51 in the embodiment shown in  
12 Figures 5 and 6 may be filled with a optically transparent  
13 material having an index of refraction between the index of the  
14 tip core 74 and the fiber core 75. The relative stiffness of the  
15 large diameter silica core 75, enhanced by the presence of  
16 cladding jacket 76 and outer sheath 77, permits advancement of  
17 the catheter through constricted tubular tissue but has a large  
18 minimum radius of curvature A. The silicone core tip 74, being  
19 relatively short compared to the silica core fiber optic 72  
20 portion, is pushed ahead of the fiber portion 72 during  
21 advancement. The silicone core tip, being more flexible, has a  
22 much smaller minimum radius curvature, shown at B in Figure 7,  
23 enabling it to track sharp turns, guiding the silicone core  
24 portion 72 during advancement. The silicone core tip 74 and the  
25 silica core 75 of the fiber optic portion 72 of the waveguide

1 form a high coupling efficiency union 73. This union 73 can  
2 conveniently be made by extending the sheath (not shown) surround  
3 the silica core portion beyond the silica core portion and  
4 filling the sheath with uncured silicone followed by curing.

5 Figure 8 shows the embodiment of the flexible tipped  
6 waveguide of Figure 7 with a variety of flexible tip terminus  
7 configurations. Since the flexible tip 74 is elastomeric, it  
8 readily bonds to various other plastics. Figure 8(a) shows the  
9 flexible tip 74 with a pointed terminus 81 suitable for  
10 interstitial use. A rounded or beveled terminus 82 (Figure 8(b))  
11 is useful for intraluminal use. Figure 8(c) shows a focusing  
12 lens 83 affixed to the flexible tip 74. The termini 81-83 may  
13 be fabricated from any transparent material or they may be opaque  
14 if the light reaching the flexible tip 74 tip need not exit the  
15 tip in the forward direction.

16 It will be appreciated that, while a preferred embodiment  
17 of the invention has been described herein, various modifications  
18 will suggest themselves to those skilled in the art. For  
19 example, variations in materials may be required for certain  
20 industrial applications. The essential feature of the invention  
21 is the placement of a flexible tip on a relatively rigid, large  
22 core optical fiber to confer the advantages of both materials to  
23 a combination product while minimizing their disadvantages.  
24 Rigid, large core fibers having relatively inflexible cores  
25 comprising a transparent material other than silica such as a

1 plastic may be used. Flexible elastomers other than silicone may  
2 also be used for the tip. These and other modifications that may  
3 suggest themselves to those skilled in the art are considered to  
4 be within the spirit and scope of the present invention as set  
5 forth in the following claims.

1  
2  
3  
4  
5  
6  
7  
8  
9  
10  
11  
12  
13  
14  
15  
16  
17  
18  
19  
20  
21  
22  
23  
24  
25

CLAIMS

What I claim is:

1. An optical waveguide for conducting light from a light source to a target, said waveguide comprising:

(a) a fiber optic portion having a proximal and a distal end and a first light conducting core consisting of a first core material coextensive with said fiber optic portion; and

(b) a tip portion comprising a light conducting second core having a proximal and distal end, the proximal end of said second core being in optical communication with the distal end of said first core and wherein the second core material is more flexible than said first core material.

2. A medical catheter for conveying light energy from a source of said light energy to a tissue undergoing light treatment, the catheter comprising:

(a) a fiber optic portion having a proximal and distal end and a light transmitting first core coextensive therewith; and

(b) a tip portion, said tip portion comprising a light-transmitting second core having a proximal and distal end, said second core consisting of a substantially transparent elastomer having a

1 flexibility greater than said first core, the proximal  
2 end of said second core being in optical communication  
3 with said distal end of said first core, and wherein  
4 said proximal end of said tip portion is affixed to  
5 the distal end of said optical fiber portion of said  
6 catheter.

7 3. The medical catheter of Claim 2 further comprising  
8 an outer sheath surrounding said second core.

9 4. The medical catheter of Claim 3 further comprising  
10 a layer of cladding interposed between said elastomeric second  
11 core and said outer sheath.

12 5. The medical catheter of Claim 4 wherein said  
13 cladding consists of silicone elastomer.

14 6. The medical catheter of Claim 2 wherein said  
15 elastomer comprises optically transparent silicone.

16 7. The optical waveguide of claim 2 further  
17 comprising a pointed terminus, affixed to said distal end of said  
18 tip portion.

19 8. The optical waveguide of claim 2 further  
20 comprising a rounded terminus affixed to said distal end of said  
21 tip portion.

22 9. The optical waveguide of claim 2 further  
23 comprising a focusing lens affixed to the distal end of said tip  
24 portion.

25 10. A medical catheter for conveying light energy from

1 a source of said light energy to a tissue undergoing light  
2 treatment, the catheter comprising:

3 (a) a fiber optic portion having a proximal and  
4 distal end and a light transmitting first core  
5 coextensive with said fiber optic portion; and

6 (b) a tip portion comprising a light-transmitting  
7 second core consisting of a substantially transparent  
8 elastomer having a proximal and distal end, said  
9 proximal end of second core being in optical  
10 communication with said distal end of said first core,  
11 and wherein a space is interposed between said  
12 proximal end of said tip portion and the distal end of  
13 said optical fiber portion of said catheter.

14 11. The medical catheter of claim 10 wherein said space is  
15 filled with a material having an index of refraction intermediate  
16 to the index of refraction of said first and second cores.

17

18

19

20

21

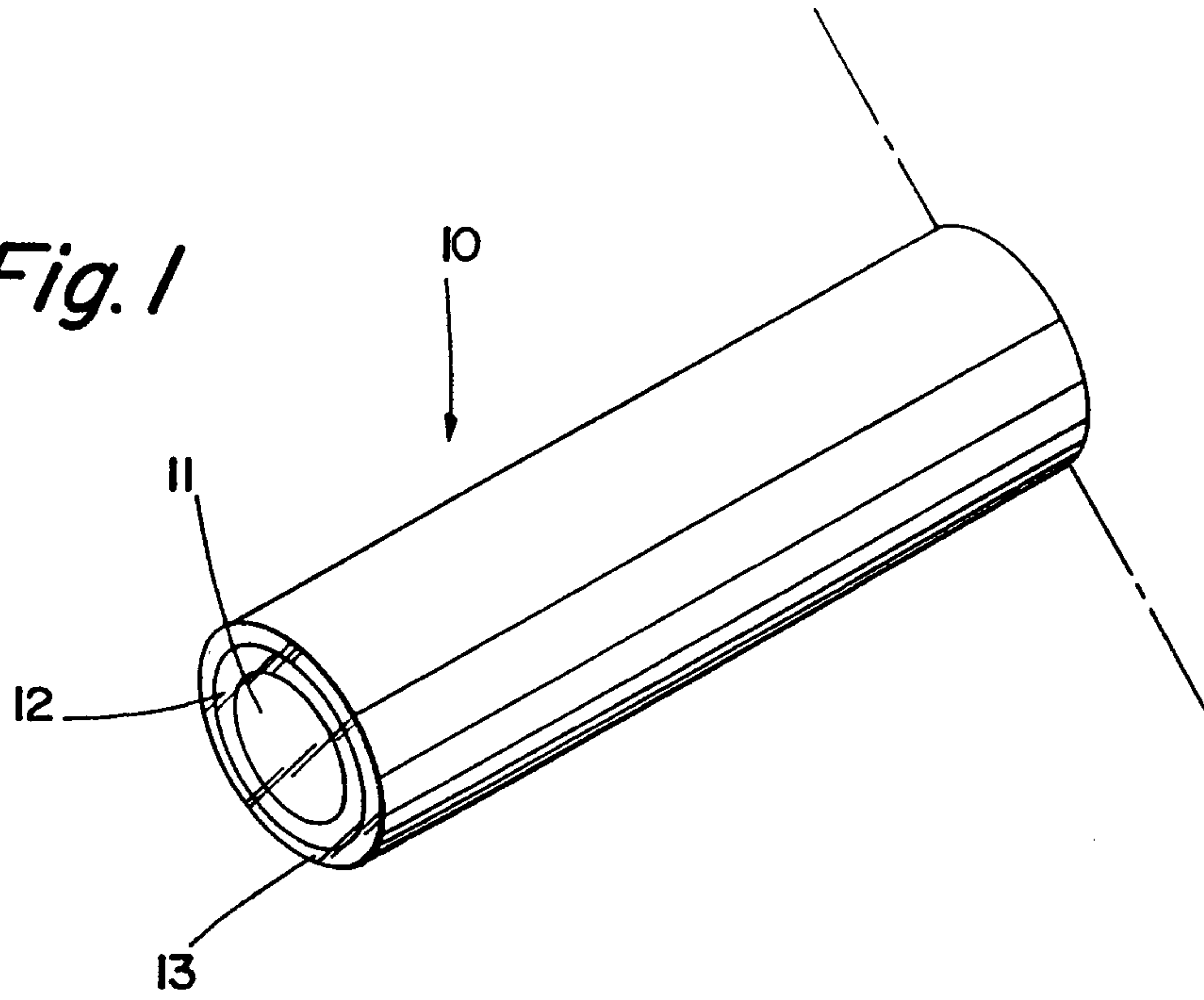
22

23

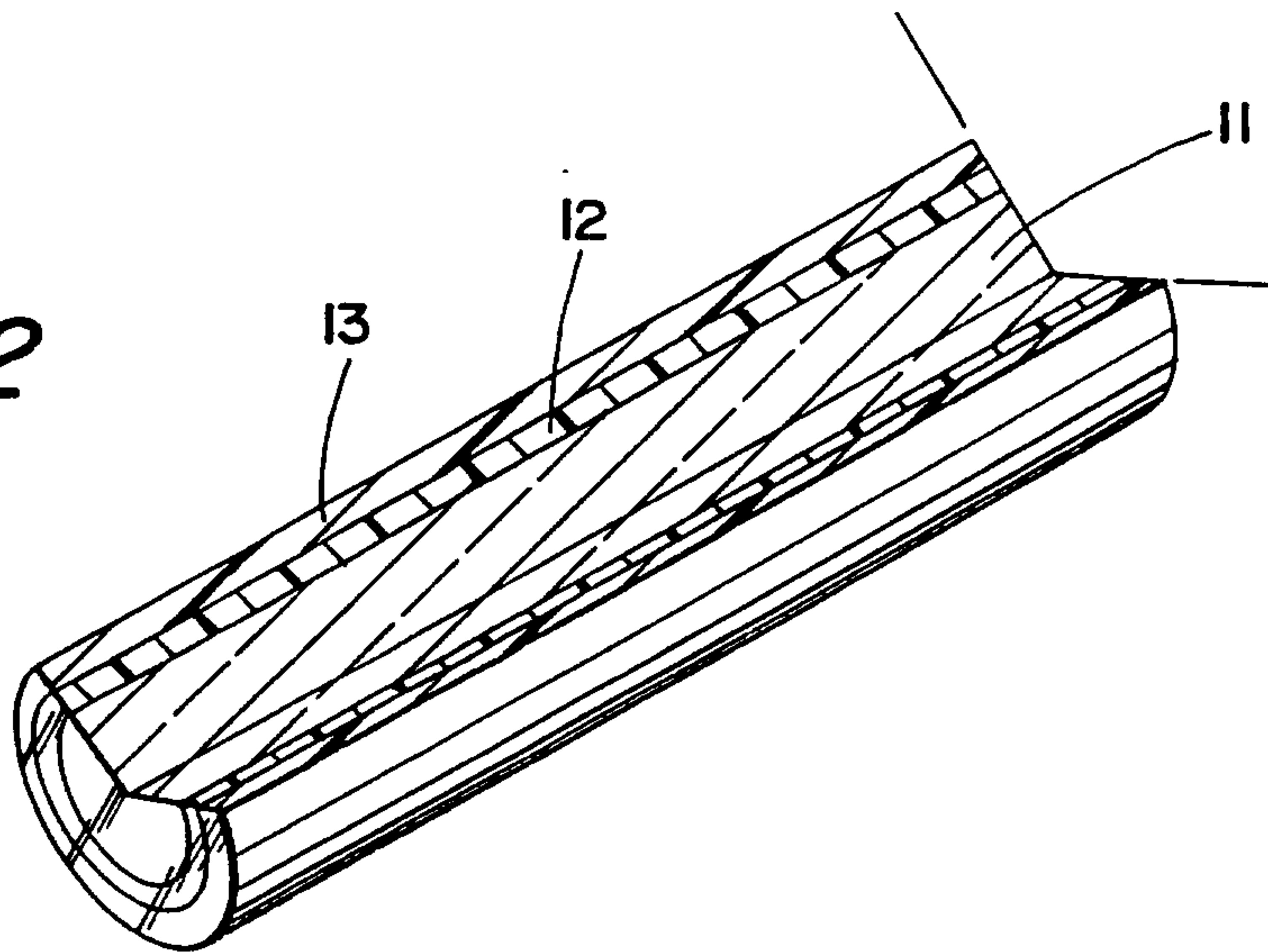
24

25

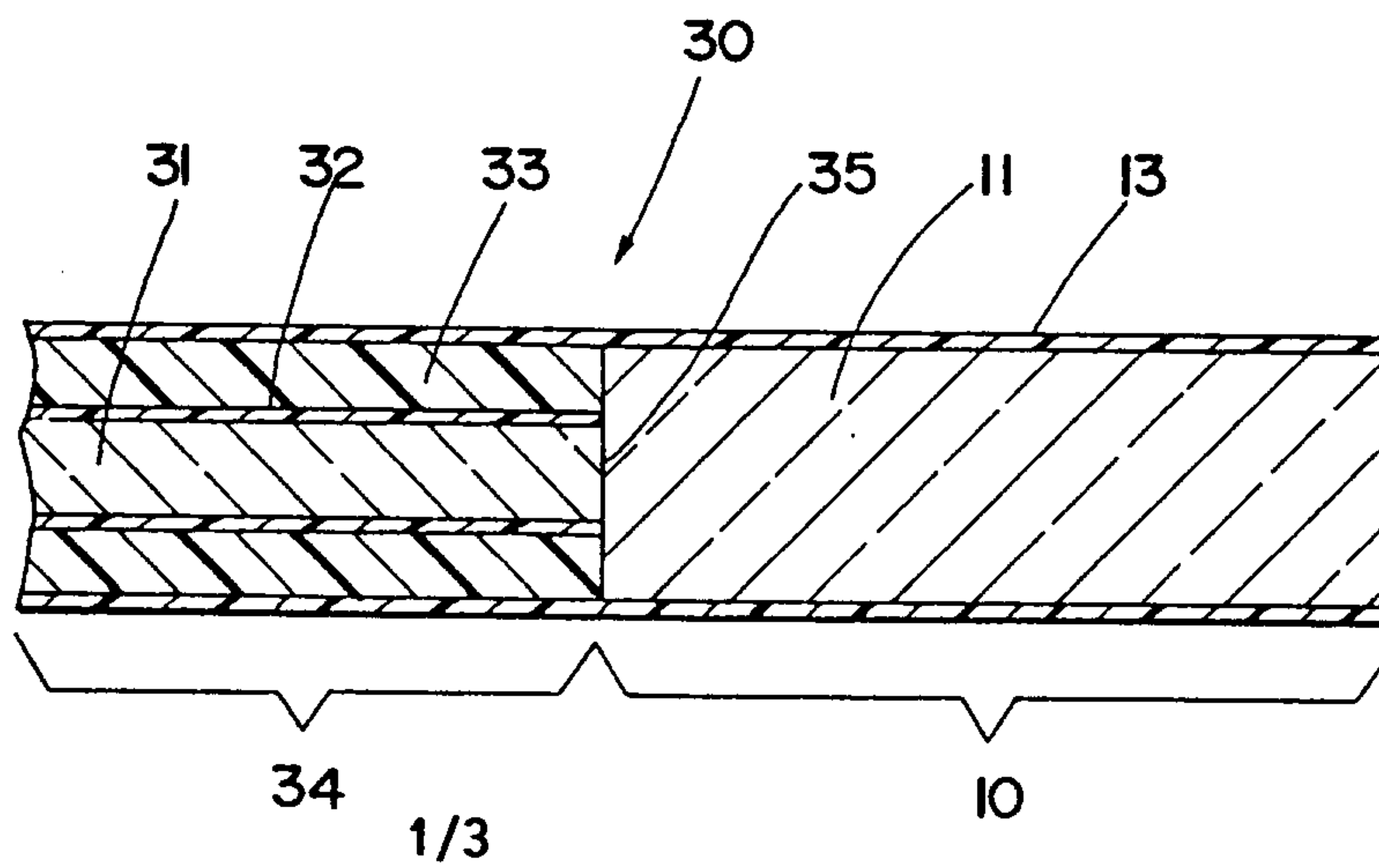
*Fig. 1*



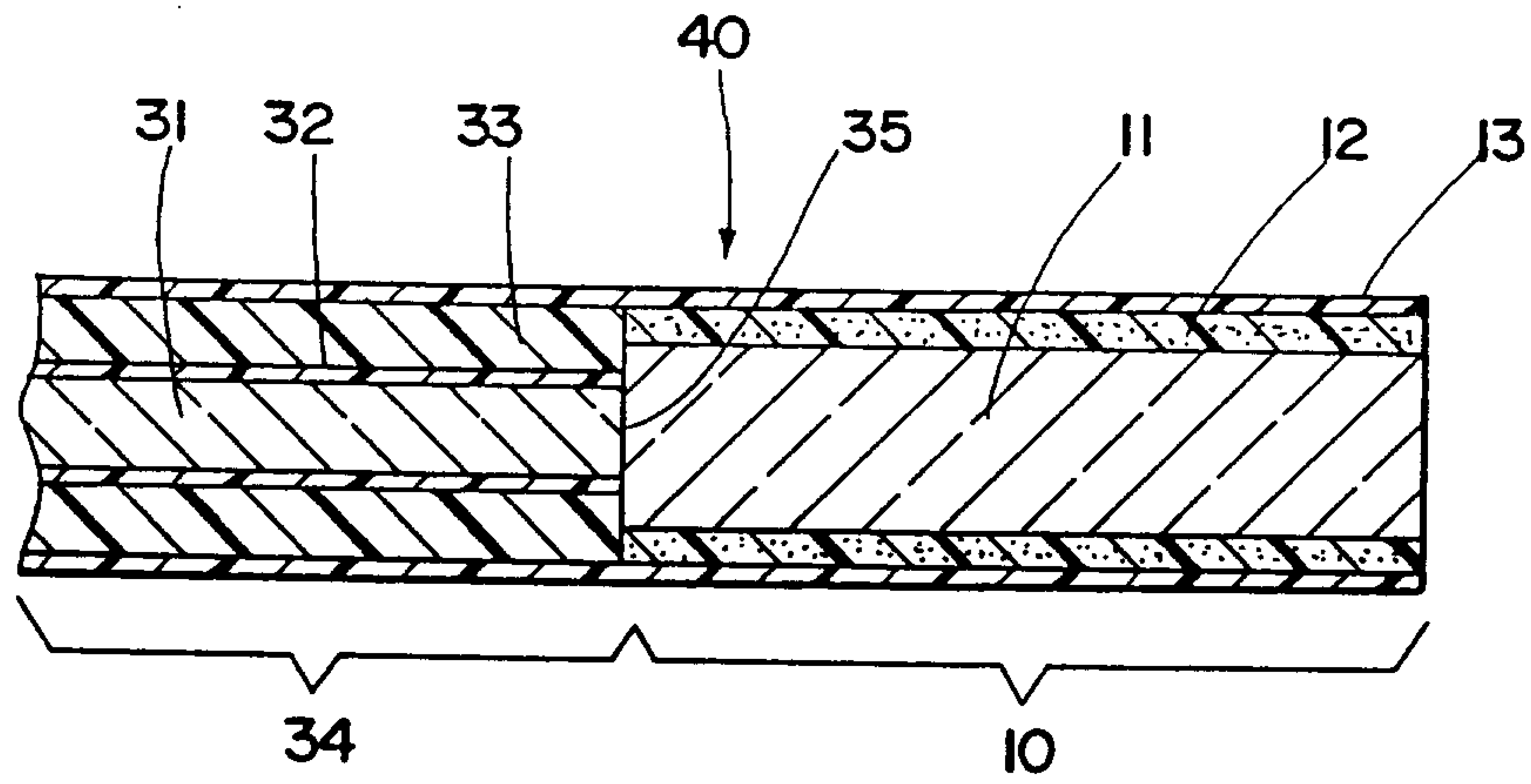
*Fig. 2*



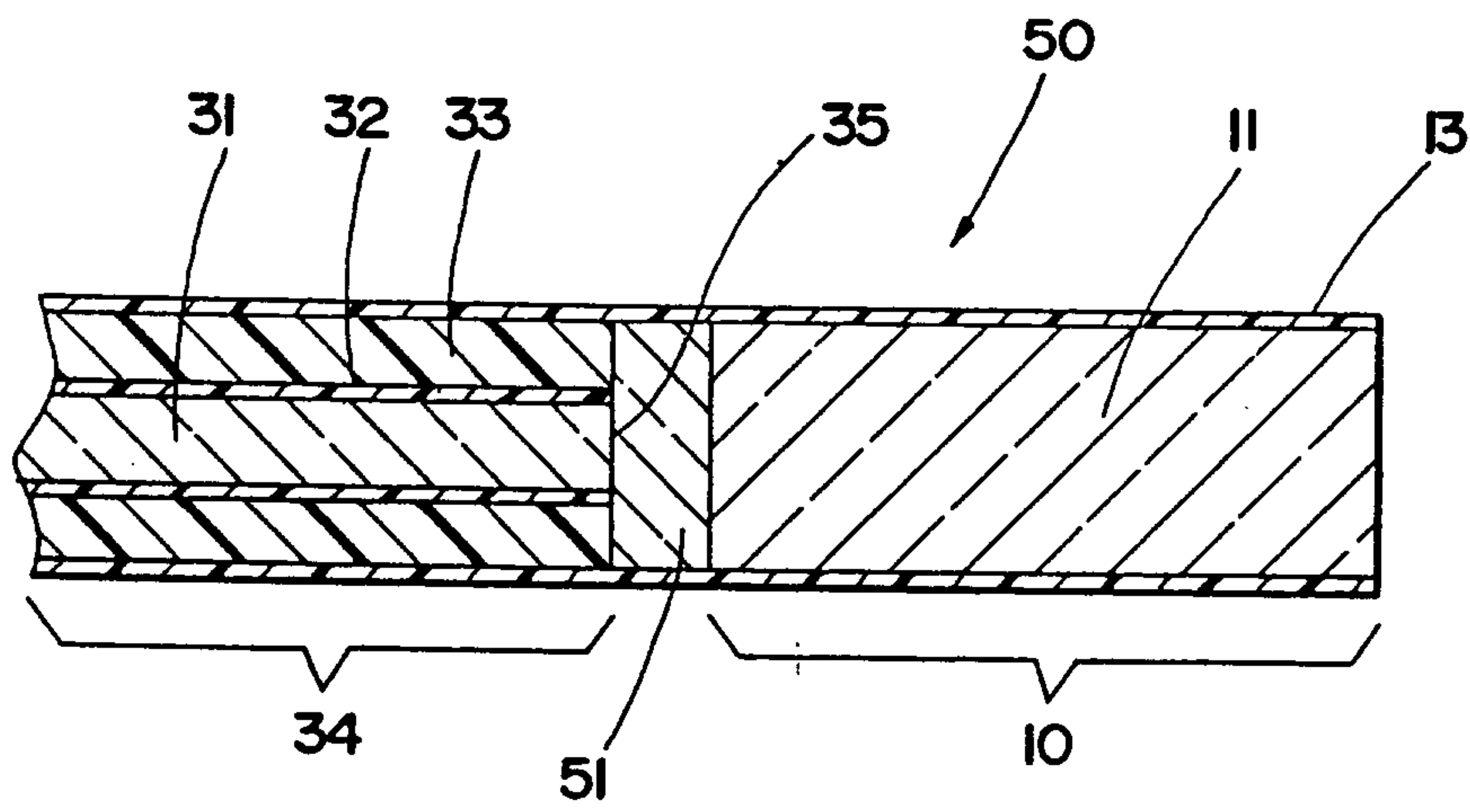
*Fig. 3*



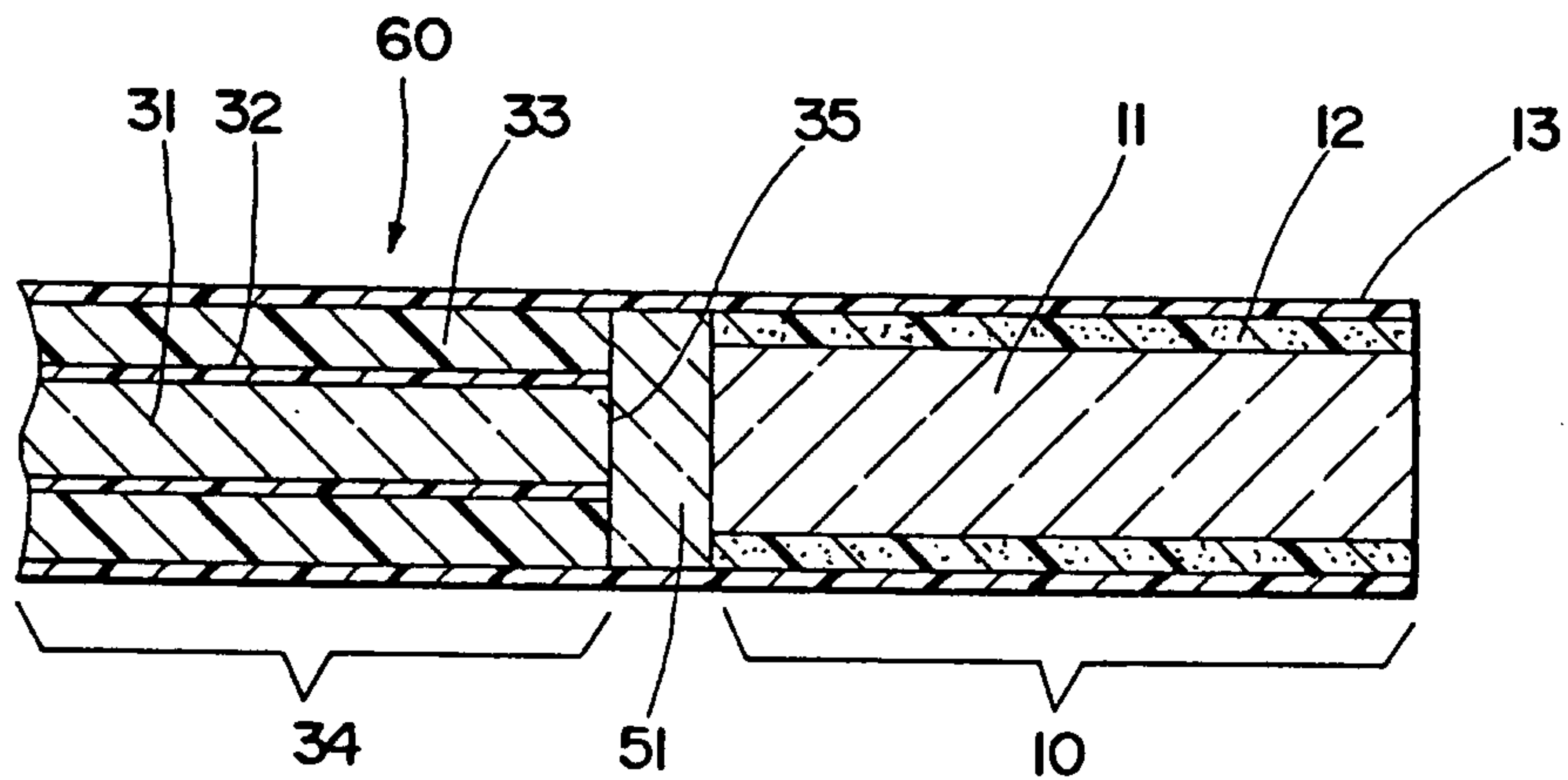




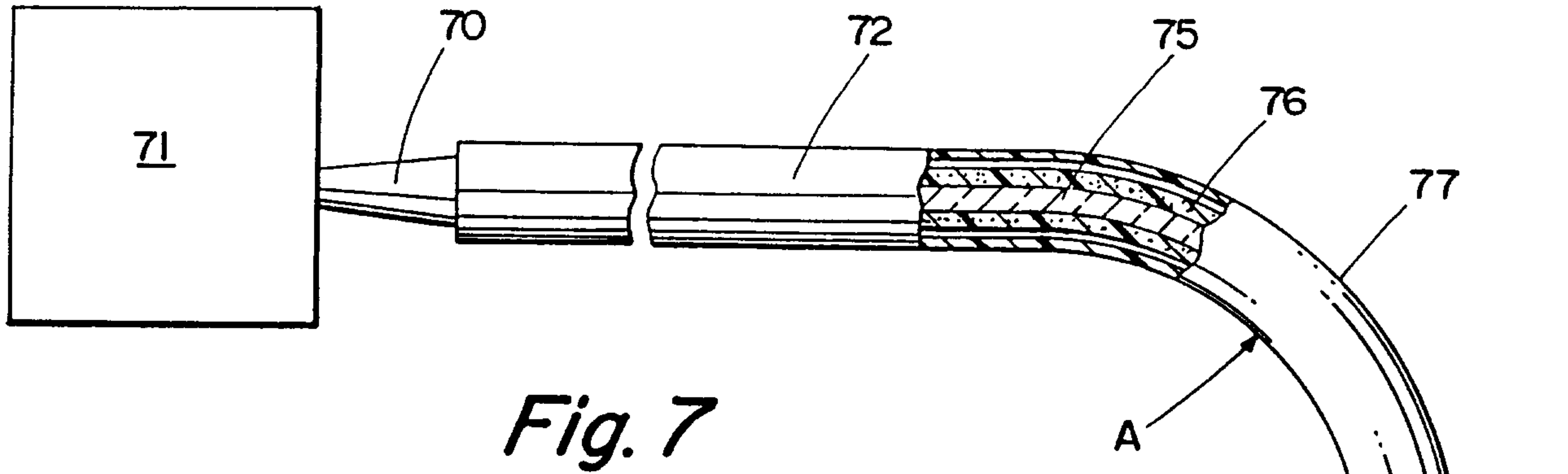
*Fig. 4*



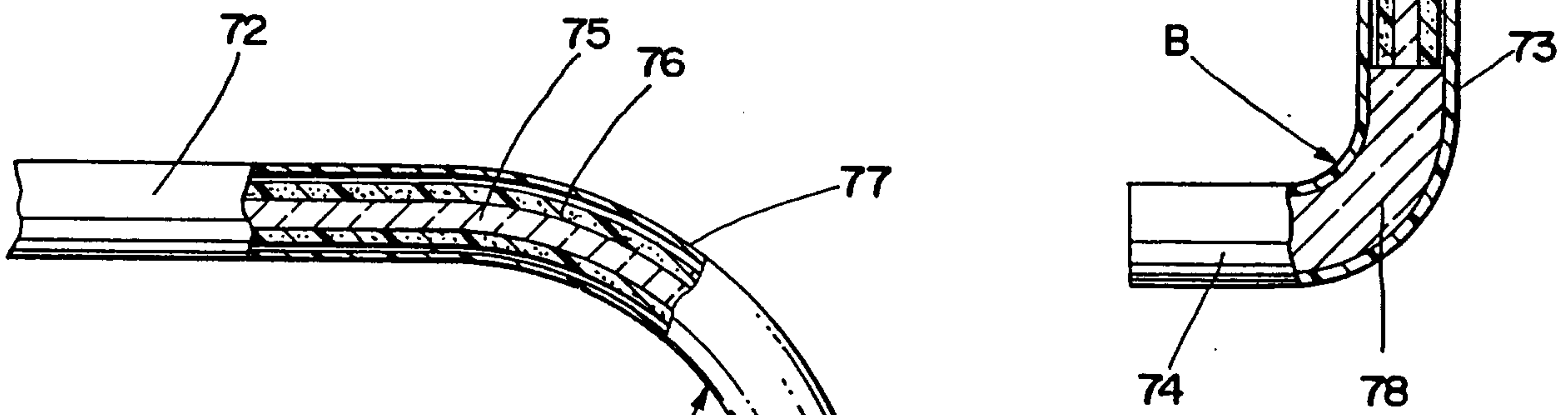
*Fig. 5*



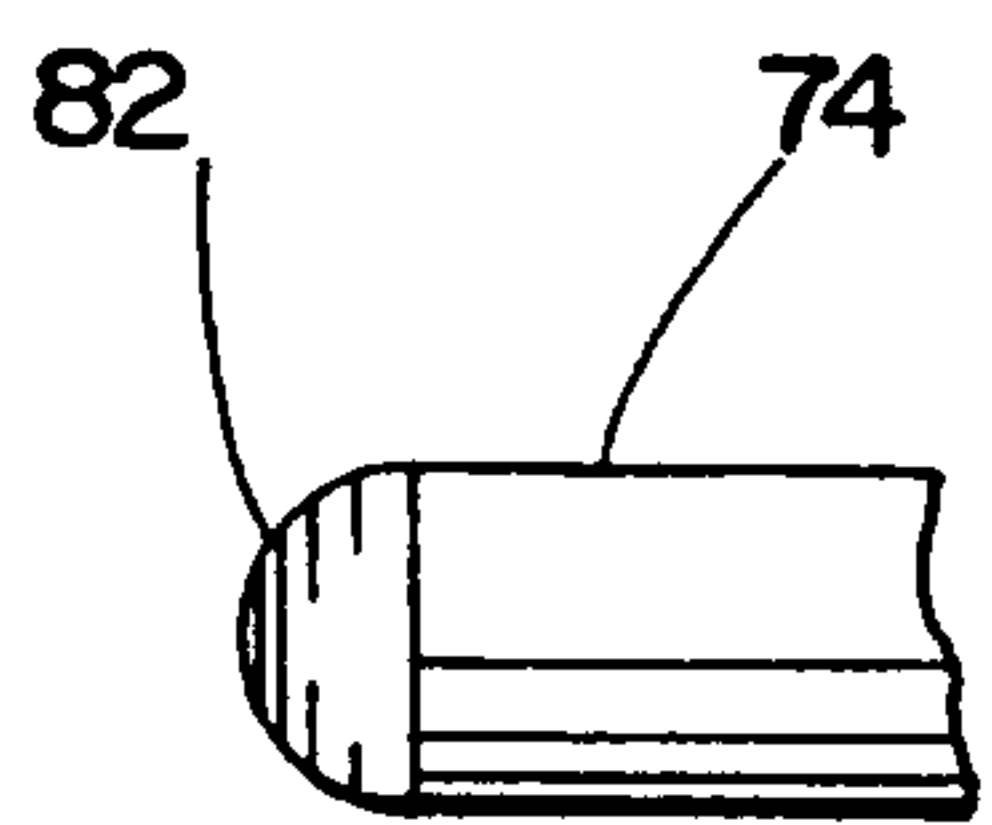
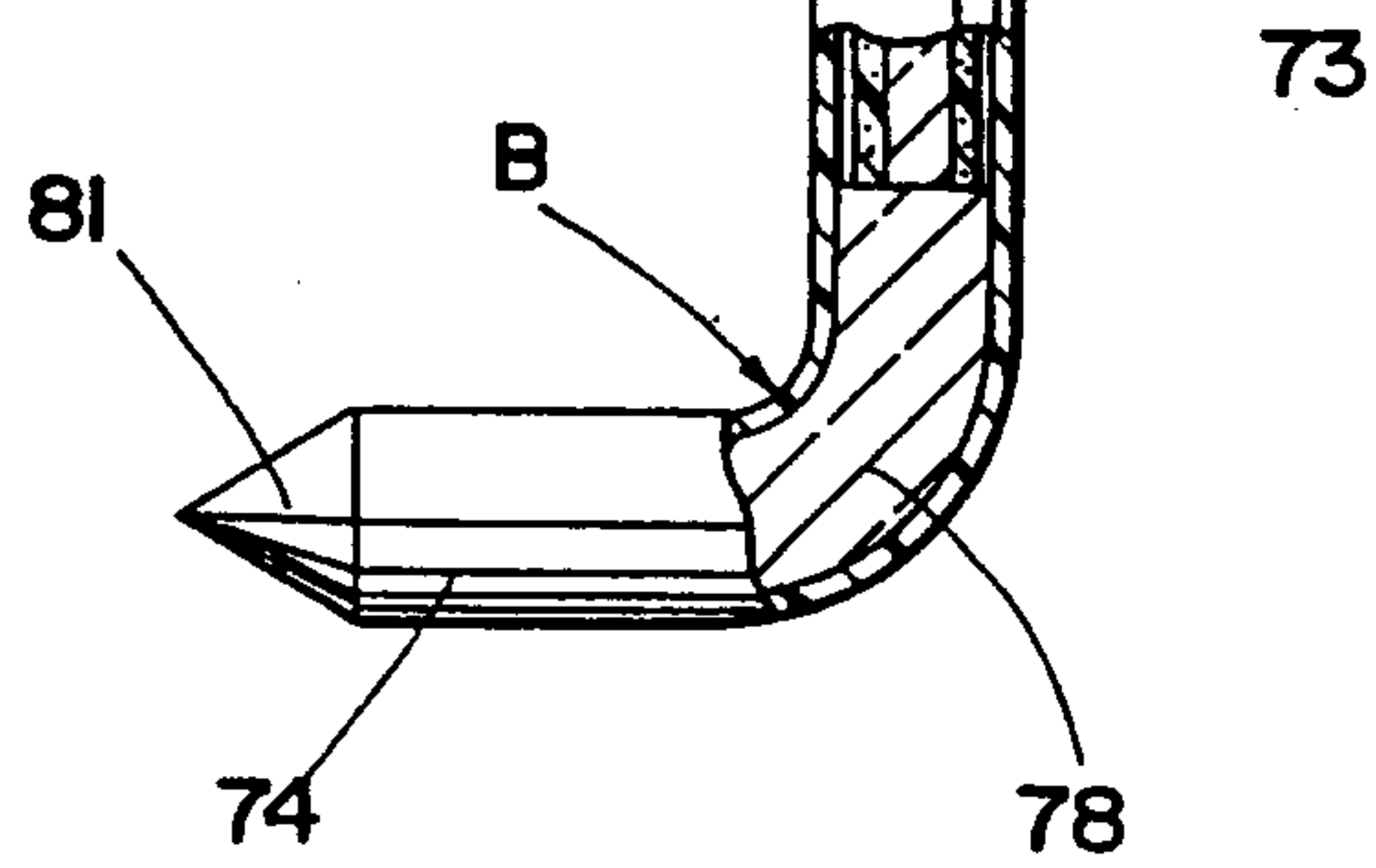
*Fig. 6*



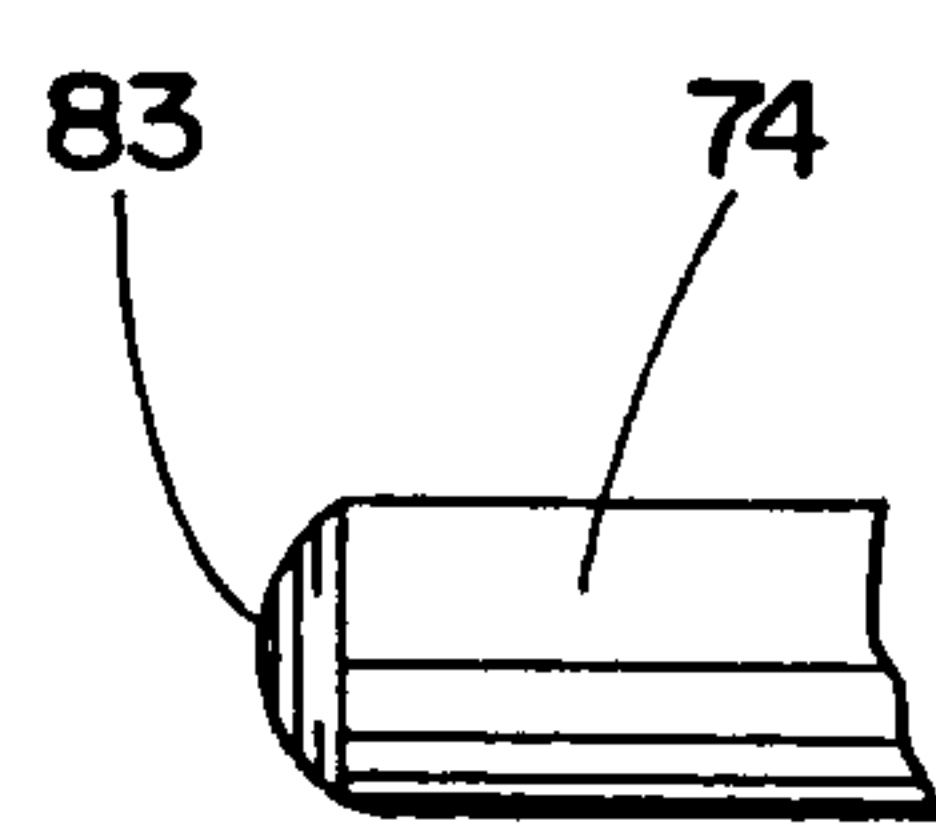
*Fig. 7*



*Fig. 8(a)*



*Fig. 8(b)*



*Fig. 8(c)*

