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(72) Inventor(s):
**Erik M Henrikson
Matthew W Simone
Yujen Huang**

(73) Proprietor(s):
**Karsten Manufacturing Corporation
(Incorporated in USA - Arizona)
2201 West Desert Cove, Phoenix, Arizona 85029,
United States of America**

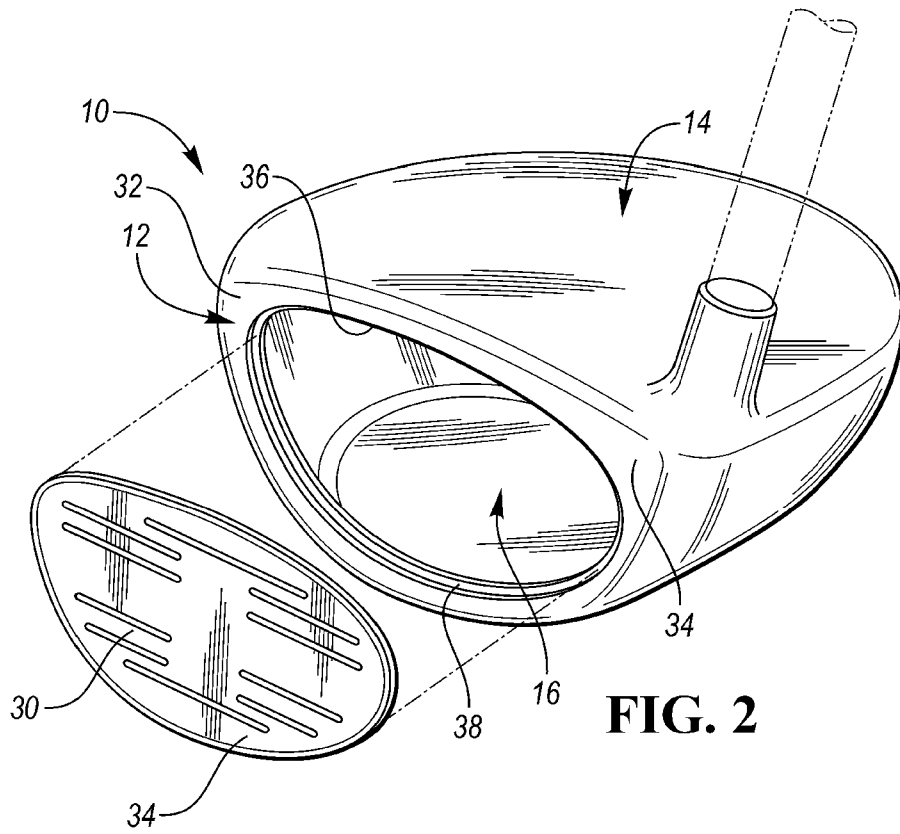
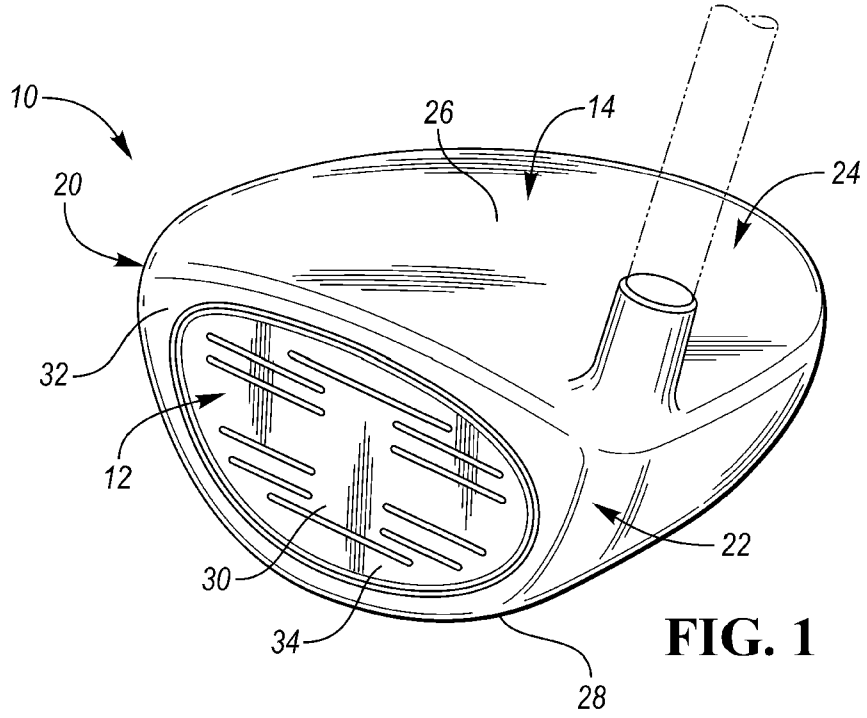
(74) Agent and/or Address for Service:
**Mewburn Ellis LLP
Aurora Building, Counterslip, Bristol, BS1 6BX,
United Kingdom**

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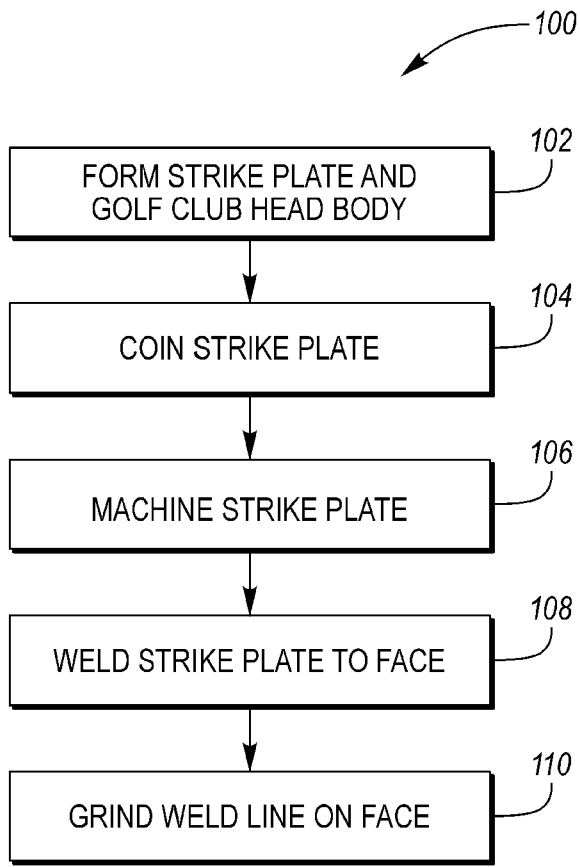


FIG. 3

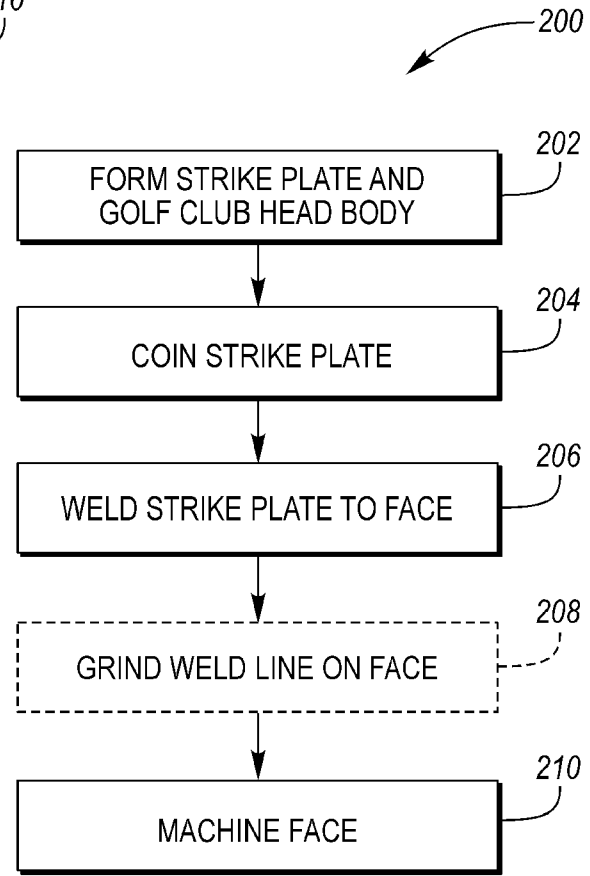


FIG. 4

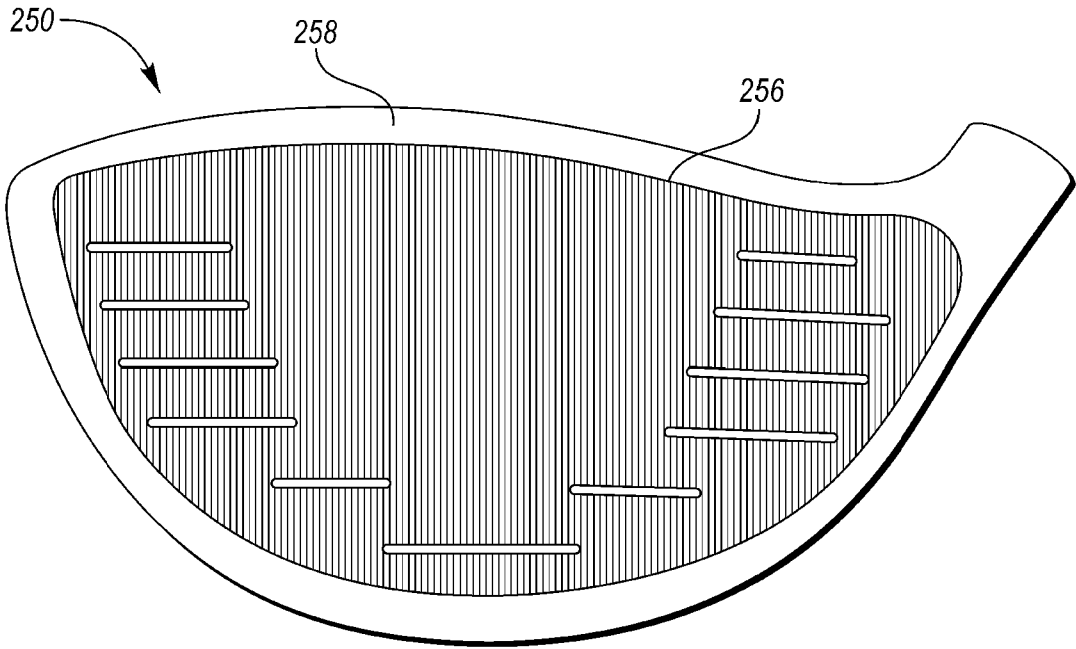


FIG. 5A

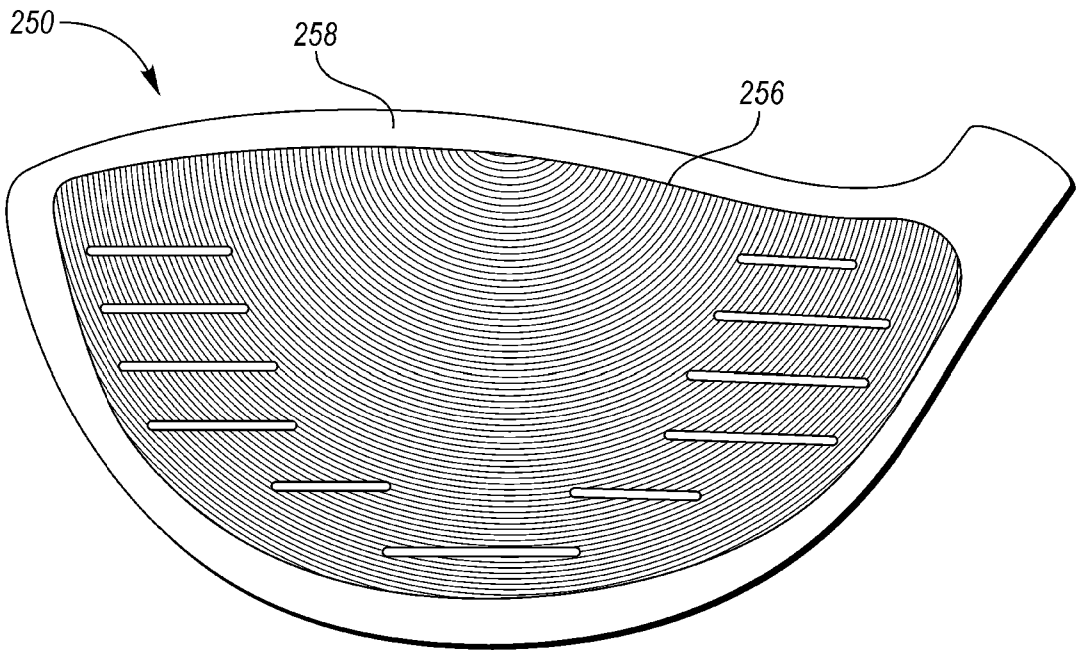


FIG. 5B

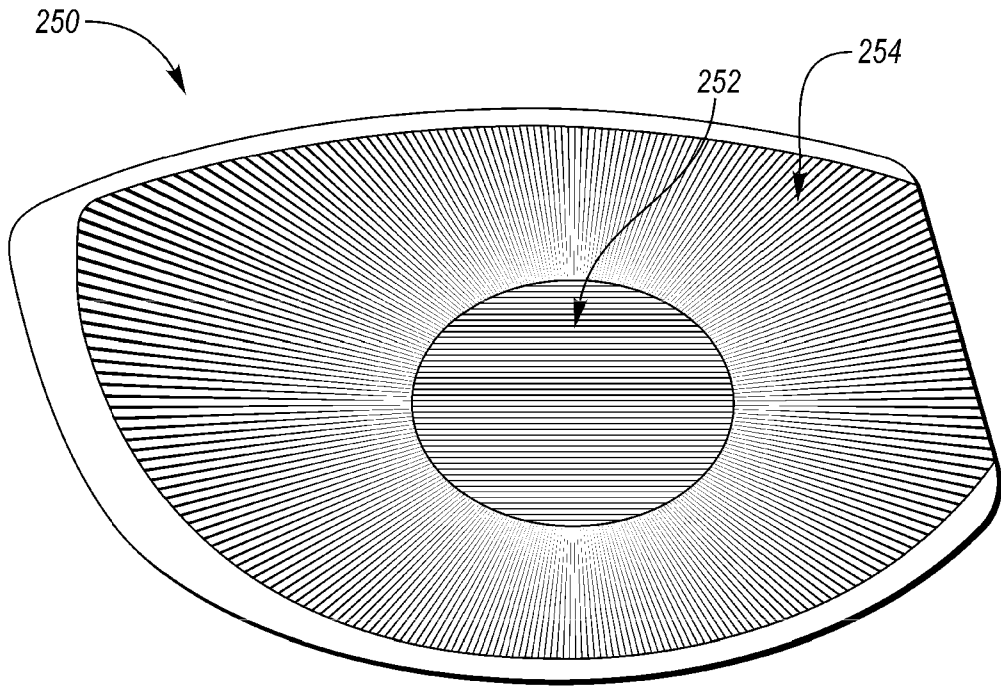


FIG. 5C

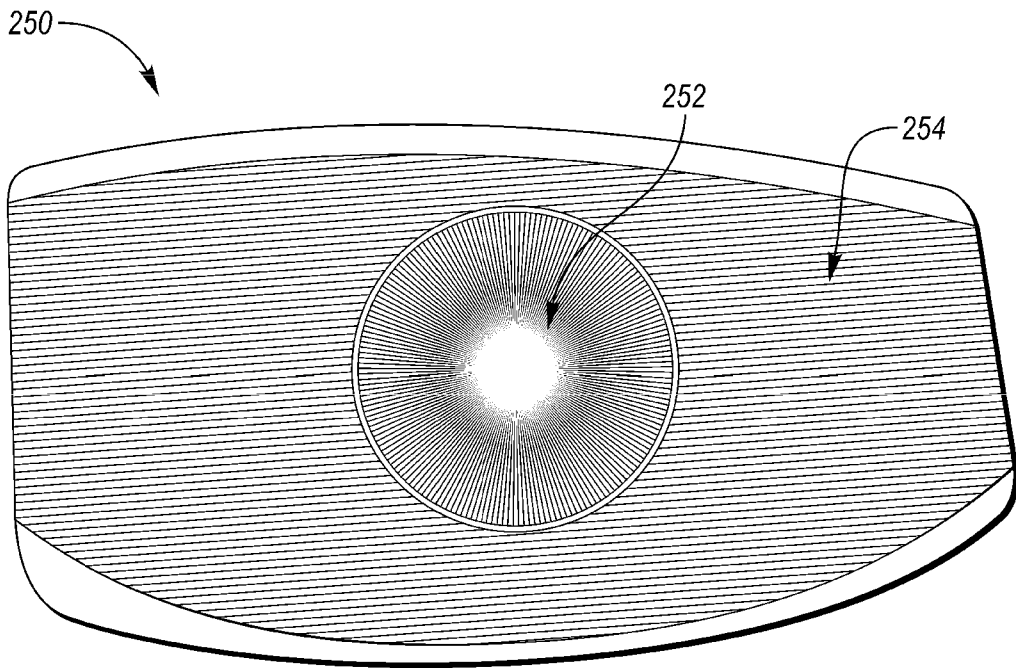


FIG. 5D

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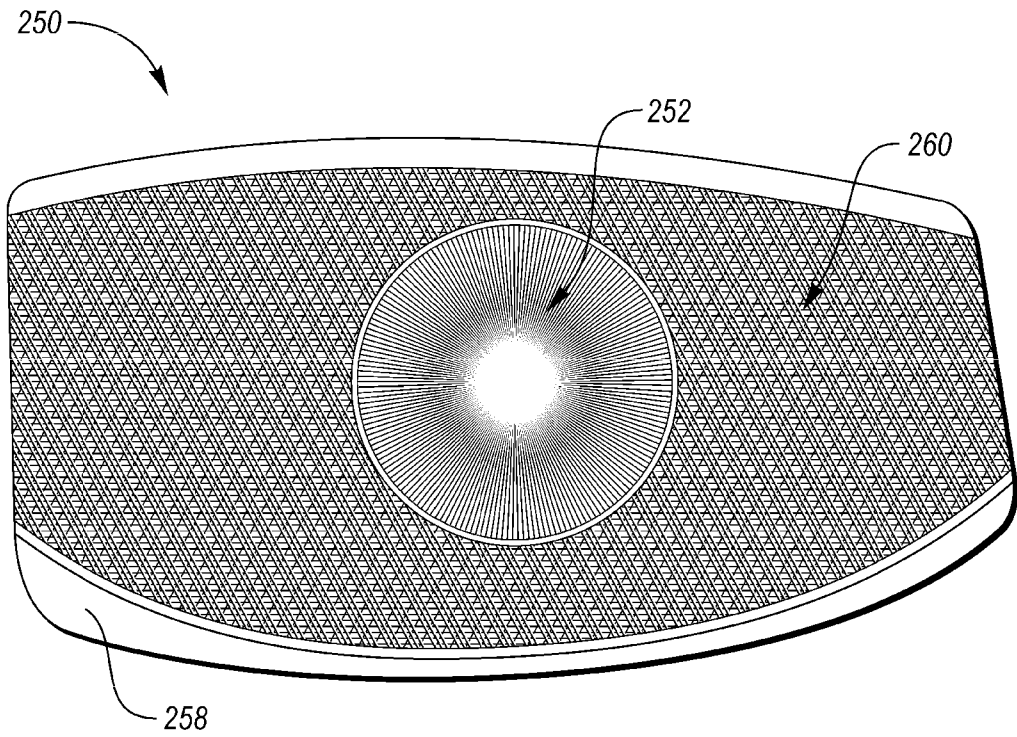


FIG. 5E

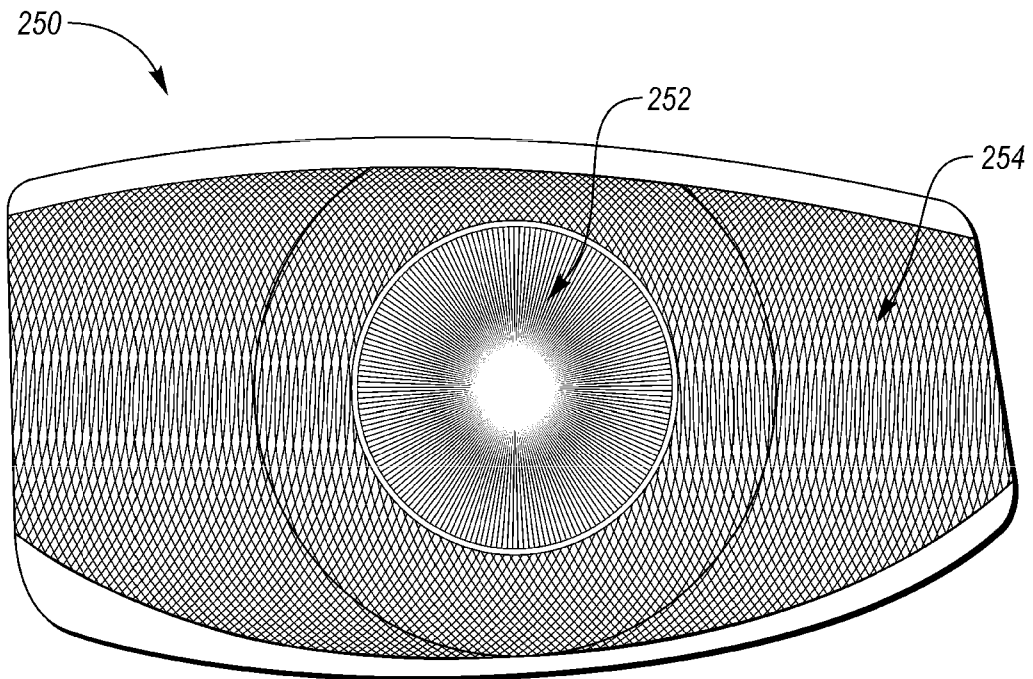


FIG. 5F

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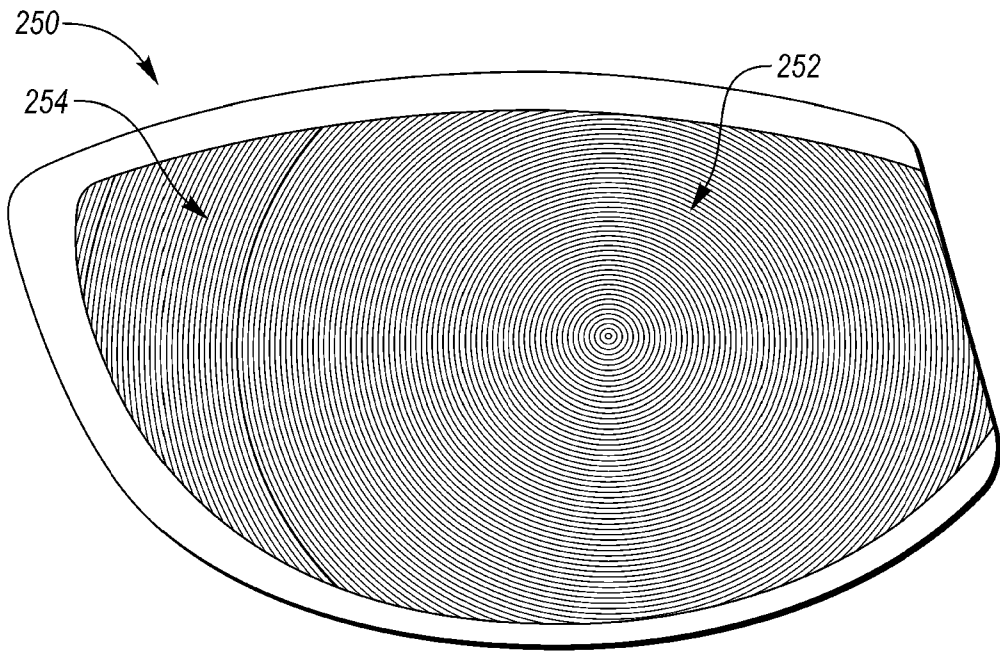


FIG. 5G

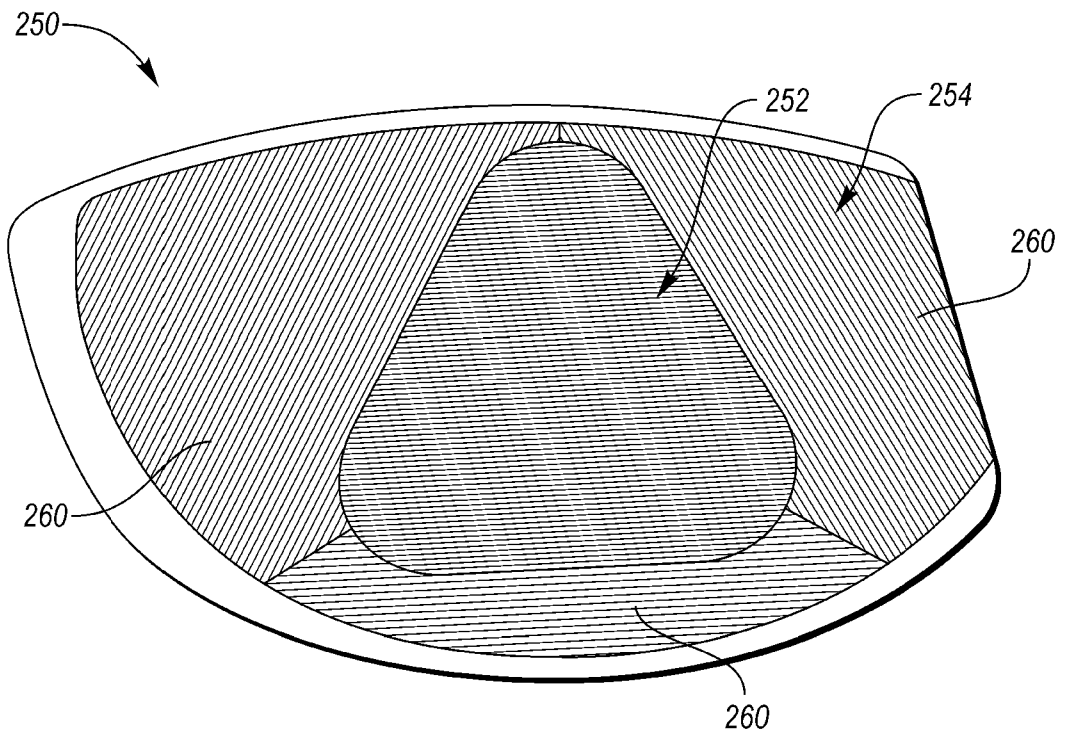


FIG. 5H

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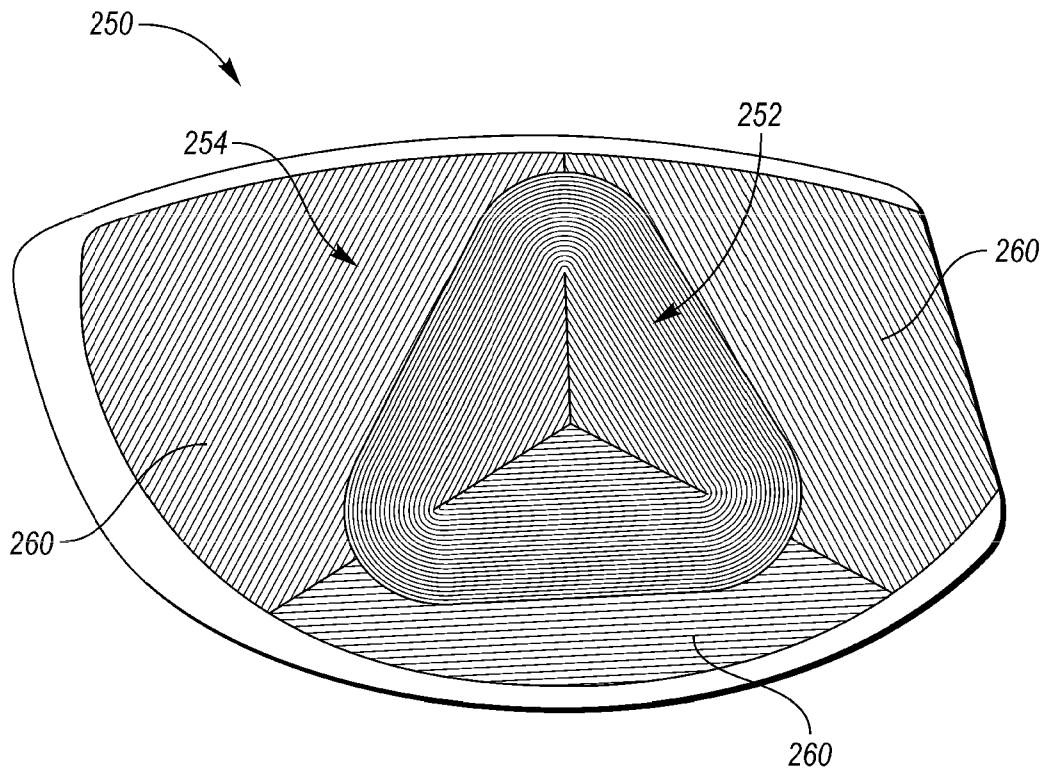


FIG. 5I

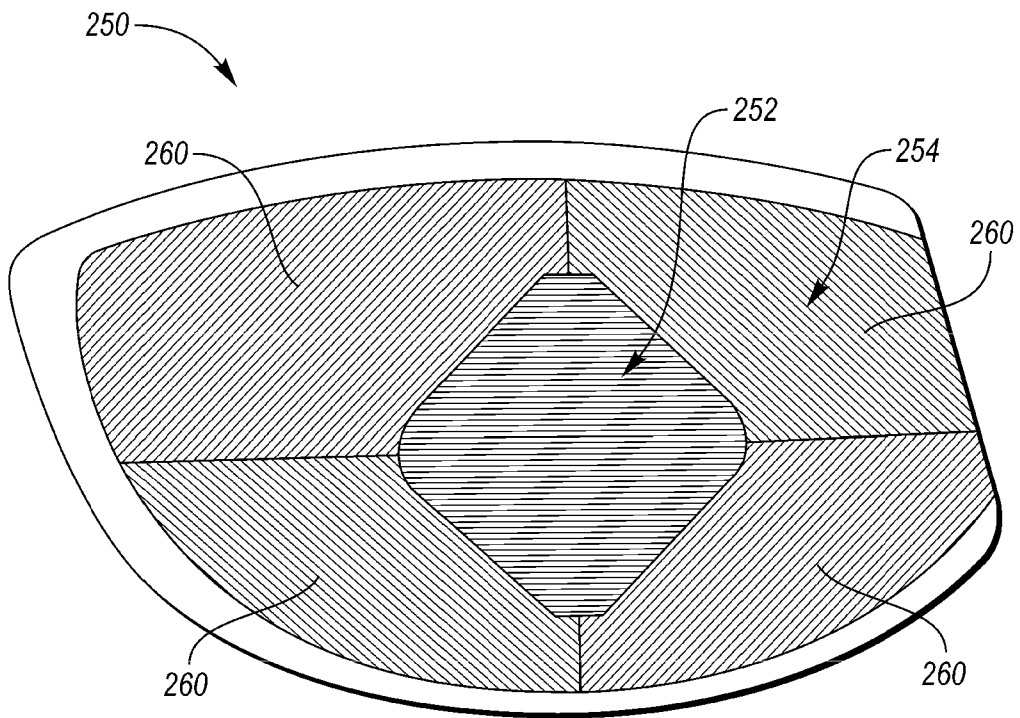


FIG. 5J

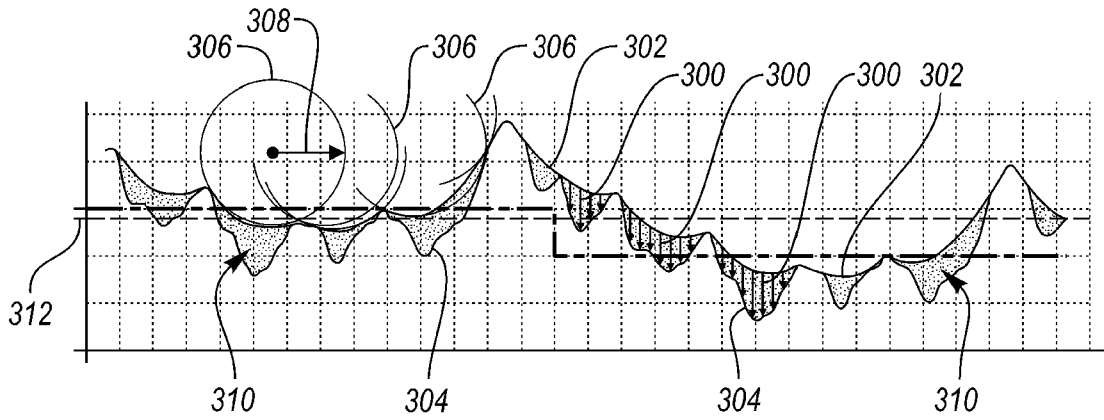


FIG. 6

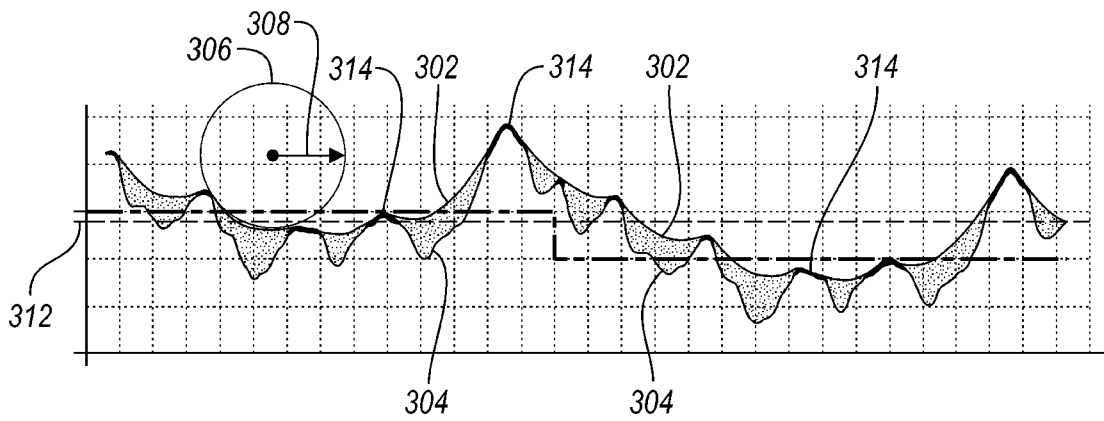


FIG. 7

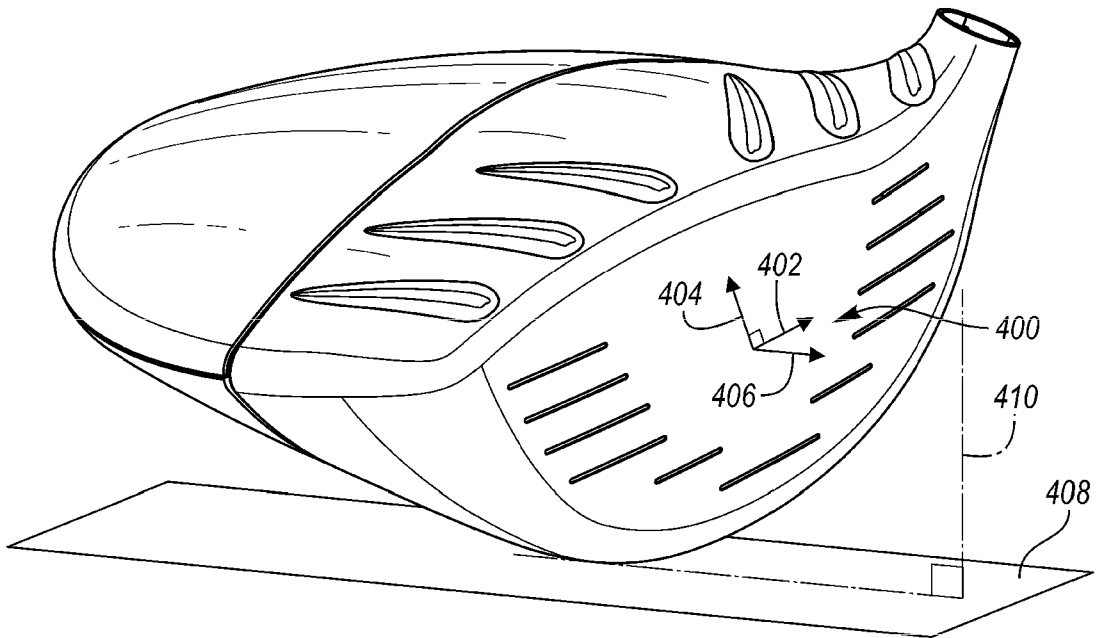


FIG. 7

LOCALIZED MILLED GOLF CLUB FACE

CROSS REFERENCE TO RELATED APPLICATIONS

[0001]

TECHNICAL FIELD

[0002] The present disclosure relates generally to a metal wood golf club having a milled ball striking surface and a set of golf clubs having milled faces.

BACKGROUND

[0003] Conventional metal wood golf club heads include a face and a body that extends rearward from the face. In some embodiments, the face may have a slightly rounded shape in order to provide a straighter and/or longer flight path for a golf ball, even when the ball is struck away from the center of the face. This rounded shape may be defined in terms of a bulge profile (curvature from a toe end to a heel end) and a roll profile (curvature from the crown edge to the sole edge).

[0004] Typical metal wood golf club heads may be formed by coining and/or machining a strike plate to have a pre-determined bulge and roll curvature, welding the strike plate within an opening provided within a forward frame, grinding away any weld bead that is outwardly exposed following the welding process, and then applying a uniform, brushed surface finish across the frame and strike plate. Such a process, however, can lead to rather large tolerances in the final product due to variability in the coining, welding, grinding, and finishing processes. As such, there is a need in the art to create a golf club with a face profile that can achieve much tighter bulge/roll tolerances to reduce the variability across multiple club heads of the same design. In addition, there is a need in low lofted club heads to reduce spin imparted on a golf ball to assist in increasing the carry distance and improving flight path of the golf ball.

[0005] Aspects of the invention will become apparent by consideration of the detailed description and accompanying drawings.

25 11 21

BRIEF DESCRIPTION OF THE DRAWINGS

- [0006]** FIG. 1 is a schematic perspective view of a golf club head.
- [0007]** FIG. 2 is a schematic partially exploded perspective view of the golf club head of FIG. 1.
- [0008]** FIG. 3 is a schematic diagram of a method of forming a golf club head.
- [0009]** FIG. 4 is a schematic diagram of a method of forming a golf club head.
- [0010]** FIG. 5A is a schematic front side view of a golf club head having a linear vertical milling pattern.
- [0011]** FIG. 5B is a schematic front side view of a golf club head having a linear horizontal milling pattern.
- [0012]** FIG. 5C is a schematic front view of a strike face having a circular center portion with a linear horizontal milling pattern and a peripheral portion with a milling pattern extending radially outward from the center portion.
- [0013]** FIG. 5D is a schematic front view of a strike face having a circular center portion with a milling pattern extending radially outward from a center and a peripheral portion with a linear horizontal milling pattern.
- [0014]** FIG. 5E is a schematic front view of a strike face having a circular center portion with a milling pattern extending radially outward from a center and a peripheral portion with a milling pattern having overlapping and intersecting linear milling marks.
- [0015]** FIG. 5F is a schematic front view of a strike face having a circular center portion with a milling pattern extending radially outward from a center and a peripheral portion with a milling pattern having overlapping and intersecting curvilinear milling marks.
- [0016]** FIG. 5G is a schematic front view of a strike face having a circular center portion with a concentric milling pattern extending radially outward from a center and a peripheral portion with a concentric milling pattern extending radially outward from the center portion.
- [0017]** FIG. 5H is a schematic front view of a strike face having a curved polygonal center portion with a linear horizontal milling pattern and a peripheral portion with a plurality of zones, each having a differently oriented linear milling pattern.

[0018] FIG. 5I is a schematic front view of a strike face having a curved polygonal center portion with a concentric milling pattern extending radially inward from an outer periphery and a peripheral portion with a plurality of zones, each having a differently oriented linear milling pattern.

[0019] FIG. 5J is a schematic front view of a strike face having a curved polygonal center portion with a linear horizontal milling pattern and a peripheral portion with a plurality of zones, each having a differently oriented linear milling pattern.

[0020] FIG. 6 is a graph that schematically illustrates the computation of the surface parameter W_{Void} .

[0021] FIG. 7 is a graph that schematically illustrates the computation of the surface parameter W_{VDCL} .

[0022] FIG. 8 is a schematic perspective view of a golf club head illustrating a face-centric coordinate system located at a geometric face center.

DETAILED DESCRIPTION

[0023] The present embodiments discussed below are generally directed to a golf club head, methods of making a golf club head, and/or coordinated sets of golf club heads that have milled surface textures across a forward ball striking surface for the purpose of affecting the spin imparted to a golf ball that is impacted by the club head.

[0024] Milling a golf club face has been shown to provide a more controlled and/or controllable surface profile, contour, and texture as compared with other golf club finishing techniques. When properly executed, it has been found that a milled surface texture may impart a greater amount of contact friction during the impact with a golf ball than other finishing techniques such as brushing. Unfortunately, milling is highly variable, and existing measures of surface roughness (e.g., average roughness (R_A)) do not properly explain differences between various milling patterns. As such, the present disclosure is further directed to milled ball striking surfaces that are characterized by newly developed surface parameters, which closely correlate to the amount of spin imparted to a golf ball by a low lofted club, such as a driver (i.e., where spin reductions in a low-lofted club may be indicative of increased contact friction at impact). Using these techniques, the presently disclosed milled faces have found a reduction in imparted spin

despite an approximately equal, or slightly decreased average roughness (R_A). This manner of characterizing a milled golf club face may further be employed to create faces that suit different design objectives (high backspin, low backspin, customized side-spin profiles (e.g., to augment the bulge profile of a driver), zonal milling patterns to affect off-center impacts, varying spin profiles as a function of loft, etc.

[0025] “A,” “an,” “the,” “at least one,” and “one or more” are used interchangeably to indicate that at least one of the item is present; a plurality of such items may be present unless the context clearly indicates otherwise. All numerical values of parameters (e.g., of quantities or conditions) in this specification, including the appended claims, are to be understood as being modified in all instances by the term “about” whether or not “about” actually appears before the numerical value. “About” indicates that the stated numerical value allows some slight imprecision (with some approach to exactness in the value; about or reasonably close to the value; nearly). If the imprecision provided by “about” is not otherwise understood in the art with this ordinary meaning, then “about” as used herein indicates at least variations that may arise from ordinary methods of measuring and using such parameters. In addition, disclosure of ranges includes disclosure of all values and further divided ranges within the entire range. Each value within a range and the endpoints of a range are hereby all disclosed as separate embodiment. The terms "comprises," "comprising," "including," and "having," are inclusive and therefore specify the presence of stated items, but do not preclude the presence of other items. As used in this specification, the term "or" includes any and all combinations of one or more of the listed items. When the terms first, second, third, etc. are used to differentiate various items from each other, these designations are merely for convenience and do not limit the items.

[0026] The terms "loft" or "loft angle" of a golf club, as described herein, refers to the angle formed between the club face and the shaft, as measured by any suitable loft and lie machine. The geometric center of the face, or “face center” is defined in terms of custom and convention for identifying the geometric center of the face. As is well understood, the face center is a location that is equidistant between the heel edge of the face and the toe edge of the face, and equidistant between the top edge of the face and the bottom edge of the face.

[0027] The terms "first," "second," "third," "fourth," and the like in the description and in the claims, if any, are used for distinguishing between similar elements and not necessarily for describing a particular sequential or chronological order. It is to be understood that the terms so used are interchangeable under appropriate circumstances such that the embodiments described herein are, for example, capable of operation in sequences other than those illustrated or otherwise described herein. Furthermore, the terms "include," and "have," and any variations thereof, are intended to cover a non-exclusive inclusion, such that a process, method, system, article, device, or apparatus that comprises a list of elements is not necessarily limited to those elements, but may include other elements not expressly listed or inherent to such process, method, system, article, device, or apparatus.

[0028] The terms "left," "right," "front," "back," "top," "bottom," "over," "under," and the like in the description and in the claims, if any, are used for descriptive purposes with general reference to a golf club held at address on a horizontal ground plane and at predefined loft and lie angles, though are not necessarily intended to describe permanent relative positions. It is to be understood that the terms so used are interchangeable under appropriate circumstances such that the embodiments of the apparatus, methods, and/or articles of manufacture described herein are, for example, capable of operation in other orientations than those illustrated or otherwise described herein.

[0029] The terms "couple," "coupled," "couples," "coupling," and the like should be broadly understood and refer to connecting two or more elements, mechanically or otherwise. Coupling (whether mechanical or otherwise) may be for any length of time, e.g., permanent or semi-permanent or only for an instant.

[0030] Other features and aspects will become apparent by consideration of the following detailed description and accompanying drawings. Before any embodiments of the disclosure are explained in detail, it should be understood that the disclosure is not limited in its application to the details or construction and the arrangement of components as set forth in the following description or as illustrated in the drawings. The disclosure is capable of supporting other embodiments and of being practiced or of being carried out in various ways.

Also, it is to be understood that the phraseology and terminology used herein is for the purpose of description.

[0031] Referring to the drawings, wherein like reference numerals are used to identify like or identical components in the various views, FIG. 1 schematically illustrates a perspective view of a wood-style golf club head 10 that includes a strike face 12 and a body 14 that cooperate to define a hollow internal club head volume 16 (shown in FIG. 2). As shown, the golf club head 10 further includes a toe portion 20, a heel portion 22, a rear portion 24, a crown 26, and a sole 28. While the present disclosure is generally made with respect to a wood-style club head, such as a driver, fairway wood, or hybrid iron, it should be understood that aspects of this disclosure, such as controlling face texture to affect contact friction and spin, may be equally applicable to iron-type golf clubs.

[0032] As generally illustrated in FIGS. 1-2, in some embodiments, the strike face 12 may include a strike plate 30 and a frame 32 that cooperate to define a continuous ball striking surface 34 (i.e., the portion of the club head 10 that is intended to directly impact a golf ball). In an embodiment, the strike plate 30 and frame 32 may be integrally formed from a singular piece of material. In some variations of this design, the frame 32 may sweep rearward away from the ball striking surface 34 to form a “cup face” portion of the club head.

[0033] In another embodiment, instead of being integrally formed, the strike plate 30 may generally be affixed within an opening 36 provided in the frame 32. For example, in some embodiments, the frame 32 may include a lip 38 or recessed shelf that extends around at least a portion of the perimeter of the opening 36. When assembled, the strike plate 30 may nest within the opening 36 such that a rear surface of the strike plate 30 abuts the lip 38 and such that the forward surface of the strike plate 30 is about flush with the forward surface of the frame 32. Once positioned within the opening 36, the strike plate 30 may then be affixed to the frame 32 around the entire perimeter/seam through an integral attachment technique such as welding.

[0034] In an embodiment where the strike plate 30 is formed separate from the frame 32, the strike plate 30 may undergo a coining process prior to being affixed within the opening 36. This coining process may impart a bulge and/or roll curvature to the ball

striking surface 34 to provide a margin of correction for off-center impacts through a dynamic response generally referred to as a “gear effect.”

[0035] During the coining process, a large force is applied to the strike plate 30 that plastically deforms the material into having the predetermined curvature (characterized by a bulge radius of curvature and a roll radius of curvature). In many embodiments, the bulge radius and the roll radius can be the same. In other embodiments, the bulge radius and the roll radius can be different. In the illustrated embodiment, both the bulge and roll have a radius of 12 inches (about 304.8 mm). In other embodiments, the bulge can have any radius of curvature. For example, in some embodiments, the bulge can have a radius of 4 in, 5 in, 6 in, 7 in, 8 in, 9 in, 10 in, 11 in, 12 in, 13 in, 14 in, 15 in, 16 in, 17 in, 18 in, 19 in, 20 in, 21 in, 22 in, 23 in, 24 in, 25 in, 26 in, 27 in, or 28 in (about 100 mm to about 720 mm). In the same or other embodiments, the roll can have any radius of curvature. For example, in some embodiments, the roll can have a radius of 4 in, 5 in, 6 in, 7 in, 8 in, 9 in, 10 in, 11 in, 12 in, 13 in, 14 in, 15 in, 16 in, 17 in, 18 in, 19 in, 20 in, 21 in, 22 in, 23 in, 24 in, 25 in, 26 in, 27 in, or 28 in (about 100 mm to about 720 mm).

[0036] The frame 32 and/or strike plate 30 may be formed from the same material or different materials, so long as they both are constructed with sufficient strength to withstand repeated impact stresses that occur when the club head 10 strikes a golf ball. Examples of suitable materials for the frame 32 and/or strike plate 30 include stainless steel or steel alloys (e.g., C300, C350, Ni (Nickel)-Co(Cobalt)-Cr(Chromium)-Steel Alloy, 565 Steel, AISI type 304 or AISI type 630 stainless steel), a titanium alloy (e.g., a Ti-6-4, Ti-3-8-6-4-4, Ti-10-2-3, Ti 15-3-3-3, Ti 15-5-3, Ti185, Ti 6-6-2, Ti-7s, Ti-92, or Ti-8-1-1 Titanium alloy), an amorphous metal alloy, aluminum alloys, or one or more high strength composite materials comprising, for example, plastic polymers and co-polymers, carbon fibers, fiberglass fibers or metal fibers.

[0037] The club head body 14 can be formed from the same material or a different material than the frame 32 and/or strike plate 30. In some embodiments, the material of the body 14, together with the design of the body structure, may provide a controlled dynamic impact response, which may affect launch angle, spin and ball speed. In some embodiments, the body 14 may be formed from stainless steel, titanium,

aluminum, steel alloys, titanium alloys, carbon fiber composites, molded filled or unfilled engineering plastics/polymers, or combination thereof.

[0038] FIG. 3 illustrates a first method 100 for forming the golf club head assembly 10. This first method 100 includes a first step 102 of forming the strike plate 30 and the club head body 14. The strike plate 30 and/or club head body 14 may be formed using processes such as machining, casting, stamping, injection molding (metal and/or polymer), direct laser sintering, powder metal forming processes, or other appropriate process known to those skilled in the art.

[0039] Once formed into a general shape, the strike plate blank may then be coined in step 104. As noted above, coining is form of precision stamping, wherein the strike plate 30 is subjected to a high force causing it to plastically deform. The coining process is used to create the bulge and roll radius described above.

[0040] The strike plate 30 may then be milled or machined in step 106 to provide a precision contour and surface texture. The machining process uses a rotary cutter to remove material from the strike plate 30 and is generally performed using a CNC system to control the process.

[0041] Once machined, the strike plate 30 may then be welded into the opening 36 of the frame 32 in step 108. The strike plate 30 is aligned with the opening 36 of the frame 32 and abuts the lip 38. The strike plate 30 is secured to the frame 32 by welding along the perimeter of the opening 36 forming the golf club head 10. In some embodiments, the welding step may utilize a pulse plasma or laser welding process.

[0042] Following the welding process in step 108 the weld line and any protruding weld bead may be removed through a grinding process in step 110. The grinding process involves a rotating abrasive wheel used to remove material along the weld line. The grinding process can also ensure that the bulge and roll radius of the frame 32 matches the bulge and roll radius of the strike plate 30 created during coining and machining steps 104, 106. A golf club head assembly 10 formed from the method 100 illustrated in FIG. 3 will include a strike face 12 that has at least two different surface finishes (i.e., the original and/or ground finish of the frame 32 and the machined/milled finish of the strike plate 30).

[0043] FIG. 4 schematically illustrates a second method 200 for forming a golf club head 10. The method 200 illustrated in FIG. 4 is similar in many respects to the first method 100 illustrated in FIG. 3, except the machining/milling of step 106 is performed after the strike plate 30 is welded to the frame 32 in step 108. In doing so, the grinding process of step 110 may be optionally removed, and the surface texture of the strike plate 30 may be optionally extended across the frame 32 in a continuous manner.

[0044] The second method 200 generally begins by forming the strike plate 30 and golf club head body 14 in step 202, such as by machining, casting, stamping, injection molding (metal and/or polymer), direct laser sintering, powder metal forming processes, or other appropriate process known to those skilled in the art. The strike plate 30 may then be coined in step 204, as described above in step 104 of FIG. 3.

[0045] The coined strike plate 30 may then be welded into the opening 36 provided in the frame 32 in step 206. Any remaining weld bead/line may then be optionally removed via a grinding process 208 (illustrated in phantom to indicate that this process is not a strictly required step). And finally, the entire ball striking surface 34 may be machined/milled in step 210. In some embodiments, this machining step 210 may be operative to remove any weld bead that was not removed via optional step 208.

[0046] By machining/milling across the entire ball striking surface 34, this manufacturing method 200 may create a surface texture with no or little regard for the specific location of the weld line/perimeter of the strike plate 30. For example, the surface texture may be uniform and continuous across both the strike plate 30 and frame 32, may continuously vary as a function of a distance from face center, or take any other pattern as may be found desirable. Most importantly, these milling patterns need not be constrained by the size and location of the strike plate perimeter.

[0047] Milling or machining the entire strike face 12, such as through the second method 200 of FIG. 4, provides an additional benefit of further tightening/reducing the profile/curvature tolerances for the bulge and roll radius (i.e., to provide a more precise curvature). Having the textured surface across the entire strike face 12 while maintaining a lower tolerance for the bulge and roll radius can create a higher performing club head assembly 10 that provides greater distance, spin control, and forgiveness.

Surface Texture

[0048] In a general sense, a milled strike plate 30 has a surface texture that can be characterized by one or more directional cutting patterns and a surface texture that is directionally dependent. Typical milling processes utilize a rotary cutting tool to remove material from the strike plate 30. This process can be automated using a Computer Numerical Control (CNC) system to provide enhanced precision, consistency, and repeatability across multiple club heads. Furthermore, the CNC machining process can ensure that a predominant pattern direction, surface texture, and overall face contour precisely match the predetermined specifications. This level of enhanced precision is desirable because it has been found that the predominant pattern direction and surface texture on the strike plate 30 can meaningfully impact the spin characteristics on the golf ball after impact. Therefore, given the level of manufacturing control and repeatability that is afforded by CNC milling, it is possible to customize the textured surface on the strike plate 30 to an individual's swing type, which may result in longer and straighter ball flight patterns.

[0049] A typical milling pattern may resemble a plurality of grooves that are concentrically or linearly cut into the outer surface. These patterns may more specifically comprise a plurality of primary peaks and primary valleys that each extend along a linear or curvilinear path. In some embodiments where milling paths overlap, each primary peak may include a plurality of secondary valleys that are disposed in a regular pattern along at least a portion of the length of the peak, and each primary valley may include a plurality of secondary peaks that are disposed in a regular pattern along at least a portion of the length of the valley. In some embodiments of the present designs, and depending on the direction along the striking plate surface you measure, the plurality of peaks and valleys (measured from a mid-plane of the peaks and valleys) can range from -100 μ -in to 100 μ -in (about -2.54 μ m to about 2.54 μ m), -140 μ -in to 140 μ -in (about -3.56 μ m to about 3.56 μ m), -200 μ -in to 200 μ -in (about -5.08 μ m to about 5.08 μ m), -500 μ -in to 500 μ -in (about -12.7 μ m to about 12.7 μ m), -700 μ -in to 700 μ -in (about -17.78 μ m to about 17.78 μ m), -1000 μ -in to 1000 μ -in (about -25.4 μ m to about 25.4 μ m), -1400 μ -in to 1400 μ -in (about -35.56 μ m to about 35.56 μ m), or more.

[0050] While in some embodiments, the surface texture across the ball striking surface 34 may be uniform across the entire strike plate 30, in other embodiments, however, the ball striking surface 34 may have a surface texture that functionally varies across the strike face 12. For example, in an embodiment, the surface texture may vary from a center region of the strike plate 30 towards the perimeter of the strike plate 30. In some embodiments, the surface roughness can vary on the strike plate 30 from near the toe portion 20 of the club head 10 to near the heel portion 22 of the club head 10. In other embodiments, the surface roughness can vary on the strike plate 30 from near the sole 28 of the club head 10 to near the crown 26 of the club head 10. In still other embodiments, surface roughness can vary in any combination of the aforementioned examples. In still other embodiments, surface roughness can be uniform in certain areas of the strike plate 30, and vary in other areas of the strike plate 30. In an embodiment, the textured surface of the strike plate 30 may have a uniform roughness of about 148 μ -in (about 3.76 μ m). In other embodiments, the textured surface can have a surface roughness between about 50 μ -in and about 300 μ -in (between about 1.27 μ m and about 7.62 μ m). In some embodiments, the textured surface can have a surface roughness between 25-350, 25-50, 50-75, 75-100, 75-100, 100-125, 125-150, 150-175, 175-200, 200-225, 225-250, 250-275, 275-300, 300-325 μ -in, 25-150, 150-350, 75-250, 25-125, 125-225, 225-350, 75-150, 150-225, or 225-300. In other embodiments, the roughness can be 25, 50, 75, 100, 125, 150, 175, 200, 225, 250, 275, 300, 325, or 350 μ -in. In still other embodiments, the surface roughness can be between about 140 μ -in and about 300 μ -in (between about 3.56 μ m and about 7.62 μ m).

[0051] As generally illustrated in FIGS. 5A-5J, the predominant pattern direction of the textured surface in any particular area may comprise one or more linear, curvilinear, or intersecting patterns to form a milling pattern 250. In some embodiments, these patterns may extend somewhat uniformly across the entire strike face 12. In other embodiments, however, these patterns may be zonal, or may vary across the face due to a curvilinear and concentric nature. In some embodiments, the milling pattern 250 may comprise a center portion 252 that is surrounded by a peripheral portion 254, such as shown in FIGS. 5C-5J. The milling profiles illustrated in FIGS. 5A-5J are examples of different milling patterns 250 that may be employed to meet different design objectives,

as will be discussed below. It should be appreciated that additional designs may be developed by combining aspects of each figure, and every combination of pattern and shape for the center portion 252 and pattern and shape of the peripheral portion 254 is regarded as a separate embodiment, even if not illustrated.

[0052] As schematically shown in FIG. 5A, in an embodiment, a milling pattern 250 may include a plurality of peaks and valleys that are oriented in a linear manner between the crown 26 and the sole 28. FIG. 5B then illustrates an embodiment where this pattern is turned 90 degrees and extends between the heel portion 22 and toe portion 20. FIGS. 5A-5B further illustrate a channel 256 that may be disposed around a perimeter of the milling pattern 250 to provide a more clear transition between the milling pattern 250 and the remainder of the club 10. As further shown in FIGS. 5A-5B, in some embodiments, an edge portion 258 of the forward most surface (i.e. the ball striking surface 34), may not include the milling texture. Such a surface may instead be polished or sandblasted to more readily blend into the body.

[0053] FIG. 5C-5J more clearly illustrate examples of milling patterns 250 that have different variations of a center portion 252 and a peripheral portion 254. As shown in FIGS. 5C-5G, in some embodiments, the center portion 252 may be round. In other embodiments, such as shown in FIGS. 5H-5J, the center portion 252 may have a rounded polygonal design, such as a rounded triangle or a rounded square (or a rounded pentagon, hexagon, heptagon, octagon, or the like). As further illustrated in FIGS. 5C-5J, the milling pattern 250 within the center portion 252 may comprise a linear pattern (FIGS. 5C, 5H, and 5J), a concentric pattern, for example, beginning at an outer perimeter of the center portion 252 (FIGS. 5G and 5I), or a radial pattern originating from a point, line, or area (FIGS. 5D-5F).

[0054] The peripheral portion 254 may comprise one or more zones 260 between which the milling pattern may change direction/orientation, change type, or begin anew. For example, FIGS. 5H-5J illustrate three peripheral designs that include a plurality of zones 260, where a linear pattern is rotated between each zone 260. FIG. 5C illustrates an emanating ray pattern (i.e., where the milling lines emanate linearly from a central point or area. FIG. 5D illustrates a linear arrangement across the peripheral portion 254. FIG. 5E illustrates an intersecting linear arrangement (i.e., where a first linear

arrangement is cut, and then a second linear arrangement in a second orientation is cut over top of the first linear arrangement). FIG. 5F illustrates intersecting curvilinear arrangements (i.e., where the first curvilinear arrangement is cut from toe to heel, and the second is cut from heel to toe – note that similar arrangements may be made by cutting from crown to sole and sole to crown, or from various corners). FIG. 5G illustrates a concentric pattern emanating from a central point or area.

[0055] In some embodiments, the strike face 12 of the golf club head assembly 10 can comprise two or more different surface finishes/textures. For example, as described above with respect to FIG. 3, the strike plate 30 can be milled or machined, creating a first surface finish prior to being welded to the opening 36 of the frame 32. The remaining portion of the strike face 12 which was not milled may then have a second surface finish, such as a smooth or sand blasted surface finish. Having the different textured surfaces on the strike face 12 can provide the player with a visual alignment aid to help position the golf ball at the center of the strike face 12. In other embodiments, the entire ball striking surface 34 (including the frame 32 and strike plate 30) can comprise the textured surface from the milling or machining process.

[0056] While a milled face is beneficial in terms of providing a more controlled face curvature, the surface texture and milling pattern created by the tool can introduce a considerable amount of variability in the resulting spin and launch characteristics of an impacted ball. For example, two clubs with milling patterns oriented 90 degrees apart may produce significantly different ball launch characteristics. Furthermore, even if patterns are oriented similarly, differences in the feed rate, cutting depth, tool diameter, end profile, and the tool spindle speed used to create the pattern can introduce variations in the surface texture that affect ball flight.

[0057] Through testing, it has been found that traditional measures of surface roughness do not appear to properly characterize the effects of different surface textures and/or milling patterns. For example, Table 1 illustrates 4 identical driver designs (i.e., similar volume, mass distribution, structure, and loft), one with a traditional brushed surface finish across the strike face 12 (i.e., the control club), and three with different milled surface finishes across the strike face 12. For each club, the average surface

roughness (R_A) was measured along a vertical line extending through the geometric center of the face (i.e. from sole 28 to crown 26).

Table 1: Imparted backspin for different driver face surface roughness

Club	R_A (μ -inch)	Spin (rpm)
Driver - Brushed	147	3005
Driver - Milled 1	144	2683
Driver - Milled 2	221	2840
Driver - Milled 3	284	2817

[0058] In this analysis, the first milled face (milled 1) attempted to match the average roughness of the brushed surface finish as closely as possible. Despite the close average roughness, the milled face produced about 10.7% less spin than the brushed face. This decrease in spin rate was an unexpected result. Then, milled faces 2 and 3 were constructed to increase the average roughness, as the prevailing belief was that, as average roughness increases, spin imparted by a driver should decrease. Milled faces 2 and 3, however, both resulted in about 5% more spin than the lower roughness milled face (milled 1). From this analysis, it was determined that average surface roughness may not be suitable to fully characterize the spin-effects caused by the surface texture of a driver face (which is counter to the prevailing understanding).

[0059] Following additional investigation, a new manner of characterizing the surface texture of a strike face has been developed to more effectively predict the resulting spin imparted to a golf ball by a strike face. Furthermore, embodiments of the present design utilize this new characterization to provide a golf club with a face that is optimized to meet one or more spin-based design objectives.

[0060] Two new surface parameters have been found to more accurately characterize how the surface texture of a golf face may affect the spin of an impacted golf ball. These parameters include: (1) the ratio of R_A to a surface void parameter referred to as W_{Void} (described below); and (2) the value of a surface contact parameter referred to as

W_{VDCL} (also described below). To eliminate any ambiguity R_A , W_{Void} , and W_{VDCL} are defined as follows:

[0061] $R_A - A_s$ is known in the art, R_A represents an arithmetic average value of absolute surface deviations relative to a mean center line. In practice, the deviations and mean center line are computed following the application of a high-pass filter with a cut-off selected to eliminate surface waviness. In the present designs, a suitable cut-off wavelength may be about 0.03 inches (about 0.762 mm).

[0062] $W_{Void} - A_s$ generally illustrated in FIG. 6, W_{Void} is a parameter that has been developed to represent the average profile void depth 300 relative to a reference surface 302 that is created by applying a morphological closing filter to the actual surface profile 304. Morphologic closing is generally an image processing technique that may be best analogized as a disc 306 (in 2D) or sphere (in 3D) of a predetermined radius 308 (i.e., radius of curvature) being theoretically rolled across the actual surface profile 304. The lower envelope formed by the rolling disc then generates the “closed” reference surface 302. In a two-dimensional context, such as illustrated in FIG. 5, W_{Void} may be calculated by summing the total void area 310 between the closed reference surface 302 the actual surface profile 304 and dividing that aggregated area by the length of the surface (i.e., the length of a mean center line 312).

[0063] $W_{VDCL} - A_s$ generally illustrated in FIG. 7, W_{VDCL} is a parameter that has been developed to represent the ratio of the contact length 314 (in 2D) or area (in 3D) between the closed reference surface 302 (as described above with respect to W_{Void} and FIG. 5) and the actual surface profile 304, to the length (in 2D) or area (in 3D) of the surface itself (i.e., measured along a mean center line 312). For a perfectly flat surface, W_{VDCL} would equal 1.0; for a wavy surface (e.g., where the radius of curvature 308 of the disc/sphere is smaller than any external radius of curvature of the surface), W_{VDCL} may be greater than 1.0; and, for a surface with a rather fine texture (e.g., where the radius of curvature 308 of the disc/sphere is greater than an external radius of curvature for a portion of the surface), W_{VDCL} may be less than 1.0.

[0064] When computing R_A , W_{Void} , and W_{VDCL} , each parameter may be calculated in a number of directionally dependent manners. More specifically, the surface profiles illustrated in FIGS. 6 and 7 may be presumed to have been taken from a

2-D cutting plane through a strike face 12, similar to the strike face 12 shown in FIG. 1. If this cutting plane is oriented perpendicular to the dominant milling grooves, all three surface parameters may differ from measurements where the cutting plane is oriented parallel to the milling grooves, which may differ still from a 3D computation where any closed reference surface is generated by a theoretical sphere.

[0065] For the purpose of this disclosure, a face-centric coordinate system 400, such as shown in FIG. 8 may be utilized to better explain how the parameters are derived. As shown in FIG. 8, the face-centric coordinate system 400 may have an origin that is coincident with the geometric face center, X and Y axes 402, 404 that are each tangential to the ball striking surface 34 at the face center, and a Z-axis 406 that is normal to the ball striking surface at 34 the face center. The X-axis 402 may further be parallel to a ground plane 408 when the club is held at address according to prescribed loft and lie angles, and may generally extend between the heel and the toe. The Y-axis 404 is orthogonal to the X-axis 402, and is generally the projection of a vertical reference line 410 onto the ball striking surface 34 when the club is held at address.

[0066] When computing the various parameters, each may be computed along a 2D line (e.g., computed within a single 2D slice taken in the Y-Z plane), averaged across a plurality of 2D lines (e.g., averaged across a plurality of 2D slices taken in adjacent Y-Z planes), or computed in 3D across the entire face (i.e., not directionally-dependent).

[0067] It is believed that R_A/W_{Void} and W_{VDCL} both provide slightly different approximations of the amount of surface area that a golf ball may directly contact (at a microscopic level) during an impact (i.e., thus providing a more accurate estimation of the actual contact friction experienced between the ball and the face during an impact). More specifically, the “closed” reference surface 302 may approximate a compliant object (i.e., a polymeric, compressible golf ball) that is in forcible contact with the surface texture and deforms about the peaks. Based on this assumption, the compliant object (golf ball) never contacts certain portions of the voids/valleys; thus, the depth and/or size of the non-contacted portions is largely irrelevant to the effective force transfer and contact friction between the ball and the strike face 12. Despite these voids being largely irrelevant, they can significantly affect traditional measures of surface roughness. Under these assumptions, as R_A/W_{Void} and W_{VDCL} increase, contact friction

should also increase, which should then decrease the imparted spin for a low-lofted club such as a driver. As illustrated through the following comparative examples, empirical testing data supports this understanding:

Ratio of R_A to W_{Void} :

[0068] Using a high pass filter for R_A of about 0.03 inches (about 0.762 mm), and a radius of curvature for W_{Void} of about 0.005 inches (about 0.127 mm) to create the reference surface 302, it has been found that the ratio of R_A to W_{Void} correlates to the amount of spin imparted to an impacted golf ball by a low lofted golf club, such as a driver. More specifically, as R_A / W_{Void} increases, imparted spin decreases, such as generally illustrated in Table 2. The figures in Table 2 were all calculated within a Y-Z cutting plane that passed through face center for drivers with similar overall geometries, constructions, and mass properties.

Table 2: Imparted backspin for driver surface textures having different values of R_A / W_{Void}

Club	R_A (μ ·inch)	W_{Void} (μ ·inch)	R_A/W_{Void}	Spin (rpm)
Driver – Brushed	147	54	2.7	3005
Driver – Milled 1	144	18	8.0	2683
Driver – Milled 2	221	33	6.7	2840
Driver – Milled 3	284	36	7.89	2817

[0069] As shown in Table 2, while the R_A values between the brushed face and the “Milled 1” face are about equal, the ratio of R_A/W_{Void} for these faces is quite different and more predictive of imparted spin.

W_{VDCL}

[0070] Using a radius of curvature for W_{VDCL} of about 0.02 inches (about 0.508 mm) to form the reference surface 302, it has been found that the value of W_{VDCL}

correlates to the amount of spin imparted to an impacted golf ball by a low lofted golf club, such as a driver. More specifically, as W_{VDCL} increases, imparted spin decreases, such as generally illustrated in Table 3. The figures in Table 3 were all calculated within a Y-Z cutting plane that passed through face center for drivers with similar overall geometries, constructions, and mass properties.

Table 3: Imparted backspin for driver surface textures having different values of W_{VDCL}

Club	R_A (μ ·inch)	W_{VDCL}	Spin (rpm)
Driver – Brushed	147	22%	3005
Driver – Milled 1	144	29%	2683
Driver – Milled 2	221	24%	2840
Driver – Milled 3	284	26%	2817

Club Face Designs

[0071] While the above-referenced characterizations of surface texture may be utilized to characterize the spin-effects of surface textures formed by various techniques (e.g., brushing, milling, sandblasting, etc.), milling may provide the most control of the resulting texture in three dimensions across the face. As such, a golf club head 10 may include a milled ball striking surface 34 that has a surface texture characterized by a R_A to W_{Void} ratio and/or by a W_{VDCL} value that is customized to suit a particular design objective. Note that for all examples described below, any numeric values assume a 0.03 inch (about 0.762 mm) high-pass cutoff filter for R_A , a 0.005 inch (about 0.127 mm) radius of curvature for creating the reference surface for W_{Void} , and a 0.02 inch (about 0.508 mm) radius of curvature for creating the reference surface for W_{VDCL} .

[0072] In a first embodiment, a low-lofted club, such as a low-loft driver (i.e., having a loft angle of from about 8 to about 14 degrees, or from about 8 to about 12 degrees, or from about 8 to about 10 degrees), may be specifically designed to have a low backspin tendency by including a milled strike face with surface texture characterized by an R_A to W_{Void} ratio, measured in a Y-Z plane through the face center, that is greater than

about 4, or greater than about 5, or greater than about 6, or greater than about 7, or greater than about 8, greater than about 9, or greater than about 10. In some embodiments, the R_A to W_{Void} ratio can range from 4 to 12, 4 to 8, 8 to 12, 6 to 10, 4 to 6, 36 to 8, 8 to 10, or 10 to 12. For example, the R_A to W_{Void} ratio can be 4, 6, 8, 10, or 12. Additionally, or alternatively, this low-spin driver face surface texture may be characterized by a W_{VDCL} value, measured in a Y-Z plane through the face center, that is greater than about 18%, or greater than about 20%, or greater than about 22%, or greater than about 24%, or greater than about 26%, or greater than about 28%, or greater than about 30%. In some embodiments, the W_{VDCL} value can range from 18% to 33%, 18% to 24%, 24% to 36%, 24% to 30%, 30% to 36%, or 27% to 33%. For example, the W_{VDCL} value can be 18%, 20%, 22%, 24%, 26%, 28%, 30%, 32%, 34%, or 36%.

[0073] In a second embodiment, a metal wood intended to induce a greater amount of loft (i.e., having a loft angle of from about 12 degrees to about 28 degrees, or from about 14 degrees to about 24 degrees) may be specifically designed to have a higher backspin tendency by including a milled strike face with a surface texture characterized by an R_A to W_{Void} ratio, measured in a Y-Z plane through the face center, that is less than about 4, or less than about 3, or less than about 2, or within a range of from about 1 to about 4, or from about 2 to about 4. Additionally, or alternatively, this higher-spin face surface texture may be characterized by a W_{VDCL} value, measured in a Y-Z plane through the face center, that is less than about 24%, or less than about 22%, or less than about 20%, or less than about 18%, or within a range of from about 20% to about 24%.

[0074] In either of these embodiments, instead of simply being a single reading, the R_A to W_{Void} and W_{VDCL} values may be an average of the values across a plurality of Y-Z slices. For example, these values may be averaged across a center strip, region, or portion of the face 12. For example, these values may be averaged across a 1.68 inch (42.67 mm) impact zone, measured along the X-axis, and centered about face center. Likewise, in some variations, these low or high backspin surface textures may be localized within a center portion 252 of the face, such as within a 1.68 inch diameter circle centered about the face center. Alternatively, these values may be averaged across a narrower center portion of the impact zone that may measure about 0.375 inches (about 9.53 mm) along the X-axis or in diameter.

[0075] In an embodiment, in an effort to maximize contact friction in a heel-toe direction, a strike face 12 may include a milled surface texture characterized by an R_A to W_{Void} ratio, measured in an X-Z plane through the face center, that is greater than about 4, or greater than about 5, or greater than about 6, or greater than about 7, or greater than about 8, greater than about 9, or greater than about 10. Additionally, or alternatively, this surface texture with directionally increased contract friction may be characterized by a W_{VDCL} value, measured in an X-Z plane through the face center, that is greater than about 18%, or greater than about 20%, or greater than about 22%, or greater than about 24%, or greater than about 26%, or greater than about 28%, or greater than about 30%. In some embodiments, the W_{VDCL} value can range from 18% to 33%, 18% to 24%, 24% to 36%, 24% to 30%, 30% to 36%, or 27% to 33%. For example, the W_{VDCL} value can be 18%, 20%, 22%, 24%, 26%, 28%, 30%, 32%, 34%, or 36%.

[0076] Alternatively, to minimize the contact friction in a heel-toe direction a strike face 12 may include a milled surface texture characterized by an R_A to W_{Void} ratio, measured in an X-Z plane through the face center, that is less than about 4, or less than about 3, or less than about 2, or within a range of from about 1 to about 4, or from about 2 to about 4. Additionally, or alternatively, this surface texture with directionally decreased contract friction may be characterized by a W_{VDCL} value, measured in an X-Z plane through the face center, that is less than about 24%, or less than about 22%, or less than about 20%, or less than about 18%, or within a range of from about 20% to about 24%.

[0077] While the above-described embodiments discuss increasing contact friction (which decreases backspin in a driver) in/around the center of the strike face 12, in other embodiments, contact friction may be promoted or discouraged in other locations or areas about the strike face 12 via changes in the surface texture. For example, the surface texture in a peripheral region (or peripheral portion 254) of the strike face 12 (e.g., outside of the central region or narrower, center portion 252) may be controlled to provide enhanced forgiveness, alter spin profiles, and/or to offset other design parameters of the club head 10.

[0078] In one embodiment, contact friction may be increased in the peripheral region by providing an R_A to W_{Void} ratio, measured in the Y-Z plane and/or in the X-Z

plane and averaged across at least a portion of the peripheral region, of greater than about 4, or greater than about 5, or greater than about 6, or greater than about 7, or greater than about 8, greater than about 9, or greater than about 10. Additionally, or alternatively, this increased friction peripheral region may have a surface texture characterized by a W_{VDCL} value, measured in the Y-Z plane and/or in the X-Z plane and averaged across at least a portion of the peripheral region, that is greater than about 18%, or greater than about 20%, or greater than about 22%, or greater than about 24%, or greater than about 26%, or greater than about 28%, or greater than about 30%. In some embodiments, the W_{VDCL} value can range from 18% to 33%, 18% to 24%, 24% to 36%, 24% to 30%, 30% to 36%, or 27% to 33%. For example, the W_{VDCL} value can be 18%, 20%, 22%, 24%, 26%, 28%, 30%, 32%, 34%, or 36%. The increased friction peripheral region, may specifically include one or more of an increased friction portion abutting the sole 28, an increased friction portion abutting the toe portion 20, an increased friction portion abutting the crown 26, and/or an increased friction portion abutting the heel portion 22.

[0079] In some embodiments, the increased contact friction in the peripheral region may be used to, for example, provide additional design flexibility in altering the bulge and/or roll radius of curvature of the strike face 12 or the center of gravity of the club head 10, or in increasing the forgiveness to certain impacts.

[0080] In an embodiment, contact friction may be decreased in the peripheral region by providing an R_A to W_{Void} ratio, measured in the Y-Z plane and/or in the X-Z plane and averaged across at least a portion of the peripheral region, of less than about 4, or less than about 3, or less than about 2, or within a range of from about 1 to about 4, or from about 2 to about 4. Additionally, or alternatively, this decreased friction peripheral region may have a surface texture characterized by a W_{VDCL} value, measured in the Y-Z plane and/or in the X-Z plane and averaged across at least a portion of the peripheral region, that is less than about 24%, or less than about 22%, or less than about 20%, or less than about 18%, or within a range of from about 20% to about 24%. The decreased friction peripheral region, may specifically include one or more of a decreased friction portion abutting the sole 28, a decreased friction portion abutting the toe portion 20, a decreased friction portion abutting the crown 26, and/or a decreased friction portion abutting the heel portion 22.

[0081] In some embodiments, an average R_A to W_{Void} ratio and/or W_{VDCL} value from within the central region or narrower, center portion 252 of the strike face 12 may be different than the average R_A to W_{Void} ratio and/or W_{VDCL} value from within a portion of the peripheral region of the strike face 12. In another embodiment, the R_A to W_{Void} ratio and/or W_{VDCL} value may vary as a function of an increasing distance from the geometric center of the strike face 12. In an embodiment, an average R_A to W_{Void} ratio and/or W_{VDCL} value (measured in one or both of the Y-Z plane and the X-Z plane) may be greater proximate the toe portion 20 and/or heel portion 22 than in the center of the strike face 12.

[0082] In practice, the R_A to W_{Void} ratio and W_{VDCL} value for a particular face may be customized during a milling process by altering one or more of the tool (e.g., a ball end mill, a square end mill, or a corner round end mill), the angle of the tool relative to the face (e.g., from greater than about 0 degrees relative to the face to about 90 degrees), the cutting speed (e.g., from about 60 to about 300 inches per minute for titanium, or from about 300 to about 1000 inches per minute for steel), the stepover (e.g., from about 0.005 inch to about 0.125 inch), and the travel velocity (e.g., from about 0.005 to about 0.010 inch/minute).

[0083] Understanding that both the R_A to W_{Void} ratio and W_{VDCL} correlate well with the spin that may be imparted to an impacted golf ball, it may also be desirable to provide a coordinated set of golf clubs that vary the R_A to W_{Void} ratio and W_{VDCL} (taken within the Y-Z plane through face center) as a function of the loft angle of the club head. For example, in a low lofted club, spin may be less desirable than in a comparatively higher lofted club. As such, the milling pattern/surface texture provided on the face may be specifically controlled to support the design objectives of the club head.

[0084] In one embodiment, a set of golf clubs may comprise three golf clubs, each having a different loft angle (L), where $L_1 < L_2 < L_3$. In this set, each golf club may have a progressively decreasing R_A/W_{Void} ratio (i.e., where $(R_A/W_{Void})_1 > (R_A/W_{Void})_2 > (R_A/W_{Void})_3$), and/or a progressively decreasing W_{VDCL} value (i.e., where $W_{VDCL1} > W_{VDCL2} > W_{VDCL3}$). In one embodiment, at least the first of the three clubs (indicated with a subscript “1” in the relationships above) is a wood-style club, and may be a driver having a loft of from about 8 degrees to about 12 degrees. In an embodiment, at least the

third golf club of the set (indicated with a subscript “3” in the relationships above) may be an iron-type golf club. In an embodiment, L_3 may be less than or equal to about 24 degrees. Finally, in an embodiment, all three clubs in the set may be wood-style golf clubs or all three may be iron-style golf clubs.

[0085] It should further be noted that the inverse correlation between spin and both R_A to W_{Void} ratio and W_{VDCL} generally only applies for lower lofted club heads (i.e., loft angles of from about 8 to about 24 degrees). For higher lofted club heads (i.e., loft angles greater than about 30 degrees), the opposite effect may exist. More specifically, in higher lofted club heads, spin may increase with a corresponding increase in both R_A to W_{Void} ratio and W_{VDCL} . It is believed that this transition occurs due to the change in the magnitude of the shear impact forces as the loft and impact angle increases (i.e., where a driver imparts predominantly a compressive force to a golf ball, a wedge imparts a much more substantial shear force).

[0086] Therefore, in an embodiment, a high-lofted iron (i.e., having a loft angle of from about 30 to about 64 degrees, or from about 34 to about 64 degrees, or from about 39 to about 64 degrees), may be specifically designed to have a high backspin tendency by including a milled strike face with surface texture characterized by an R_A to W_{Void} ratio, measured in a Y-Z plane through the face center, that is greater than about 4, or greater than about 5, or greater than about 6, or greater than about 7, or greater than about 8, greater than about 9, or greater than about 10. In some embodiments, the R_A to W_{Void} ratio can range from 4 to 12, 4 to 8, 8 to 12, 6 to 10, 4 to 6, 36 to 8, 8 to 10, or 10 to 12. For example, the R_A to W_{Void} ratio can be 4, 6, 8, 10, or 12. Additionally, or alternatively, this high-spin iron face surface texture may be characterized by a W_{VDCL} value, measured in a Y-Z plane through the face center, that is greater than about 18%, or greater than about 20%, or greater than about 22%, or greater than about 24%, or greater than about 26%, or greater than about 28%, or greater than about 30%. In some embodiments, the W_{VDCL} value can range from 18% to 33%, 18% to 24%, 24% to 36%, 24% to 30%, 30% to 36%, or 27% to 33%. For example, the W_{VDCL} value can be 18%, 20%, 22%, 24%, 26%, 28%, 30%, 32%, 34%, or 36%.

[0087] Likewise, in an embodiment, a set of golf clubs may comprise three golf clubs, each having a different loft angle (L), where $L_1 < L_2 < L_3$. In this set, each golf

club may have an R_A/W_{Void} ratio where $(R_A/W_{\text{Void}})_1 > (R_A/W_{\text{Void}})_2$ and $(R_A/W_{\text{Void}})_3 > (R_A/W_{\text{Void}})_2$. Alternatively, or in addition, each club may have a W_{VDCL} value where $W_{\text{VDCL}1} > W_{\text{VDCL}2}$ and $W_{\text{VDCL}3} > W_{\text{VDCL}2}$. In an embodiment, at least the first of the three clubs (indicated with a subscript “1” in the relationships above) is a wood-style club, and may be a driver having a loft of from about 8 degrees to about 12 degrees, and the third of the three clubs (indicated with a subscript “3” in the relationships above) is an iron-type club having a loft of from about 30 to about 64 degrees, or from about 34 to about 64 degrees, or from about 39 to about 64 degrees.

[0088] Replacement of one or more claimed elements constitutes reconstruction and not repair. Additionally, benefits, other advantages, and solutions to problems have been described with regard to specific embodiments. The benefits, advantages, solutions to problems, and any element or elements that may cause any benefit, advantage, or solution to occur or become more pronounced, however, are not to be construed as critical, required, or essential features or elements of any or all of the claims, unless such benefits, advantages, solutions, or elements are expressly stated in such claims.

[0089] As the rules to golf may change from time to time (e.g., new regulations may be adopted or old rules may be eliminated or modified by golf standard organizations and/or governing bodies such as the United States Golf Association (USGA), the Royal and Ancient Golf Club of St. Andrews (R&A), etc.), golf equipment related to the apparatus, methods, and articles of manufacture described herein may be conforming or non-conforming to the rules of golf at any particular time. Accordingly, golf equipment related to the apparatus, methods, and articles of manufacture described herein may be advertised, offered for sale, and/or sold as conforming or non-conforming golf equipment. The apparatus, methods, and articles of manufacture described herein are not limited in this regard.

[0090] While the above examples may be described in connection with an iron-type golf club, the apparatus, methods, and articles of manufacture described herein may be applicable to other types of golf club such as a driver wood-type golf club, a fairway wood-type golf club, a hybrid-type golf club, an iron-type golf club, a wedge-type golf club, or a putter-type golf club. Alternatively, the apparatus, methods, and articles of

manufacture described herein may be applicable to other types of sports equipment such as a hockey stick, a tennis racket, a fishing pole, a ski pole, etc.

[0091] Moreover, embodiments and limitations disclosed herein are not dedicated to the public under the doctrine of dedication if the embodiments and/or limitations: (1) are not expressly claimed in the claims; and (2) are or are potentially equivalents of express elements and/or limitations in the claims under the doctrine of equivalents.

[0092]

[0093]

[0094]

CLAIMS

1. A wood-style golf club head comprising:
- a toe portion, a heel portion, a crown, and a sole;
 - a strike face and a body that cooperate to define a hollow internal club head volume, the strike face further comprising a ball striking surface having a surface texture characteristic of milling;
 - wherein the strike face is disposed at a loft angle of from 8 degrees to 14 degrees;
 - the surface texture comprises a plurality of peaks, a plurality of valleys, and a reference mid-plane extending in between the plurality of peaks and the plurality of valleys, wherein below the reference mid-plane is a negative distance, and above the reference mid-plane is a positive distance, and the plurality of peaks and the plurality of valleys extend an average maximum distance of at least -200 micro inches (-5.08 micro meters) to at least 200 micro inches (5.08 micro meters) from the mid-plane;
 - the surface texture further comprises a center portion that is surrounded by a peripheral portion;
 - the central portion is round and comprises a concentric milling pattern;
 - the peripheral portion comprises an emanating ray milling pattern;
 - the surface texture further comprises an average surface roughness (R_A), representing an arithmetic average value of absolute surface deviations relative to a mean center line, a surface void parameter (W_{Void}), representing an average depth of the plurality of valleys relative to a closed reference surface created using a morphologic closing filter applied to the surface texture, and a surface contact parameter (W_{VDCL}), representing the amount of contact between the closed reference surface and the surface texture;
 - wherein the closed reference surface is defined as a theoretical disc with a predetermined radius rolled across the surface texture;
 - wherein the surface texture, measured within at least one of a vertical cutting plane or a second cutting plane that is orthogonal to both the vertical cutting plane and the ball striking surface, is characterized by at least one of: a ratio of R_A to W_{Void} being greater than about 4; or, a W_{VDCL} parameter being greater than about 24%; and

wherein the RA is measured using a high-pass filter having a 0.762 mm cutoff, the WVoid parameter is measured using a 0.127 mm radius closing filter, and the WVDCL parameter is measured using a 0.508 mm radius closing filter.

2. The golf club head of claim 1, wherein the at least one of the vertical cutting plane and the second cutting plane extends through a geometric center of the strike face.
3. The golf club head of any of claims 1-2, wherein the surface texture is further characterized by at least one of: the ratio of RA to WVoid being greater than about 8; or, the WVDCL parameter being greater than about 28%.
4. The golf club head of any of claims 1-3, wherein the plurality of peaks comprises a plurality of smaller valleys; and wherein the plurality of valleys comprises a plurality of smaller peaks.
5. The golf club head of any of claims 1-4, wherein the surface texture varies as a function of a distance from a geometric center of the face.
6. The golf club head of any of claims 1-5, wherein the surface texture is further characterized by at least one of the ratio of RA to WVoid or the WVDCL parameter being greater within the peripheral portion than within the center portion.
7. The golf club head of any of claims 1-6, wherein the strike face comprises a strike plate and a frame that surrounds the strike plate, wherein the strike plate is affixed within an opening provided in the frame such that the strike plate and frame cooperate to define the ball striking surface.
8. A wood-style golf club head comprising:
a toe portion, a heel portion, a crown, and a sole;

a strike face and a body that cooperate to define a hollow internal club head volume, the strike face further comprising a ball striking surface having a surface texture characteristic of milling;

wherein the strike face is disposed at a loft angle of from 8 degrees to 14 degrees;

the surface texture comprises a plurality of peaks, a plurality of valleys, and a reference mid-plane extending in between the plurality of peaks and the plurality of valleys, wherein below the reference mid-plane is a negative distance, and above the reference mid-plane is a positive distance, and the plurality of peaks and the plurality of valleys extend an average maximum distance of at least -200 micro inches (-5.08 micro meters) to at least 200 micro inches (5.08 micro meters) from the mid-plane;

the surface texture comprises a concentric pattern emanating from a central point on the strike face;

the surface texture further comprises an average surface roughness (R_A), representing an arithmetic average value of absolute surface deviations relative to a mean center line, a surface void parameter (W_{Void}), representing an average depth of the plurality of valleys relative to a closed reference surface created using a morphologic closing filter applied to the surface texture, and a surface contact parameter (W_{VDCL}), representing the amount of contact between the closed reference surface and the surface texture;

wherein the closed reference surface is defined as a theoretical disc with a predetermined radius rolled across the surface texture;

wherein the surface texture, measured within at least one of a vertical cutting plane or a second cutting plane that is orthogonal to both the vertical cutting plane and the ball striking surface, is characterized by at least one of: a ratio of R_A to W_{Void} being greater than about 4; or, a W_{VDCL} parameter being greater than about 24%; and

wherein the R_A is measured using a high-pass filter having a 0.762 mm cutoff, the W_{Void} parameter is measured using a 0.127 mm radius closing filter, and the W_{VDCL} parameter is measured using a 0.508 mm radius closing filter.

9. The golf club head of claim 8, wherein the surface texture, measured within a vertical cutting plane offset from the geometric center of the face, is characterized by at

least one of: the ratio of R_A to W_{Void} being less than about 4; or, the W_{VDCL} parameter being less than about 24%.

10. The golf club head of any of claims 8-9, wherein the surface texture, measured within a vertical cutting plane offset from the geometric center of the face, is characterized by the ratio of R_A to W_{Void} being greater than the ratio of R_A to W_{Void} measured within a plane intersecting the geometric center; or, the W_{VDCL} parameter being greater than the W_{VDCL} parameter measured within the plane that intersects the geometric center.

11. The golf club head of any of claims 8-10, wherein the surface texture, measured within the vertical cutting plane extending through the geometric center of the face, is further characterized by an R_A of between about $3.56 \mu\text{m}$ ($140 \mu\text{-in}$) and about $7.62 \mu\text{m}$ ($300 \mu\text{-in}$).

12. The golf club head of any of claims 8-11, wherein the ball striking surface comprises a first region having a first surface texture and a second region having a second surface texture; and

wherein at least one of: an average ratio of R_A to W_{Void} measured within a vertical cutting plane is different between the first region and the second region; or, an average W_{VDCL} parameter measured within a vertical cutting plane is different between the first region and the second region.

13. The golf club head of claim 12, wherein the second region surrounds the first region.

14. The golf club head of any of claim 8, wherein the surface texture varies as a function of a distance from a geometric center of the face.

15. The golf club head of any of claim 8, wherein the surface texture is further characterized by at least one of: the ratio of R_A to W_{Void} being greater than about 8; or, the W_{VDCL} parameter being greater than about 28%.
16. The golf club head of claim 8, further comprising a body that extends rearward from the ball striking surface.
17. The golf club head of claim 8, wherein the strike face includes:
a strike plate having an outer perimeter; and
a frame surrounding the strike plate, wherein the strike plate is welded to the frame across the entire outer perimeter; and
wherein the ball striking surface and the surface texture extend continuously across both the strike plate and the frame.