# Product Document



**Application Note No. AN032** 



## **PCB** technologies for LED applications

## **Application Note**



Valid for: all OSRAM Opto Semiconductors LEDs

#### **Abstract**

This application note provides a general survey of the various available Printed Circuit Board (PCB) technologies for the use in LED applications.

Authors: Huber Rainer / Lang Kurt-Jürgen

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#### A. Introduction

Due to the direct conversion of electrical current to light (optical radiation) in the semiconductor, LEDs are highly efficient — more efficient than most traditional light sources. However, with LEDs as well most of the electrical power is converted to heat rather than light. This thermal loss must be dissipated to ensure reliable and stable LED operation for exploiting the complete performance and efficiency of the LEDs. Because of the trend towards miniaturization, thermal output per surface unit is increasing, which means that ever increasing heat is emitted onto an ever smaller surface area for dissipation. With high-power applications, sufficient thermal management is of central importance.

In general, many options exist to achieve this, although these depend on the specific applications and ambient conditions. An universal, optimal design or concept is not realizable for this reason, but has to be individually designed according to the specific assembly, the specific requirements and the complete system. A principal overview of PCB technologies available on the market and their suitability for LED applications is outlined below.

### B. PCB technologies commonly used for LED applications

As a support element with direct contact to the components, the PCB is in certain respects the primary component for achieving thermal management. Making mistakes here with insufficient optimization means that resultant disadvantages at other locations in the complete system must be compensated for by measures that increase the costs.

For this reason the following fundamental considerations must be made beforehand:

- Which thermal quantity (power loss) must be dissipated where?
- How are the dimensions and performance data of the components?
- Where are the LEDs positioned on the PCB (position of heat sources)?
- Available space and assembly periphery?
- Application temperatures and ambient temperatures?
- What mechanisms are used to cool the system? (free or forced convection)
- How should the heat be conducted to the heat sinks?
- Do specific reliability requirements exist (e.g cycle stability)?
- Do special cost factors have to be observed?

The selection of appropriate materials for the circuit board is therefore of utmost importance.

#### FR4 printed circuit board (PCB)

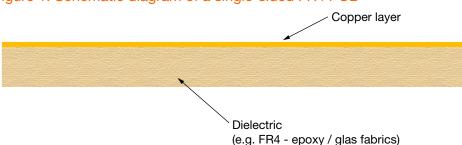
Classic composite PCB of glass fiber and epoxy resin, available in various compounds, versions (single-/ multilayer) and thickness (0.3 — 3.5 mm).

Table <sup>-</sup>	1: F	R4 F	CB	versions
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Designation	Material	Note
FR4 standard	Epoxy + glass fabrics	T <sub>g</sub> = 130 — 140 °C, RoHS/WEEE compliant
FR4 non-halogen	Epoxy + glass fabrics	T <sub>g</sub> ≥ 150 °C, CAF-resistant
FR4 mid T <sub>g</sub>	Epoxy + glass fabrics	$T_g \sim$ 140 $-$ 160 °C, increased thermal stability, low elongation in z-axis, high steadiness at lead-free soldering, often CAF-resistant
FR4 high T <sub>g</sub>	Epoxy + glass fabrics	T <sub>g</sub> ~160 — 190 °C, increased thermal stability, low elongation in z-axis, high steadiness at lead-free soldering, often CAF-resistant

Thermal distribution occurs here in the copper layer (typical thickness 35  $\mu$ m) on the PCB surface via heat distribution. Thicker copper layers (e.g. 70  $\mu$ m & 105  $\mu$ m) improve thermal dissipation properties and thus enable heat distribution over larger surfaces.

Figure 1: Schematic diagram of a single-sided FR4 PCB



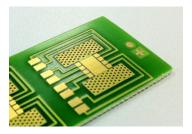
Pure standard substrates without improvements such as FR4 are normally not suitable for use with high-power LEDs due to their low thermal conductivity ( $\sim 0.2 - 0.5 \text{ Wm}^{-1} \text{K}^{-1}$ ).

#### FR4 PCB with thermal via array

Thin double-sided FR4 material with plated through-holes (= thermal vias) to ensure a thermal path through the FR4 substrate and to improve heat conduction.

The thickness of the PCB is typically in the range of 0.3 mm  $\leq$  t < 1.6 mm.

Figure 2: Example of an FR4 PCB with thermal via arrays

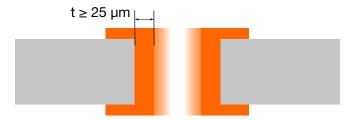


The vias take on the heat transport function here, thus significantly improving vertical thermal resistance of the FR4 material in a targeted and localized manner. The thermal conduction capability of the vias themselves is determined by the plating, via diameter and via pitch. Standard copper thicknesses of  $20-25\,\mu m$  have become established in the industry, but greater wall plating thicknesses are also used. As a general rule, the thicker the copper layer, the better the performance — but also costs increase with thickness.

Two types of thermal via are possible:

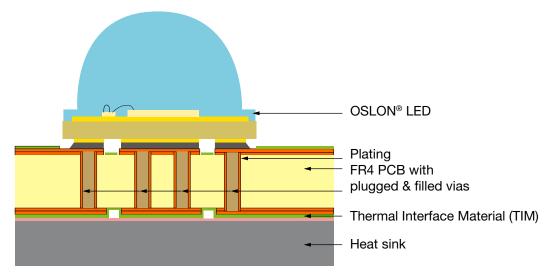
- Simple open PTH (plated through hole) vias (Figure 3)
- Vias filled with epoxy and then capped with copper (Figure 4)

Figure 3: Schematic layout of a thermal via



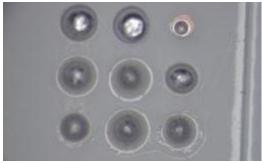
The use of thermally conductive silver pastes for filling in order to improve the thermal conductivity of the vias has in practice only a minor thermal effect but increases costs. For economic reasons it is thus better to slightly enlarge the copper thickness in the hole.

Figure 4: Schematic diagram of an OSLON® LED on an FR4 PCB with plugged and filled vias



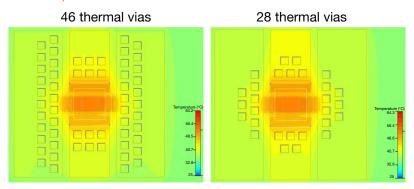
The filled, copper-capped vias have the advantage that they can be arranged directly under the thermal solder pad of the LED (e.g. OSLON®, OSLON® Black Flat, etc.), meaning they are able to directly conduct heat. The copper plugging prevents uncontrolled solder wicking / solder voiding during reflow soldering at open vias (solder run-off).

Figure 5: Unfilled thermal vias have solder wicking if used in solder pads



Uncontrolled solder wicking generates solder balls on the backside of the PCB (Figure 5), leading to insufficient thermal connection between the PCB and the heat sink. In many cases however, simple thermal vias are sufficient to achieve a clear reduction in thermal resistance down to the targeted value. The level of resultant thermal resistance is affected by the number and position of the vias. The closer the vias are located to the heat source, the better and faster the heat can be dissipated and the lower the thermal resistance (Figure 6).

Figure 6: Comparison of the effect of two different configurations of thermal vias (simulation)

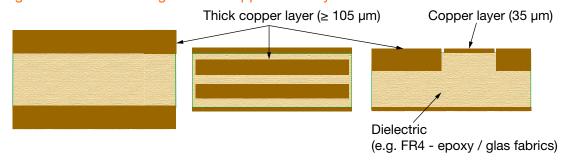


As a general rule it is advisable to design the copper surface around the solder pads, especially at the thermal pad if existing, to be as large as possible in order to achieve sufficient heat distribution across the FR4.

#### Thick copper PCB

Are PCBs with copper layer thicknesses of 105  $\mu$ m to 400  $\mu$ m, and up to 500  $\mu$ m in special cases. According to requirements and technology used, layers are applied in a planar way as external and/or internal layer. The basis material used is FR4 or a metal substrate (Al, Cu) with a dielectric. The primary application sector consists of applications with high power (high current) and for the cooling of components with large thermal power losses. Constructions are mainly multilayer or double-sided PCBs.

Figure 7: Schematic diagram of a copper thick-layer PCB

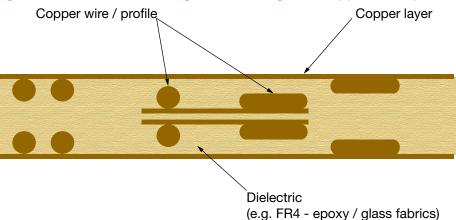


A special form is the so-called "iceberg" technology. Here a thin-layer copper layout is combined with selectively applied thick copper layers. The thick layer areas are recessed into the basis material (FR4) to achieve a uniform surface level. Expanding the copper cross-section achieves significantly wider heat dissipation as well as enabling local thermal build-up to be controlled.

#### Integrated copper wires and profiles

The base materials of FR4 technology are used here, in which applicationspecific copper wires and/or copper profiles are integrated and connected to the connection surfaces.

Figure 8: Schematic PCB diagram with integrated copper wire / profile

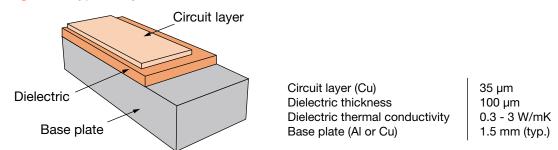


Expansion of the copper cross-section favors thermal distribution, and heat can be specifically dissipated due to the individual position in the PCB. Typical copper cross-sections are for example: 2000 µm x 500 µm, 4000 µm x 500 µm

#### **Insulated Metal Substrate (IMS)**

Insulated metal substrate (IMS) is the term for a PCB constructed with a metallic support plate separated by a thin dielectric from the copper conductors of the circuit. Aluminum is usually used as a carrier material because of low costs, and copper is also used with higher power densities because of its superior thermal conductivity. The attached dielectric has significant influence on total performance and is the determining factor for thermal resistance. Layers of unfilled and filled epoxy resins are used. With filled resins, 3 to 10-fold higher thermal conductivity is achieved compared to FR4 depending on filling material and quantity, but filling materials influence the cycle resistance of the board. Layer thickness of the dielectric is in the range of 20 µm to 200 µm, although the fact that decreasing thickness of the layer usually leads to a reduction of electrical dielectric strength must generally be taken into account. However, based on the structure, the IMS is mostly single-layer. Multi-layer versions are available but with higher costs.

Figure 9: Typical layer construction of an insulated metal substrate PCB



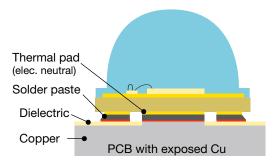
In most applications IMS boards are attached to the heat sink together with a thermal interface material (TIM) by screws. When using an IMS-PCB with ceramic-based LEDs, it should be considered that the difference in the coefficients of thermal expansion (CTE) between the ceramic material of the LED and the IMS PCB creates stress on the solder joint.

To minimize this effect, copper (Cu) is therefore preferred to aluminum (Al) as base plate material because of its lower CTE. Due to its significant higher thermal conductivity compared to FR4 technology (~ factor 10), IMS is widely-used in LED applications, especially with high power LEDs. In terms of material prices, costs with IMS can be approximately 2 to 4 times higher than with FR4.

#### IMS with exposed copper

This is an optimized variant of IMS PCBs where the copper partially protrudes through the insulation layer. The package is partly directly connected to the metallic carrier here for bridging the dielectric.

Figure 10: LED on PCB with exposed copper

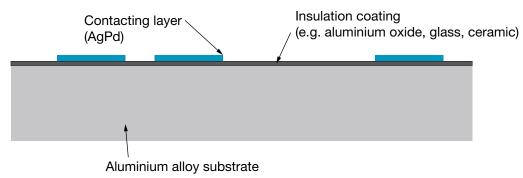


Here, heat can be dissipated without requiring any insulation between the thermal pad, the metal layer and the heat sink. This permits LEDs to be operated at higher currents or higher power levels for example. It should be generally considered here that the connected thermal contact points are electrically neutral. In combination with ceramic based packages however, some PCB designs with exposed copper may cause higher thermal mechanical stresses during the assembly process. Because of this, application designs need to be verified to avoid damage. Please confer with application team of OSRAM Opto Semiconductors.

#### **Aluminum with thin insulation layer**

This is a modified form of IMS technology. Instead of a dielectric made of epoxy resin, a thin aluminum oxide or ceramic layer is used. Depending on the required dielectric strength, the dielectric layer thickness is in the range of  $< 40 \, \mu m$  to 125  $\mu m$ , whereby thermal conductivity of approximately 2 W/mK is achieved.

Figure 11: Schematic PCB diagram of aluminum with thin insulation layer



#### Thick / thin film ceramics

The core of the PCB here is a ceramic carrier substrate to which the conductors are directly applied via thick film or thin film technology. According to the specific variant, ceramic carriers have thicknesses of 0.25 mm to 3 mm. Because ceramic substrates themselves are electrically insulating but are thermally conductive, heat can be dissipated directly without other thermal barriers. Aluminum oxide and aluminum nitride are usually used as substrate materials, the latter having significantly superior thermal conductivity properties. The thermal conductivity of aluminum oxide is in the range of ~ 20 — 25 Wm<sup>-1</sup>K<sup>-1</sup>, and that of aluminum nitride is at (~ 170 Wm<sup>-1</sup>K<sup>-1</sup>). Another advantage among many is low thermal expansion. In combination with ceramic-based High-Power LEDs, they are thus primarily suitable for applications with high thermal cyclic loads

With regard to thermal management, ceramic PCBs are generally very effective, but are often seen as a luxury variant because of their higher costs.

## C. PCB pad finishes

In general, all finishes are well-proven for SMT assembly, but with smaller solder pads the quality of the plating/finish is more important. Hot Air Solder Leveling (HAL/HASL) finish is less preferred for assembly because of the uneven surface compared to completely "flat" platings such as Cu-OSP (OSP: Organic Solderability Preservative) or immersion Sn or NiAu (ENIG). From a package point of view, it is difficult to recommend a particular PCB pad finish that will always meet all requirements. The choice of finish also depends strongly on board design, pad geometry, needs of other components on the board and process conditions, and must be chosen according to the needs of the specific application. Internal tests at OSRAM Opto Semiconductor have shown that Cu-OSP or NiAu are suitable and reliable platings in most cases.

Table 2: Comparison of PCB finishes

Finish / solder pad plating	Typ. layer thickness	Advantages / properties	Concerns
OSP (Organic Solde- rability Preservative)	0.3 — 0.5 μm	Lowest cost, fully planar surface, simple easy to operate process	Solderability degradation (storage conditions, multiple thermal cycles → N <sub>2</sub> reflow) exposed copper
HAL / HASL (Hot Air Soldering Leveling)	0.5 — 10 μm	Low cost, widely usage, excellent wetting	Uneven surface, formation of humps, flatness of single pads, during process high ther- mal stress on PCB, residues (flux)
Immersion Sn (electroness)	0.3 — 1.3 μm	Simple process, planar surface, only copper and solder in solder joit	Limited shelf life and storage, cop- per diffusion into Sn, baking or 2x reflow on PCB may be critical
Immersion Ag (electroless)	0.3 — 0.5 μm	Planar surface, wire bondable	Limited shelf life and storage, con- cerns of tarnishing/ corrosion, baking or 2 x reflow of PCB may be criti- cal
Electroless Ni/ Immersion Au (ENIG)	3 — 7 μm 0.06 — 0.1 μm	Fully planar sur- face, very good shelf life	High cost process control, compati- ble to solder mask, concerns of Ni cor- rosion (Black pad)
Electroless Ni / Electroless Pd/ Immersion Au (ENE- PIG)	3 — 7 μm 0.05 — 0.15 μm 0.01 — 0.1 μm	Fully planar sur- face, "universal Finish" solderable and wire bondable, reduce Au thick- ness, Pd reduces	High cost, pro- cess control, com- patible to solder mask

#### Second level reliability

The term "second level reliability" usually appears in connection with the requirements and characteristics of the application or of the overall system (Figure 12). It ultimately however refers to the reliability of the solder connection between the component (e.g. LED) and the printed circuit board (PCB) or carrier substrate.

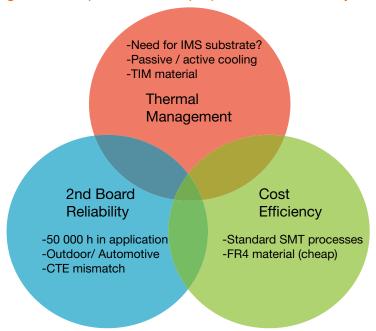


Figure 12: Requirements and properties for efficient system design

The reliability of the soldered joint itself is determined or influenced by various factors, e.g. component housing, solder, mounting and soldering process and printed circuit board (Table 3).

This influence can take place either directly at the system development stage, e.g. an unsuitable combination of SMD package and PCB material (CTE mismatch), or when the individual components are processed, e.g. misalignment due to insufficient accuracy in assembly. Especially for LEDs with ceramic carrier substrate the aspect of second board reliability should therefore be considered when selecting the PCB type, or the possible effects should be considered.

Table 3: Influencing factors on 2nd board reliability

#### SMD package

#### Solder material

- Material (CTE, thickness); Al<sub>2</sub>O<sub>3</sub>, AIN, ...)
- Dimensions, Pin configuration
- Metallization / layer construction
- Footprint layout
- Solderability

- Alloy (eutectic SnPb, Pb-free: SnAgCu (SAC305), Innolot, ...low melting temp.)
- Flux material and contend → Voiding
- Particle size and shape (Type 3, Type 4, ...)

#### PCB / substrate

- Material (CTE; FR4, Aleptwin, Bergquist MP, LM Schooner, ...)
- Solder pad / design SMD / NSMD (Solder Mask Defined)
- Solder resist topology
- Metallization finish / HASL, immersion Sn, OSP, NiAu (ENIG)
- Wettability / residues
- Outgasing from PCB material

#### Assembly & soldering process

- Solder paste printing, stencil thickness / aperture printing quality (Alignment, slumping)
- Pick & place, position accuracy, turning / tilting
- Reflow soldering
- Soldering profile 245 °C 260 °C (optimized for paste)
- Reflow oven (Standard-Reflow Air-N<sub>2</sub>, Vacuum-Vaporphase)

## **D. Thermal comparison of PCBs**

Based on data from the high-power LED OSRAM OSTAR Compact and a predefined heat sink, an exemplary thermal comparison of specific PCB concepts was carried out via thermal simulation. Typical key data and material parameters were used for the various PCB concepts. Figure 13 shows the principal construction and peripheral condition for the simulation as well as results for the individual PCB variants. The parameter for comparison was the resulting junction temperature T<sub>.1</sub> of the LED. The comparison was carried out exclusively according to thermal factors, and did not consider aspects of 2<sup>nd</sup> Board Reliability or other application-related requirements. If only the resultant junction temperature is considered, then all lie below the maximum permissible temperature level of 150 °C, related to the 25 °C ambient temperature. They are thus fundamentally suitable according to the specified conditions, but have differing optimization potential with regard to additional requirements or higher performance classes with the LEDs. In summary, all PCB types have their advantages, and which type is best depends on the respective application in terms of individual requirements and conditions. Since PCB design, construction and material are essential for optimized thermal design, verification of the total system is therefore recommended.

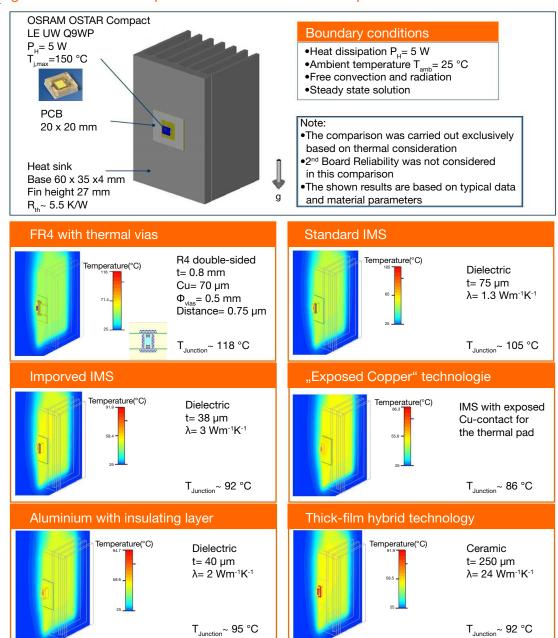


Figure 13: Thermal comparison of different PCB concepts

#### **E.** Conclusion

Many PCB technologies available on the market, along with their individual benefits and disadvantages, are suitable for LED applications.

Because of good thermal distribution and mechanical stability, IMS technology with improved dielectrics is often given preference for many LED applications, especially for higher performance classes. In the mid-level to higher performance ranges, a focus is placed on FR4 technology with thermally optimized layouts.

With simple measures such as supplementary copper surfaces, higher copper densities and thermal vias, the total system can be influenced at relatively low cost. Nevertheless, all PCB types have their benefits, and which is best depends on the respective application with individual requirements and conditions. Since PCB design, construction and material are essential for optimized thermal designs, it is therefore recommended to verify the total system.

OSRAM Opto Semiconductors is able to support its customers during their development and design processes in finding the best solution for their specific applications.

Further information regarding thermal management, processing and specific LED types etc. can be found on the OSRAM Opto Semiconductor website in the "Application Notes" section.



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**OSRAM Opto Semiconductors GmbH** 

Head office:

Leibnizstr. 4 93055 Regensburg Germany www.osram-os.com

