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16. Abstracts On February 26, 1972, a coal refuse dam, owned and operated by the Buffalo Mining Company, failed near Saunders, W. Va. The resulting flooding of the Buffalo Creek Valley had national ramifications. The immediate consequences of the flooding were the deaths of 118 persons and 7 reported missing, the loss of over 500 homes, and extensive flood damage to other property in Buffalo Creek Valley. Basic data were gathered during the investigation of the Middle Fork Valley dams and refuse bank above Saunders during field investigations of the site conducted from the end of March through mid-September 1972. This information consisted of field mapping, subsurface exploration and sampling by means of auger drill holes, field density tests, field permeability tests, aerial photography, vane shear tests, and cone penetration tests. Volume II, the appendices, covers these details.				
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**ANALYSIS OF
COAL REFUSE DAM FAILURE
MIDDLE FORK BUFFALO CREEK
SAUNDERS, WEST VIRGINIA**

UNITED STATES
DEPARTMENT OF THE INTERIOR
BUREAU OF MINES
WASHINGTON, D.C.

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VOLUME 2 OF 2 - APPENDICES

FEBRUARY 1973

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**W. A. WAHLER
& ASSOCIATES**

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ANALYSIS OF
COAL REFUSE DAM FAILURE
MIDDLE FORK BUFFALO CREEK
SAUNDERS, WEST VIRGINIA

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Drill Logs and Water Pressure Test Results:

<u>Hole No.</u>	<u>No. of Sheets</u>
S-1	1
S-2	2
S-3	4
S-4	3
S-5	3
S-6	4
S-7	3
S-8	2

TABLES (continued)

Table No.

Drill logs and Water Pressure Test Results (continued):

Hole No.	No. of Sheets
S-9	3
S-10	3
S-11	3
S-12	4
S-13	3
S-14	3
S-15	2
S-16	2
S-17	2
S-18	2
S-19	2
S-20	1
S-21	2
S-22	1

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Key for Exploration Logs (Foldout for Interpretation of Logs)

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APPENDIX A

FIELD INVESTIGATION

A. INTRODUCTION

Basic data were gathered during the investigation of the Middle Fork Valley dams and refuse bank above Saunders, West Virginia, during field investigations of the site conducted from the end of March through mid-September, 1972. This information consisted of field mapping, subsurface exploration and sampling by means of auger drill holes, field density tests, field permeability tests, aerial photography, vane shear tests, and cone penetration tests. The locations of most exploration features are shown on Figure VI-20; Hole BS-19, at the downstream end of the refuse bank is shown on Figure III-3A, and exploration features at the upstream end of Pool 3 and in Dam No. 4 and Pool 4 are shown on Figure III-3C. A drill hole summary is included here as Table A-1. Hundreds of photographs were taken during the field investigation. The locations of most of those used in this report are indicated on Figure A-1; a few photograph locations are shown on Figure III-3C. Unless otherwise credited, the full-page photographs are by Robert T. Johnson of Logan, West Virginia. The small-format photographs are by staff personnel of W. A. Wahler and Associates.

B. AUGER DRILLING

Sixty exploration holes totaling 3302.9 feet were drilled in Middle Fork Valley utilizing truck-mounted Acker AD-2 and CME-45 drill rigs. The drilling services were subcontracted to Tinney Drilling Co., Bridgeville, Pennsylvania. The equipment used varied with the purpose of the hole.

Twenty-two S-series holes (S-1 through S-22) were drilled for sample retrieval. These holes were drilled with 6-inch O.D. (3 9/32-inch I.D.) hollow stem augers (Figure A-2, Photo A) except for hole S-20 which was drilled and sampled continuously with a Pitcher barrel of 5-7/8-inch O.D. (Figure A-2, Photo D). The S-series holes varied in depth from 14.0 to 174.0 feet, and their combined footage totaled 1,879.8 feet.

The hollow stem auger holes were sampled at intervals determined in the field by W. A. Wahler and Associates' representatives. Sampling was done largely with such conventional sampling tools as the standard (3-inch diameter by 30 inches long) Shelby tube, Shelby tube with piston, and the standard split-spoon penetrometer (ASTM D-1586-67). Figure A-3 (Photo B) shows typical disturbed recovery with the standard penetrometer sampler, and Figure A-2 (Photo B) shows the hammer set-up for a standard penetration test. The standard penetration test consists of driving a 2-inch O.D. by 1 3/8-inch I.D. split-spoon sampler with a 140-lb. hammer falling a distance of 30 inches. Where possible, the sampler was driven 18 inches into undisturbed material and the blow count recorded for each successive 6 inches of penetration. The standard penetrometer blow count, N, is the total number of blows for the second and third 6-inch intervals driven. It is recorded on the drill hole logs.

The Pitcher barrel, utilizing a Shelby-type tube measuring 4 inches in diameter by 36 inches long (Figure A-2, Photo D) was used in hole S-20 to retrieve larger diameter samples than could be obtained with the more common Shelby tubes. Non-standard sampling tools included a "poorboy" sampler (used in hole S-4) which was a discarded Nx inner core barrel, and double-length Shelby tubes, fabricated off-site by welding the nose of one standard (3 x 30 inches) Shelby tube to the top of another, and filling the attachment holes in the lower tube. A double Shelby tube is shown on Figure A-2, Photo C.

The materials encountered in the S-series holes were logged on a continuous basis by a W. A. Wahler and Associates representative and were described in accordance with the Unified Soil Classification (ASTM D-2487). The classification is described on the Key for Exploration Logs, which accompanies the logs included in this Appendix. Relatively undisturbed samples were obtained by pushing 3-inch O.D., thin-walled Shelby tubes into embankment and reservoir sediment (sludge) materials. When possible, the 2.5-foot long Shelby tubes were pushed 2.0 feet and the double Shelleys were pushed 4.0 to 4.5 feet if refusal was not met. The Pitcher sampling technique is properly described as a push-drill method of sampler advancement. The 3.0-foot long Pitcher tubes were advanced 2.0 feet unless earlier refused.

The presence of coarse gravel and cobbles in embankment materials made it difficult to obtain undisturbed samples in the embankment. In fact, attempts to take Shelby samples in this material often met with complete refusal of penetration in only a few tenths of a foot. Usually, Shelby samples obtained from the sludge were only slightly disturbed. However, recovery of this wet, fine-grained, material was also rendered difficult since samples were often lost from the tubes as they were pulled from the drill holes. The double Shelby tube was devised in an attempt to solve two problems: 1) poor recovery of samples of the sludge with normal Shelby or piston techniques, and 2) a sampler was needed that was long enough to get through the sludge which often rose into the auger stem after the inner bit was removed. The double Shelby tubes were moderately successful in both applications. A discussion of sampling problems and techniques in coal refuse will be included in another report to the Bureau of Mines.

When the auger was refused, Nx coring commenced in most holes. Generally, 10 feet of bedrock were cored; in some holes the coring was carried deeper. The following S-series holes were not cored: S-14, 16, 18, 19,

20, 21 and 22. Figure A-3, Photo A, shows typical core. Water pressure tests were conducted in the bedrock in holes S-3 and S-6. Results of the tests are presented immediately after the respective drill hole logs in this Appendix.

Nineteen BS-series holes (BS-1 through BS-19) were drilled with 4- and 6-inch diameter solid-stem augers. Nearly all of these holes were drilled to refusal, which was generally taken to represent the bedrock surface underlying the overburden and fill. The BS-series holes were used to supplement our knowledge of the configuration of the bedrock surface, and to provide more precision in delineating the surface than could be attained with scattered S-series holes.

Data for the BS-series holes are presented in Table A-1; the holes were not logged due to the difficulty of determining precisely the depth from which the auger returns came. Some data about depths to various contacts are presented in Table A-1, but they are approximate only, and in part based on correlation with nearby S-series holes. The total footage drilled in the BS-series holes is 1012.6 feet.

Five P-series pilot holes were drilled for the portable vane shear and cone penetrometer equipment. These holes, also listed in Table A-1, were drilled with the truck-mounted auger rig. They penetrated gravel that the vane and cone could not, and permitted the vane and cone to test the sludge material underlying the gravels. Descriptions of the results of vane shear and cone penetrometer testing are presented elsewhere in this Appendix. The total footage involved in these pilot holes is 205 feet.

Fourteen FP-series holes were drilled in the left abutment for field permeability tests. Most of these holes were drilled to shallow depths with either solid or hollow stem auger. Holes FP-9A through 14A were

drilled by pushing a Shelby tube or tubes and retrieving undisturbed samples where possible. The total footage involved in the FP-series holes is 205.5 feet. The field permeability tests are described below.

C. FIELD PERMEABILITY TESTS

Fourteen field permeability tests were conducted in substantial accordance with U.S. Bureau of Reclamation Designation E-19. Test conditions were modified slightly in the field to make the test procedure consistent with the nature of the material to be tested. Results of these tests follow the drill hole logs in this Appendix, and are summarized in Table A-1. Figure A-3, Photo C, shows the test equipment set up at hole FP-3A. All field permeability tests were located in the left abutment remnant of Dam No. 3 as shown on Figure VI-20.

D. FIELD DENSITY TESTS

In order to determine the in-place density variation of the embankment and foundation materials within the Middle Fork Valley, a total of 44 field density tests, which are summarized in Table A-2, were performed in accordance with ASTM Test Designation D-1556-65. The location of all tests performed near Dams 1, 2, and 3 are shown on Figure VI-20 and those upstream of Dam No. 3 on Figure III-3C. Because of the wide variation in grain sizes, two different size cones were used. A 6-inch diameter sand cone was used exclusively in the foundation sludge material, whereas a 12-inch diameter sand cone was used in areas of coarse coal and shale waste.

As a result of the massive failure of Dam No. 3, it was impossible to obtain a good cross section of in-place density variation of the

original embankment material; however, a large bulldozer trench was excavated (Figure A-3, Photo D and Figure VI-20) in the remnant of the left abutment from the crest to the downstream toe, and a total of 10 in-place density tests were performed at about 5-foot vertical intervals throughout the length of the trench. A second dozer trench was excavated in the refuse dump downstream of Dam No. 2 near hole S-4 in order to obtain some in-place density data on the older coal waste material.

E. CONE PENETROMETER AND VANE SHEAR TESTS

Static penetration tests were performed by W. A. Wahler and Associates personnel, using portable equipment manufactured in Sweden by Jonnell & Nillson. The test procedure consisted of mechanically advancing a 10 square centimeter cone with automatic and continuous recording of total penetration resistance. A specially sealed vertical clip coupling is provided about 10 cm from the tip, which facilitates separating the two components of total penetration resistance; namely, skin friction along the rod surface and actual tip friction resistance at the cone. Six penetration probes were performed at Buffalo Creek Dam No. 3, one at Dam No. 2, and three within Pool 3 sludge at the upstream end of Pool 3.

In situ shear strengths were determined using the same portable equipment described above, except the penetrometer tip was removed and a 12 cm long by 6 cm wide vane was attached to the end rod. The vane shear probes were located adjacent to the penetrometer probes in order to correlate penetration resistance to shear strength. Predrilled pilot holes were required at Dam No. 2 (Figure A-3, Photo D) and in the channel area of Dam No. 3 in order to penetrate the overlying coarse materials prior to starting the in-place testing.

Where the equipment did not have to penetrate gravel, the penetrometer was first advanced until refusal was met. At an interval of approximately two meters, a friction test was conducted in order to separate rod friction from total penetration resistance of the material. After completing the penetration tests, the equipment was moved approximately 1 to 2 feet from the penetration hole to insure that vane shear tests would be performed in undisturbed material. The penetrometer cone was replaced by a vane, which also was advanced to refusal. At two-meter intervals a shear test was conducted to determine in-place shear strength of the material. Figure V-15, Photo C, shows the site of tests in Pool 3 sludge. Results and locations of both penetration and vane shear tests are presented in Table A-3 and Figure A-5, sheets 1 through 10.

As a result of the coarse-grained nature of the foundation sludge material, the penetration and vane shear data were used only as a means of interpreting the consistency of the material. The vane shear test results, in particular, can be very misleading and were not, in any way, used in the engineering analyses. The reason for the data not providing more useful information was a result of the sludge material exhibiting a dilatancy during the application of shearing strain. This dilatancy resulted in the development of negative pore pressures at the tip of the vane, thus increasing the undrained shear strength by some unknown amount. Similarly, the vertical slip coupling associated with the penetrometer equipment was not effective in separating the total and tip penetration resistance. The reasons for this are thought to be associated with (1) the relatively low in-place densities, (2) the low undrained shear strength, and (3) absence of any cohesion of these materials when saturated. Because of the difficulties associated with interpreting the rod friction portion of the test, the results have been presented in the form of total penetration resistance versus depth.

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F. BACKHOE PITS AND BULLDOZER TRENCHES

Eleven backhoe pits were excavated in the Pool 2, Pool 1, and Dam No. 1 areas to expose shallow contact relations and materials for observation. Logs of selected walls of the pits are presented on Figure A-6. Locations of the pits are shown on Figure VI-20. A typical backhoe operation is shown on Figure A-4, Photo A. Bulldozer trenches were excavated in the left abutment of Dam No. 3 and in the refuse bank near hole S-4. The trenches exposed the coal waste for detailed observation and for field density testing. The bulldozer was primarily used to construct an access road from the Buffalo Creek county road and secondarily for trenching and for on-site drill rig roads and ramps. The bulldozer and backhoe, along with equipment operators, were provided by the Paul J. Rayburn Company, a subcontractor from the local area.

G. AERIAL PHOTOGRAPHY AND TOPOGRAPHIC MAPPING

Aerial photography and the associated ground control were subcontracted to Michael Baker, Jr., Inc., of Beaver, Pennsylvania. Two series for vertical stereo coverage were flown as follows:

	<u>Date</u>	<u>Photo scale</u>	<u>Medium</u>
1.	March 9, 1972	1:6,000 1:6,000	black and white
2.	April 11, 1972		color

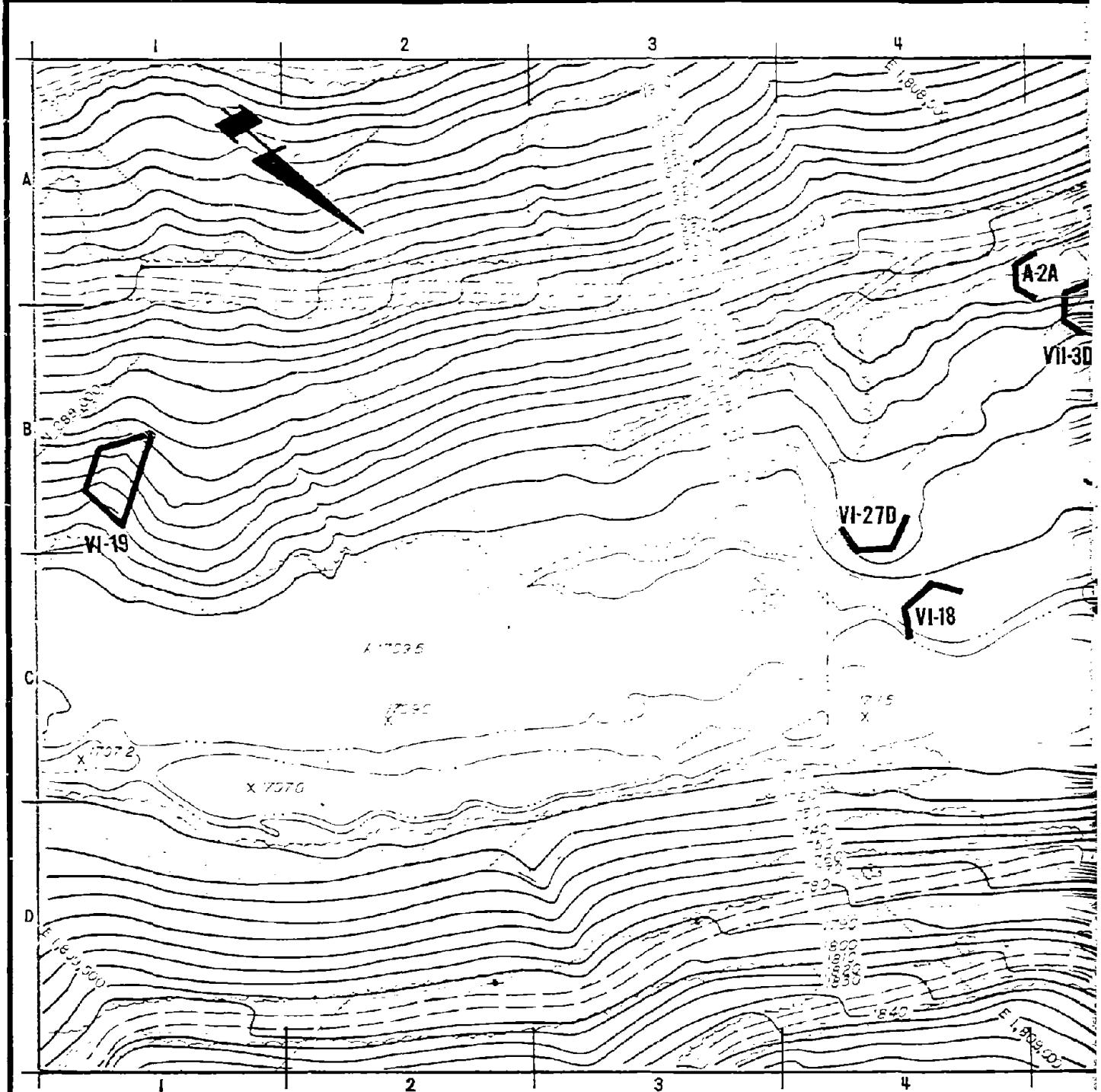
In addition, the subcontractor made available from his files black and white vertical aerial photographs taken February 28, 1972, November 28, 1962, and January 28, 1963.

The subcontractor prepared topographic maps of Middle Fork Valley and specific portions of the valley at scales of 1" = 100', 1" = 200',

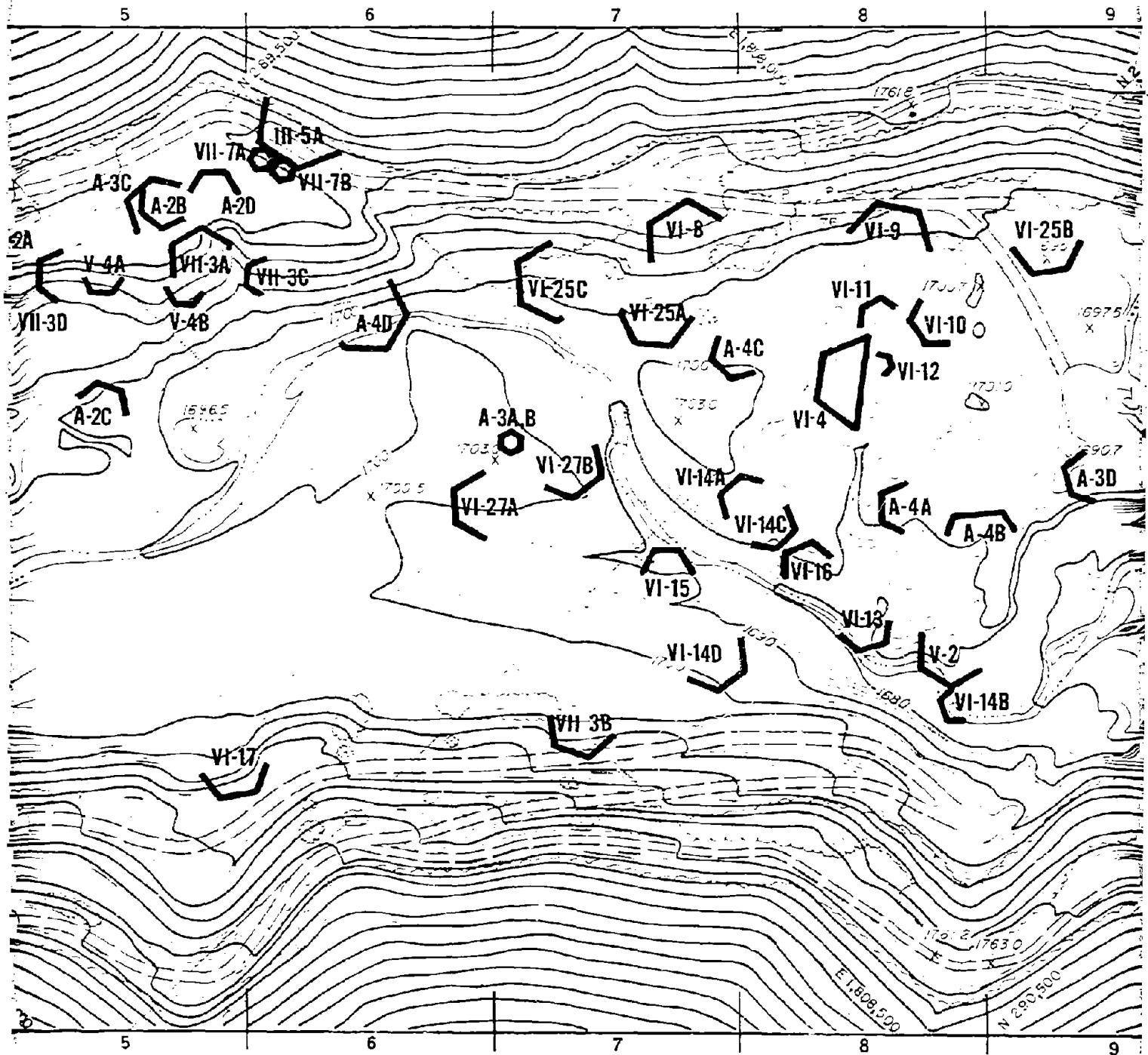
and 1" = 400'. Portions of the 1" = 100' map were enlarged to 1" = 50' for detailed geologic mapping. The 1" = 400' map was prepared from the small-scale November 28, 1962, aerial photographs in the files of the subcontractor.

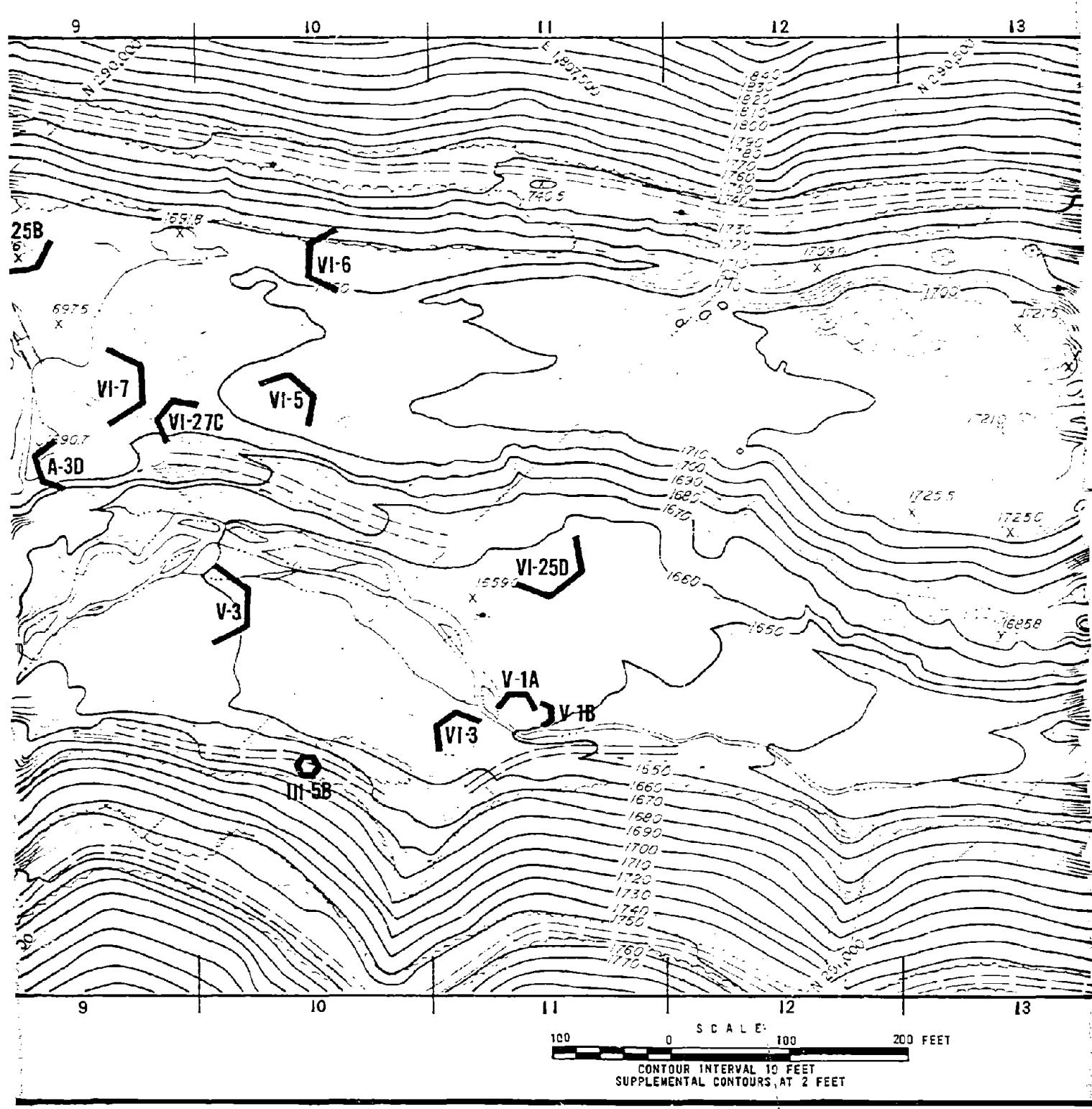
H. GEOLOGIC MAPPING

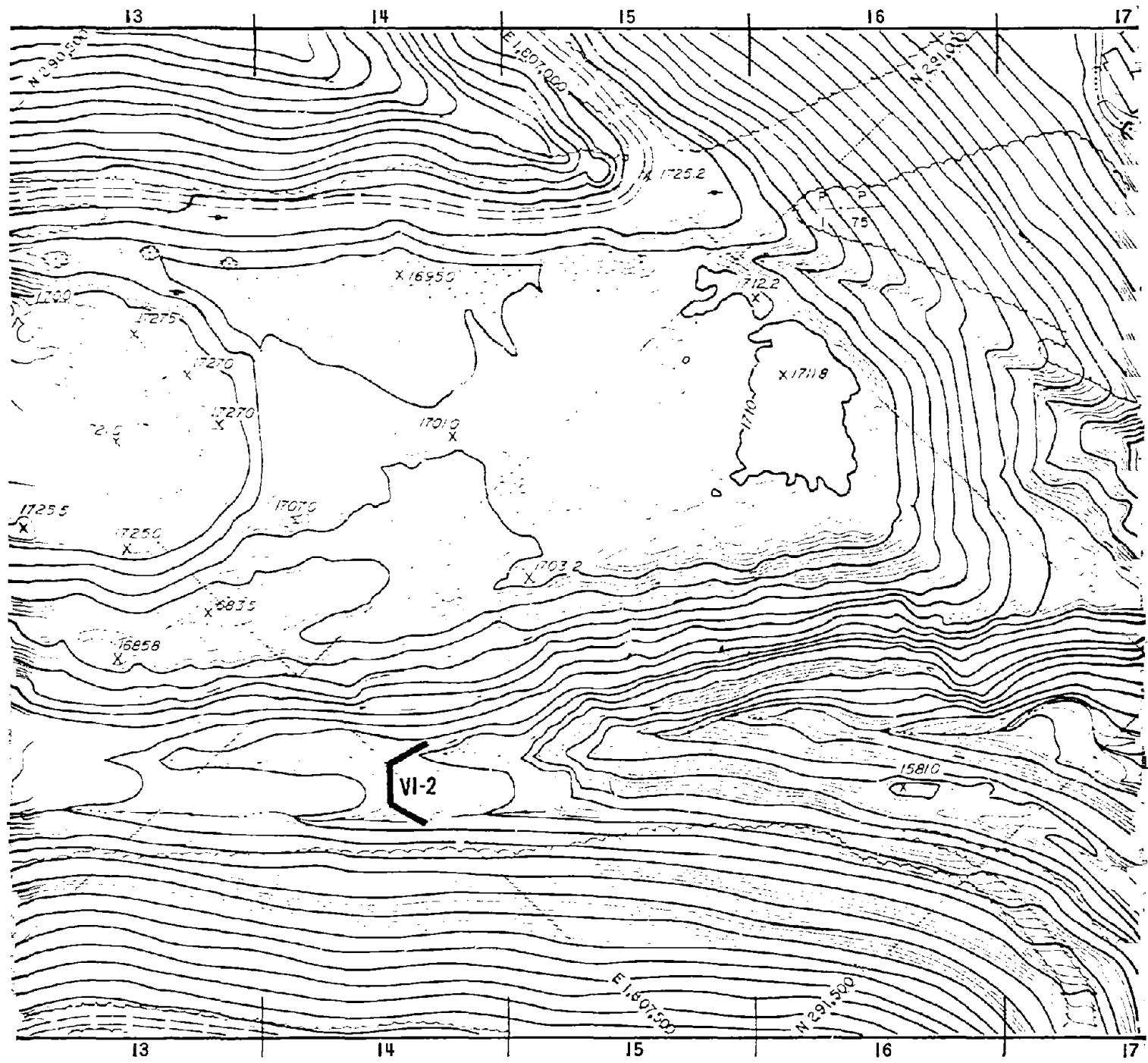
Geologic mapping was done intermittently from April through September, 1972. The initial efforts were concentrated on the areas most likely to change due to natural erosion or sliding, or due to subsequent exploration activities such as constructing access roads. Conventional surface mapping was supplemented by the use of aerial photographs and subsurface exploration.



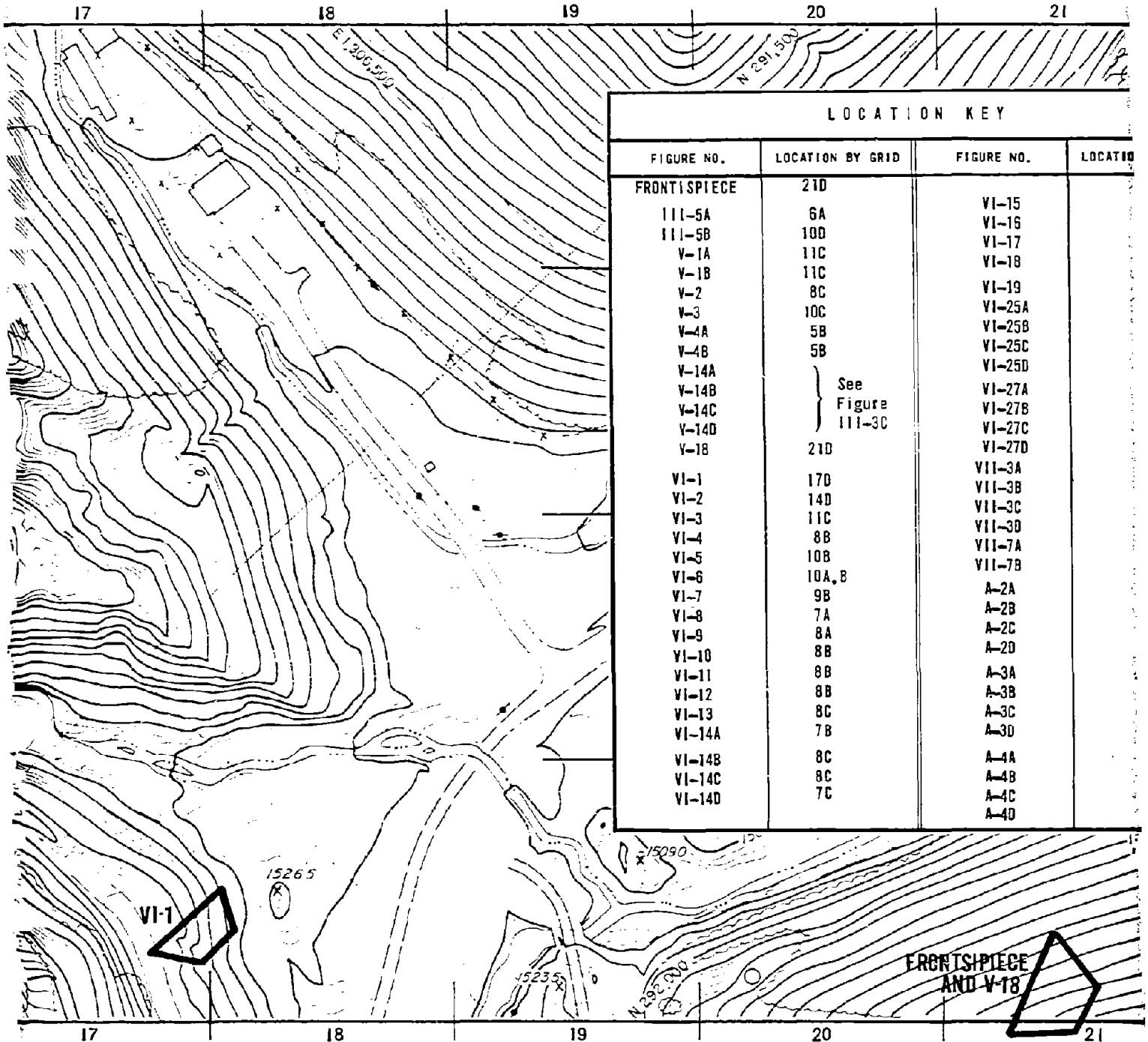
BASE MAP BY MICHAEL BAKER, JR., INC.
COMPILED FROM AERIAL PHOTOS FLOWN ON
4/9/72.





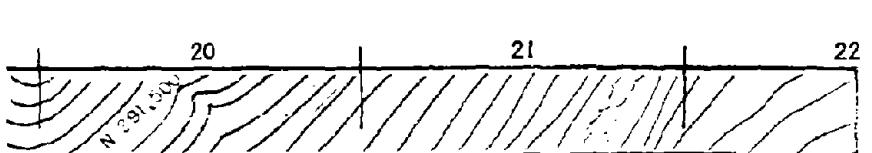


80 FEET



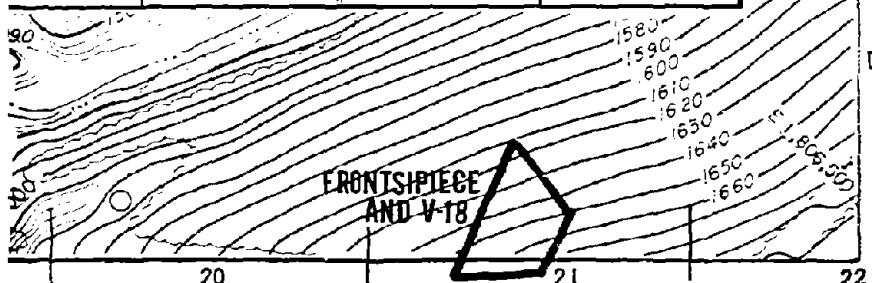
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& ASSOCIATES

COAL REFUSE
SAUNDERS, W. E.
PALO ALTO & NEWPORT



LOCATION KEY

SURE NO.	LOCATION BY GRID	FIGURE NO.	LOCATION BY GRID
TISPIECE	21D		
VI-5A	6A	VI-15	7C
VI-5B	10D	VI-16	8C
V-1A	11C	VI-17	5D
V-1B	11C	VI-18	4C
V-2	8C	VI-19	1B
V-3	10C	VI-25A	7B
V-4A	5B	VI-25B	9A
V-4B	5B	VI-25C	7B
V-14A		VI-25D	11C
V-14B	See Figure III-3C	VI-27A	6B
V-14C		VI-27B	7B
V-14D		VI-27C	4B
V-18	21D	VI-27D	9B
VI-1	17D	VII-3A	5A
VI-2	14D	VII-3B	7C
VI-3	11C	VII-3C	6B
VI-4	8B	VII-3D	5B
VI-5	10B	VII-7A	6A
VI-6	10A,B	VII-7B	6A
VI-7	9B	A-2A	5A
VI-8	7A	A-2B	5A
VI-9	8A	A-2C	5B
VI-10	8B	A-2D	5A
VI-11	8B	A-3A	7B
VI-12	8B	A-3B	7B
VI-13	8C	A-3C	5A
VI-14A	7B	A-3D	9B
VI-14B	8C	A-4A	8B
VI-14C	8C	A-4B	8B
VI-14D	7C	A-4C	7B
		A-4D	6B



KEY



AERIAL PHOTOGRAPH



SURFACE VIEW (NEAR-VERTICAL DOWNWARD).



SURFACE PHOTOGRAPH (NEAR-HORIZONTAL VIEW, SIZE OF HALF-HEXAGON ROUGHLY SCALED TO AREA OF VIEW).

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& ASSOCIATES

COAL REFUSE DAM FAILURE
SAUNDERS, WEST VIRGINIA

PALO ALTO • NEWPORT BEACH • CALIF.

PHOTOGRAPH LOCATIONS

PROJECT NO.	DATE	FIGURE NO.
0700	NOVEMBER 1972	A-1

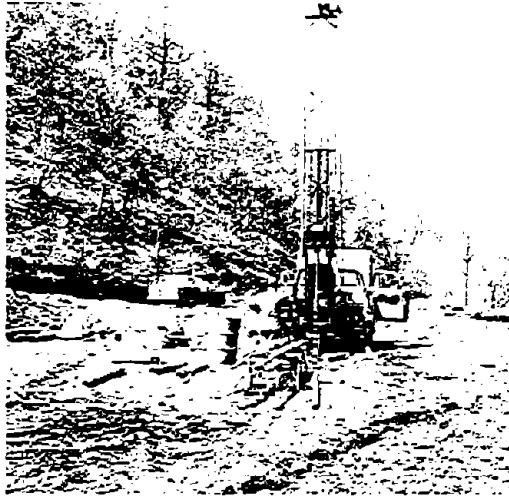


PHOTO A. CME-45 DRILL RIG USING HOLLOW STEM AUGERS ON HOLE S-1.

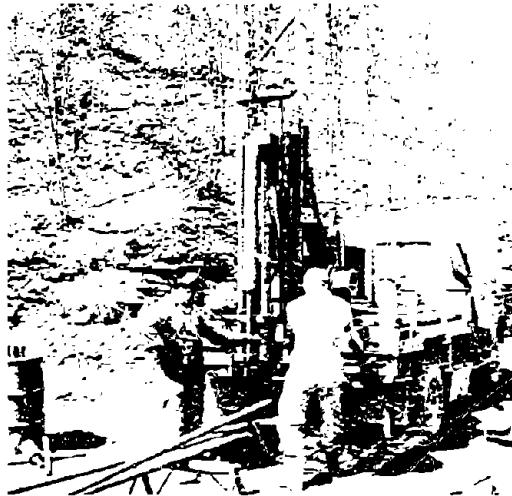


PHOTO B. STANDARD PENETROMETER TEST IN HOLE S-2.

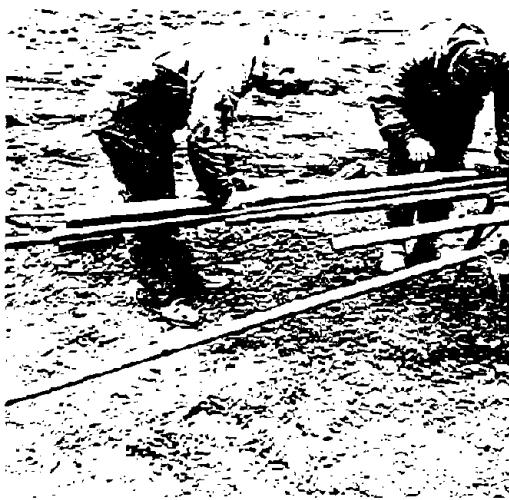


PHOTO C. SPECIAL DOUBLE-LENGTH SHELBY TUBE BEING REMOVED FROM SHELBY HEAD, HOLE S-8.

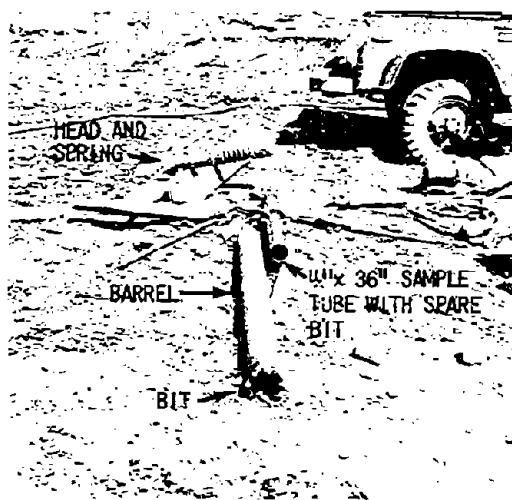


PHOTO D. PITCHER BARREL USED ON HOLE S-20. HERE DISASSEMBLED, PARTS LABELLED

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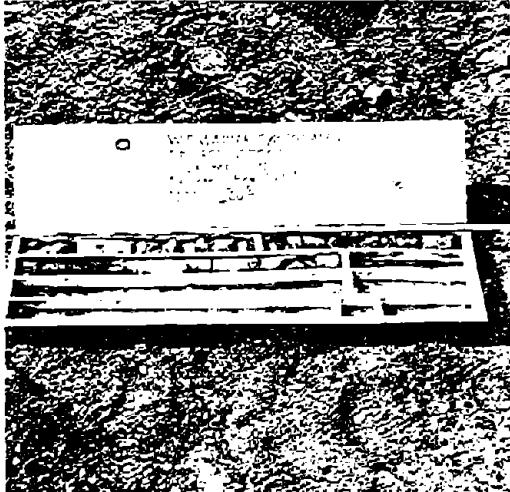


PHOTO A. CORE FROM HOLE S-11.

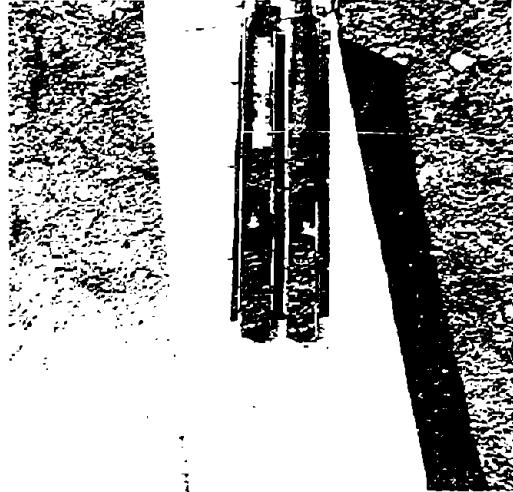


PHOTO B. STANDARD PENETROMETER RECOVERY.
HOLE S-11.

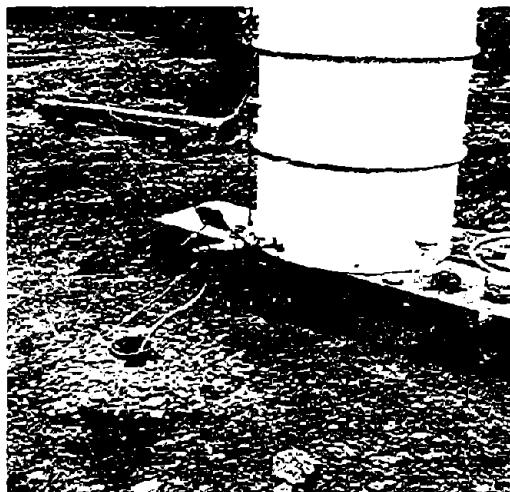


PHOTO C. TYPICAL FIELD PERMEABILITY TEST
SET-UP. FLOAT VALVE KEEPS CONSTANT HEAD
IN HOLE; WATER LEVEL IN BARREL IS READ
PERIODICALLY IN SIGHT TUBE.

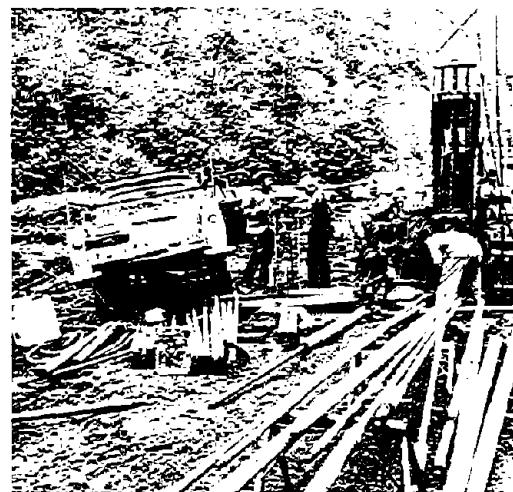


PHOTO D. PORTABLE VANE SHEAR EQUIPMENT
IN USE ADJACENT TO HOLE S-4. THE DRILL
RIG DRILLED A PILOT HOLE THROUGH THE
REFUSE DUMP TO THE UNDERLYING SLUDGE
FOR THE PORTABLE EQUIPMENT.

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PHOTO A. BACKHOE EXCAVATING PIT 2.



PHOTO B. WALL OF PIT 2. HAMMER HEAD IS
AT CONTACT OF DISPLACED POOL 2 SLUDGE
OVER IN-PLACE DAM NO. 2 ABANKMENT
GRAVELS. SEE ALSO PIT 2 LOG IN
FIGURE A-6.

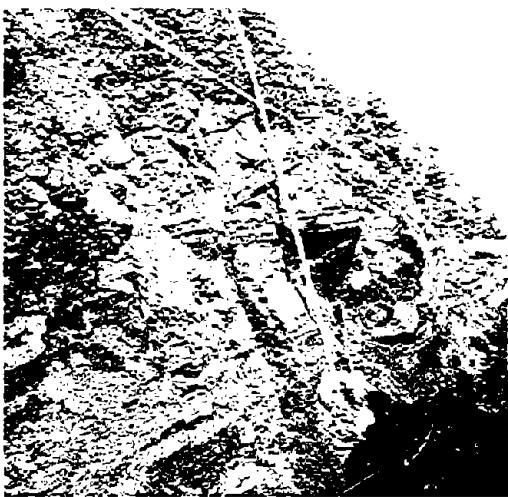


PHOTO C. PIT 7, GRAVEL OF DAM NO. 3 OVER-
LYING SLUDGE OF POOL 2. SEE ALSO PIT 7
LOG IN FIGURE A-6.



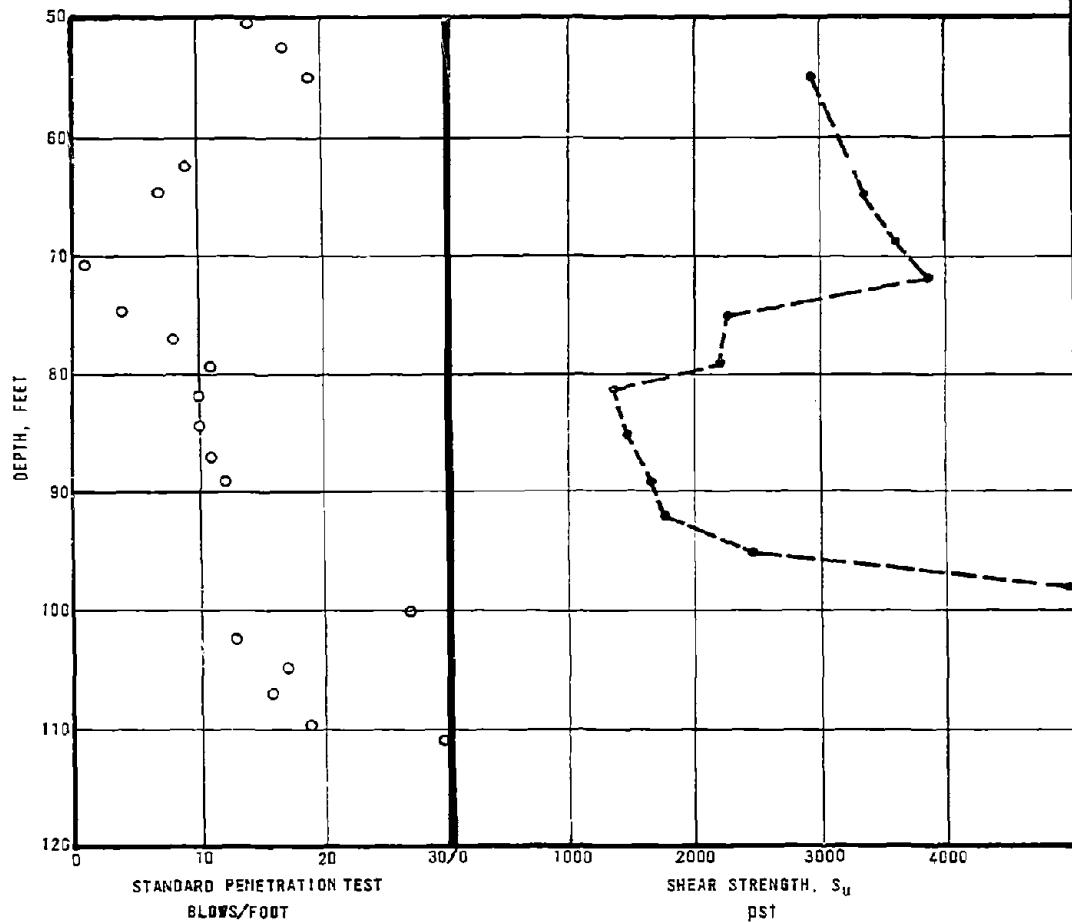
PHOTO D. EXPLORATORY BULLDOZER TRENCH
IN LEFT ABUTMENT REMNANT OF DAM NO. 3.
FIELD DENSITY TEST BEING SET UP IN
MIDDLEGROUND.

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& ASSOCIATES

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FIGURE A-4

SUFFALO CREEK, DAM NO. 2, V-1
PREDRILLED HOLE AT S-4 TO 52.0 FEET



NOTE: STANDARD PENETRATION TEST RESULTS IN ADJACENT DRILL HOLE GIVEN FOR COMPARISON.

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COAL REFUSE DAM FAILURE
SAUNDERS, WEST VIRGINIA

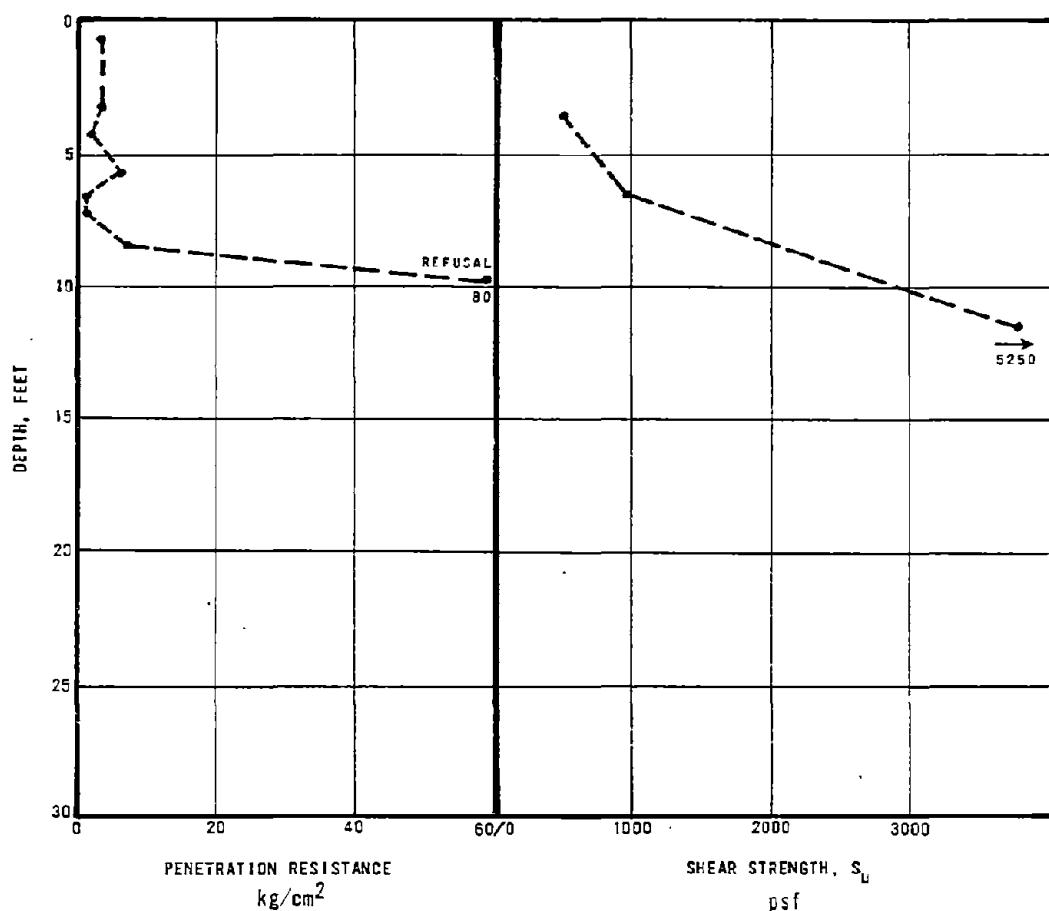
PALO ALTO • NEWPORT BEACH • CALIF.

FIELD VANE SHEAR AND (OR) CONE PENETROMETER TEST RESULTS

PROJECT NO.	DATE	FIGURE NO.
0708	NOVEMBER 1972	A-5

BUFFALO CREEK DAM NO. 3

PV-1

W.A. WAHLER
& ASSOCIATESCOAL REFUSE DAM FAILURE
SAUNDERS, WEST VIRGINIAFIELD VANE SHEAR AND (OR) CONE PENETROMETER
TEST RESULTS

PALO ALTO • NEWPORT BEACH • CALIF

PROJECT NO.

DATE

FIGURE NO.

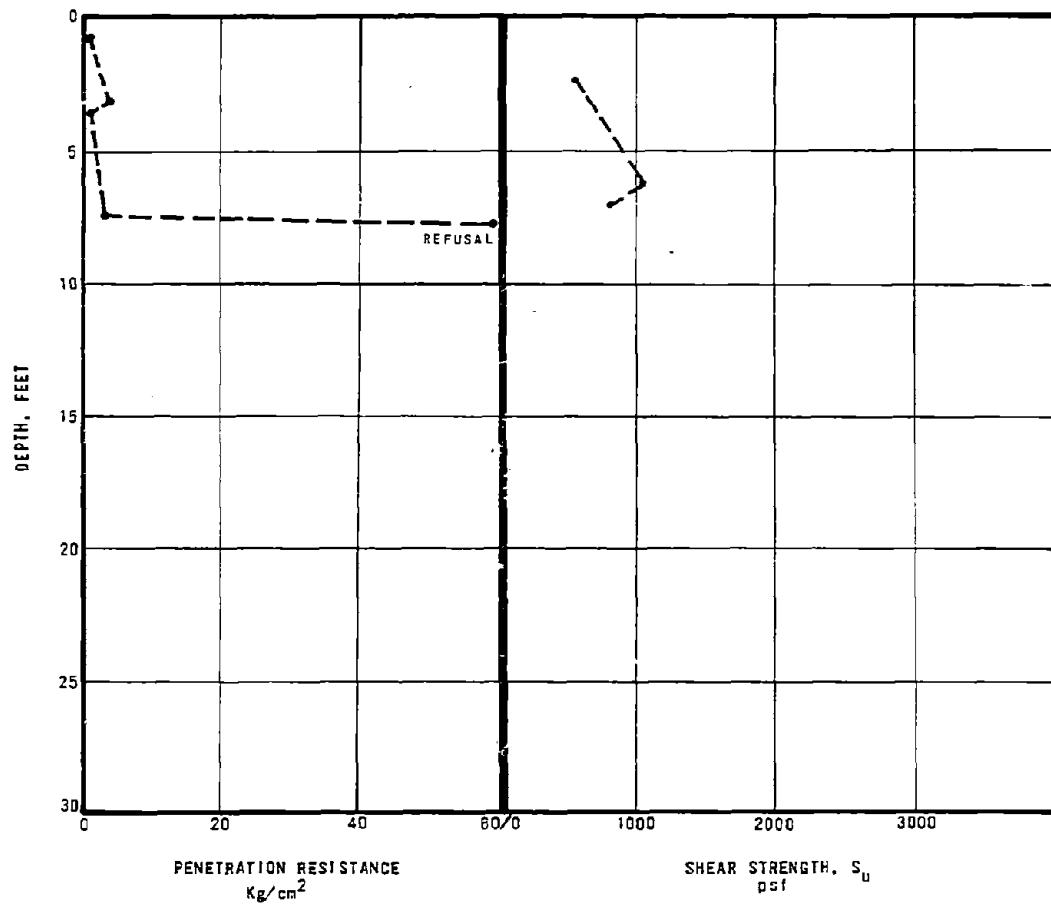
0700

NOVEMBER 1972

A-5

BUFFALO CREEK DAM NO.3

PV-2

W.A. WAHLER
& ASSOCIATESCOAL REFUSE DAM FAILURE
SAUNDERS, WEST VIRGINIA

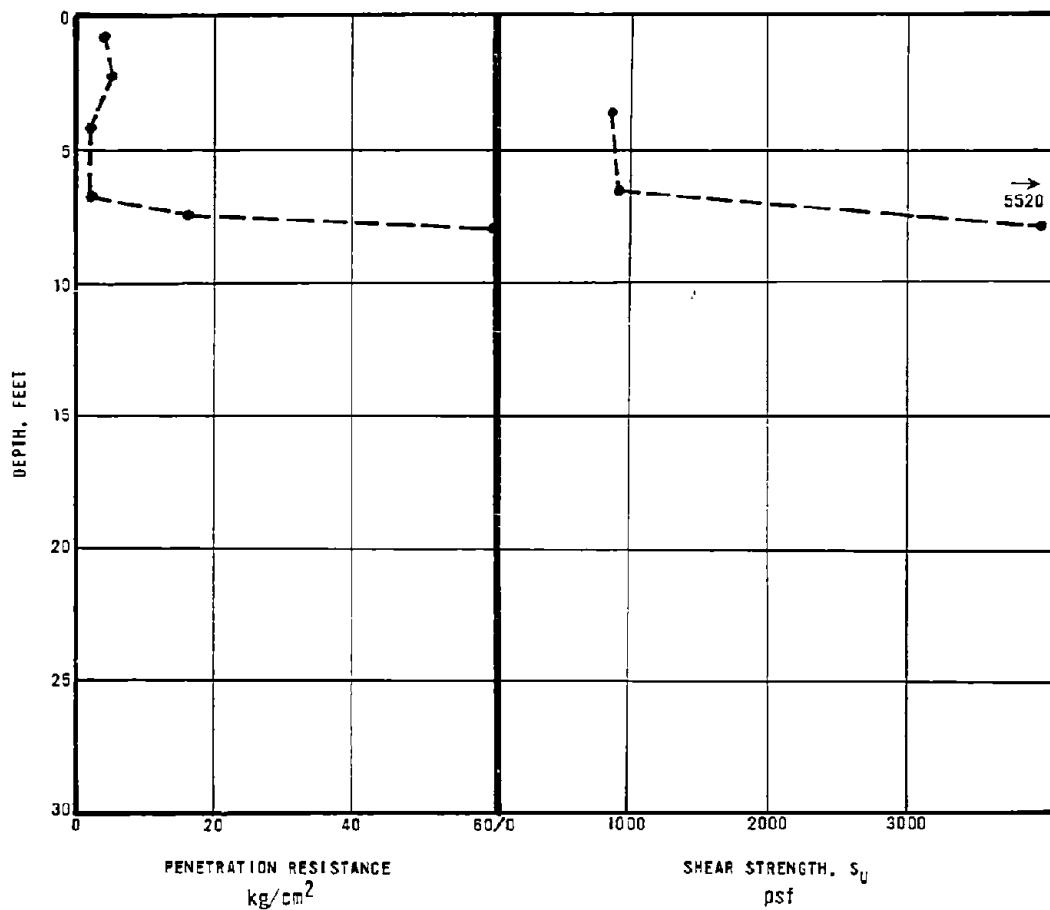
PALO ALTO • NEWPORT BEACH • CALIF.

FIELD VANE SHEAR AND (OR) CONE PENETROMETER
TEST RESULTS

PROJECT NO. 0700 DATE NOVEMBER 1972 FIGURE NO. A-5

BUFFALO CREEK DAM NO.3

PV-3



W. A. WAHLER
& ASSOCIATES

COAL REFUSE DAM FAILURE
SAUNDERS, WEST VIRGINIA

PALO ALTO • NEWPORT BEACH • CALIF.

FIELD VANE SHEAR AND (OR) CONE PENETROMETER
TEST RESULTS

PROJECT NO.

DATE

FIGURE NO.

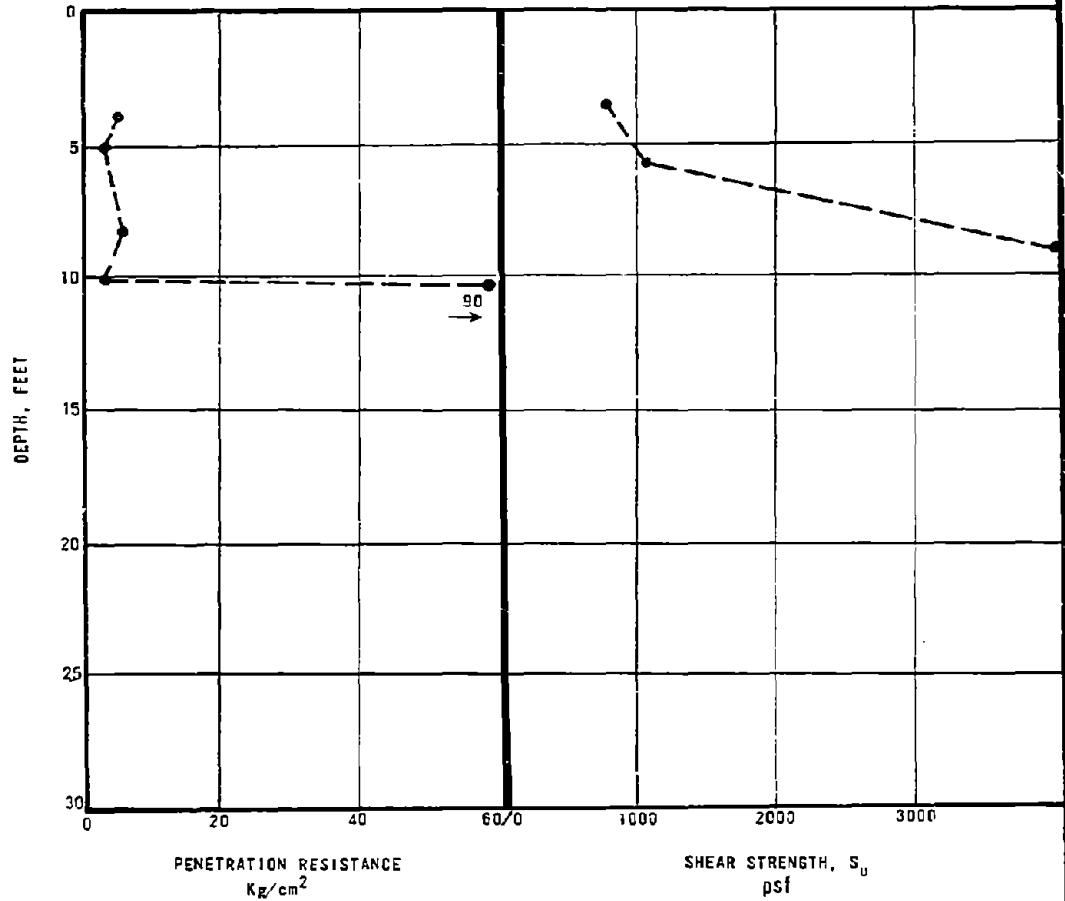
0700

NOVEMBER 1972

A-5

BUFFALO CREEK DAM NO.3

PV-4



W.A. WAHLER
& ASSOCIATES

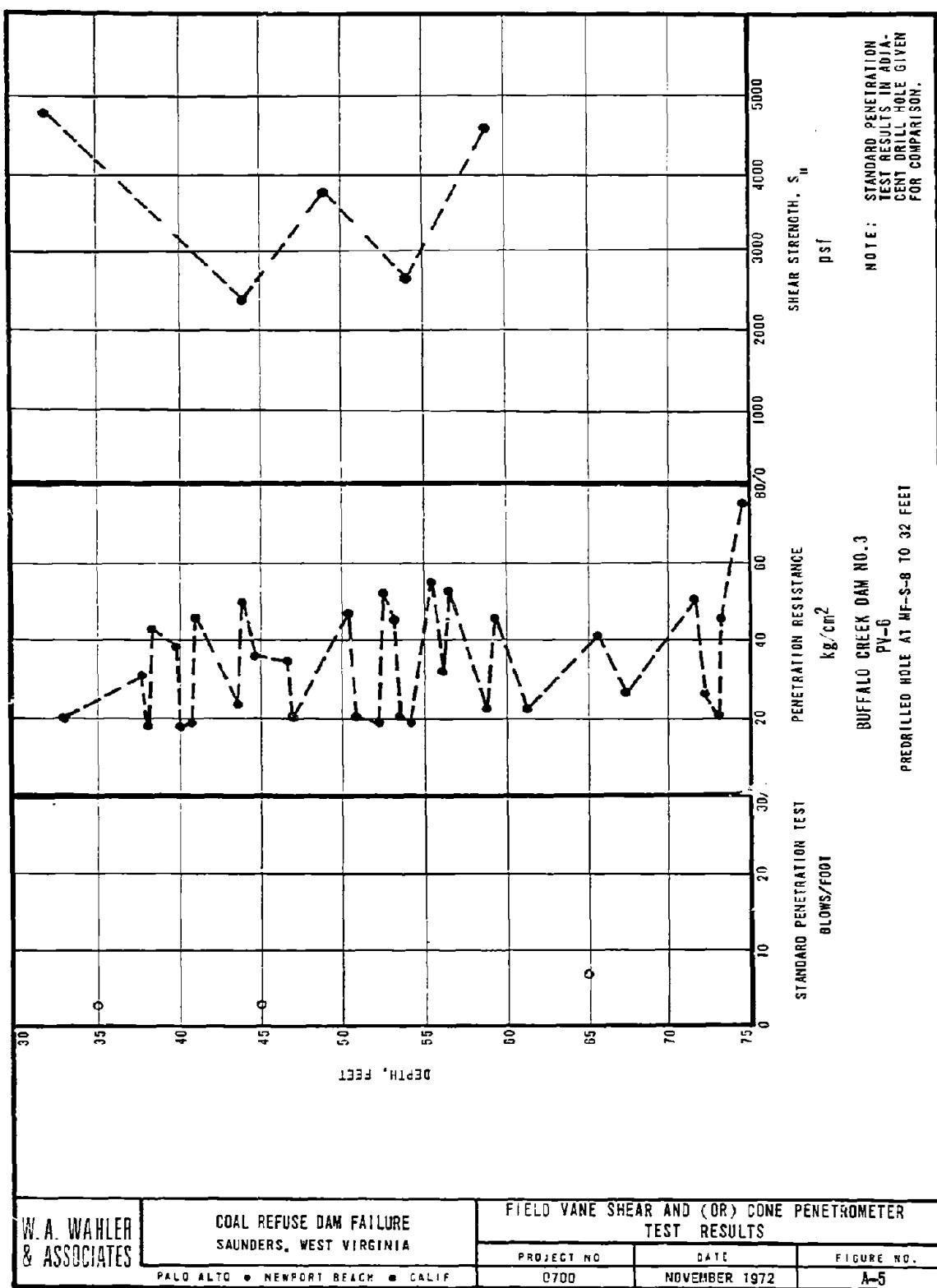
COAL REFUSE DAM FAILURE
SAUNDERS, WEST VIRGINIA

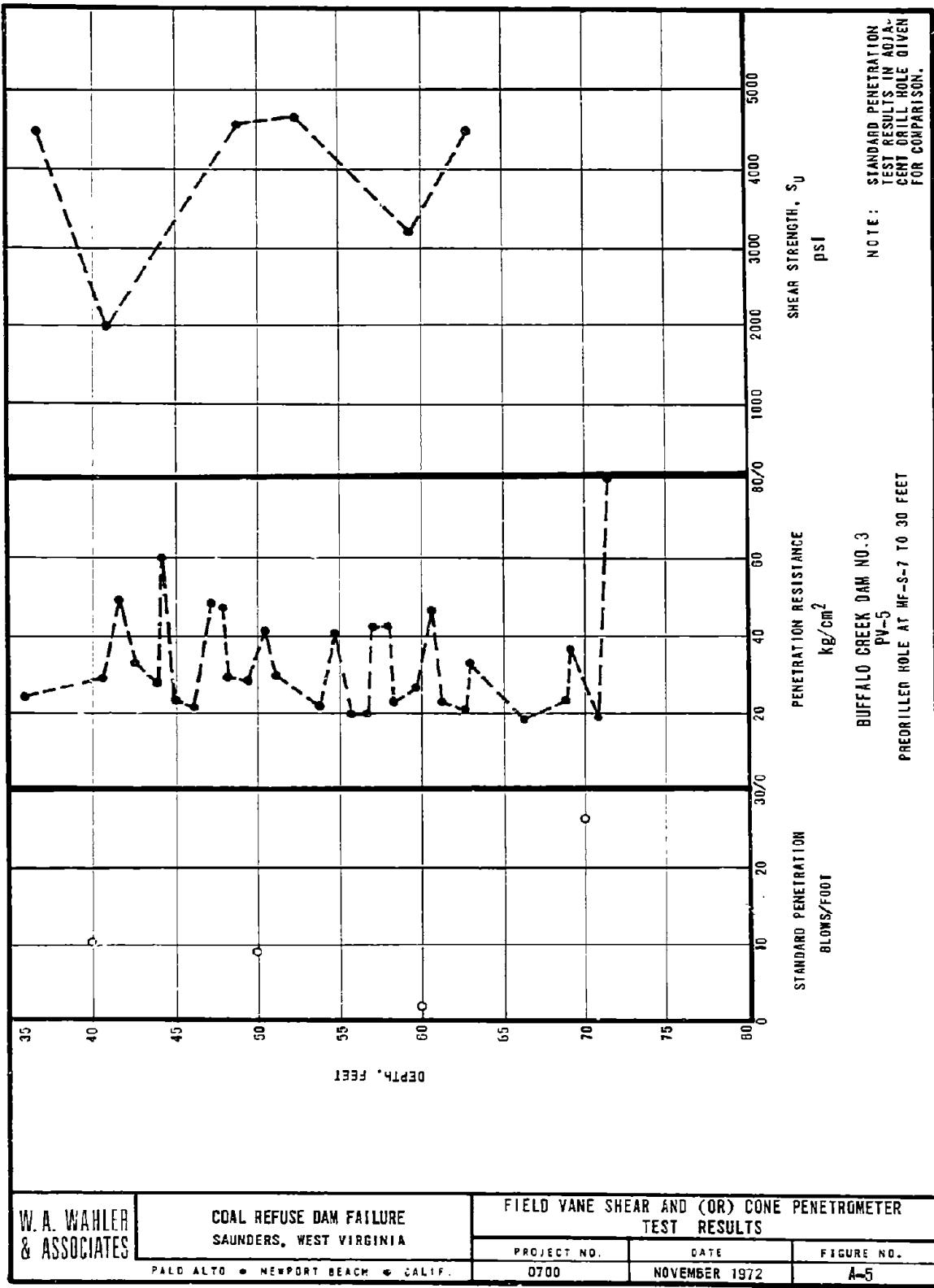
PALO ALTO • NEWPORT BEACH • CALIF.

FIELD VANE SHEAR AND (OR) CONE PENETROMETER
TEST RESULTS

PROJECT NO	DATE	FIGURE NO.
0700	NOVEMBER 1972	A-5

SHEET 5 OF 10

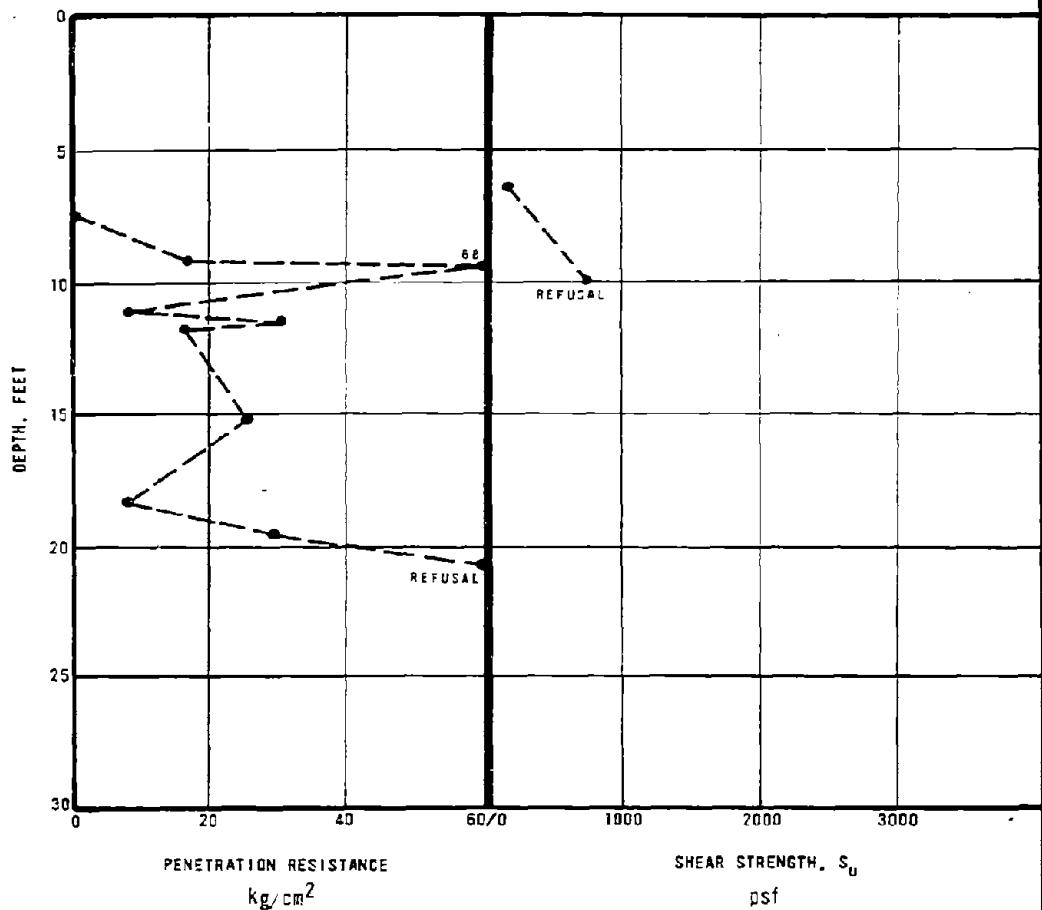




SHEET 7 OF 10

BUFFALO CREEK DAM NO. 4,

PV-1



W.A. WAHLER
& ASSOCIATES

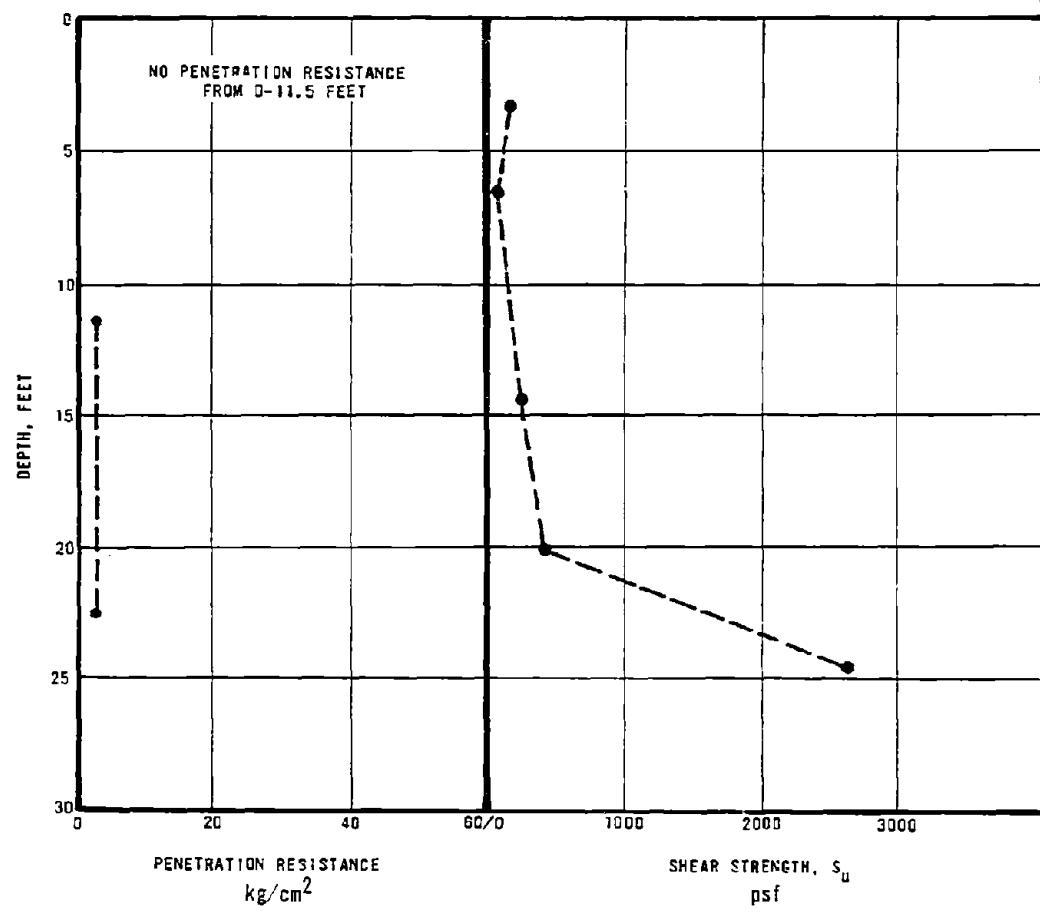
COAL REFUSE DAM FAILURE
SAUNDERS, WEST VIRGINIA

PALO ALTO • NEWPORT BEACH • CALIF

FIELD VANE SHEAR AND (OR) CONE PENETROMETER
TEST RESULTS

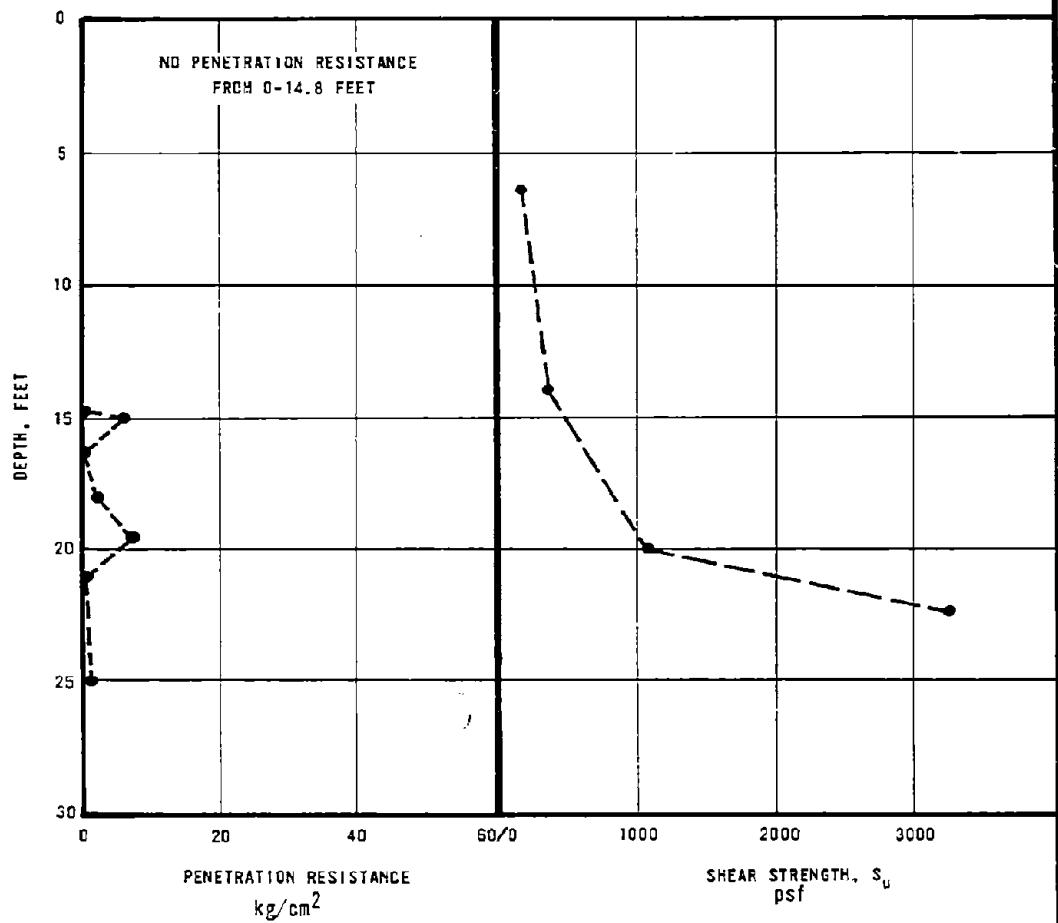
PROJECT NO.	DATE	FIGURE NO.
0700	NOVEMBER 1972	A-5

BUFFALO CREEK DAM NO.4
PV-2



W.A. WAHLER & ASSOCIATES	COAL REFUSE DAM FAILURE SAUNDERS, WEST VIRGINIA	FIELD VANE SHEAR AND (OR) CONE PENETROMETER TEST RESULTS		
		PROJECT NO.	DATE	FIGURE NO.
	PALO ALTO • NEWPORT BEACH • CALIF.	0700	NOVEMBER 1972	A-5

BUFFALO DAM NO.4
PV-3



W. A. WAHLER
& ASSOCIATES

COAL REFUSE DAM FAILURE
SAUNDERS, WEST VIRGINIA

PALO ALTO • NEWPORT BEACH • CALIF.

FIELD VANE SHEAR AND (OR) CONE PENETROMETER
TEST RESULTS

PROJECT NO.

DATE

FIGURE NO.

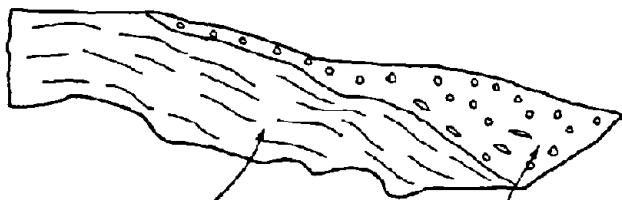
0700

NOVEMBER 1972

A-5

PIT NO. 1 NORTHEAST WALL

N68°W

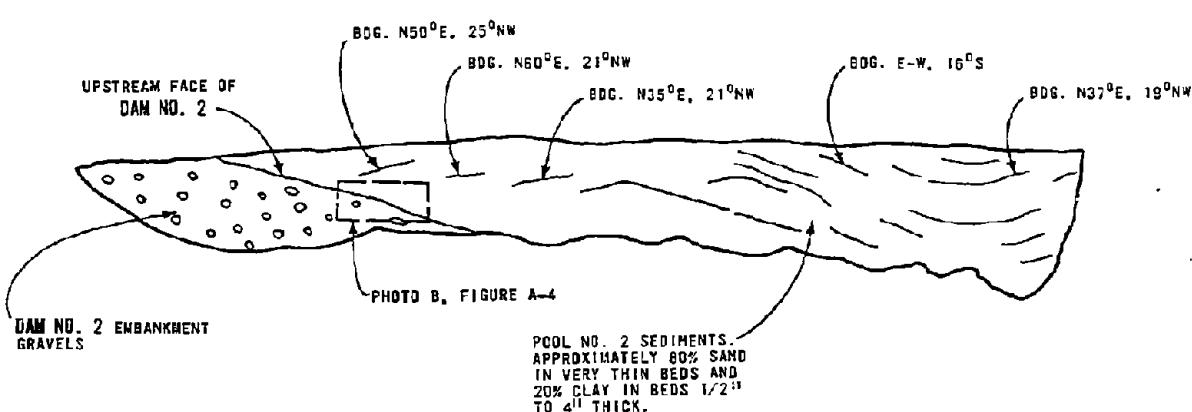


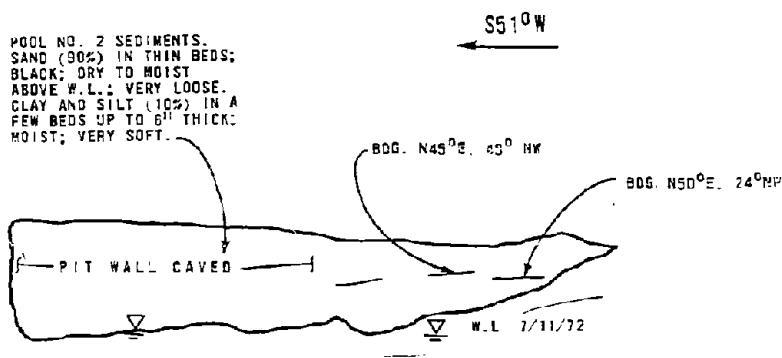
RESERVOIR SEDIMENT OF POOL NO. 2.
SAND; BLACK; VERY THINLY BEDDED;
DRY TO SLIGHTLY DAMP; VERY LOOSE.
BEDDING SLIGHTLY CONTORTED, SE
DIPS PREVAIL.

SANDY GRAVEL; BEDDING VAGUE. PIT
CUT AT RIGHT ANGLES TO STRIKE OF
GRAVEL-SAND CONTACT

PIT NO. 2 NORTHEAST WALL

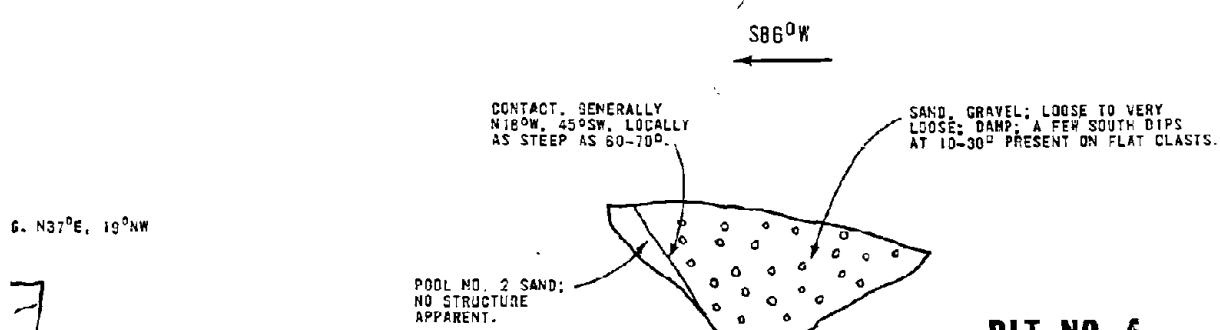
N50°W





PIT NO. 3 NORTHWEST WALL

(PIT CUT SUB-PARALLEL TO STRIKE OF
BEDDING. STRUCTURE OF SEDIMENTS
IS OBSCURE LARGELY FOR THIS REASON.)



PIT NO. 4 NORTH WALL



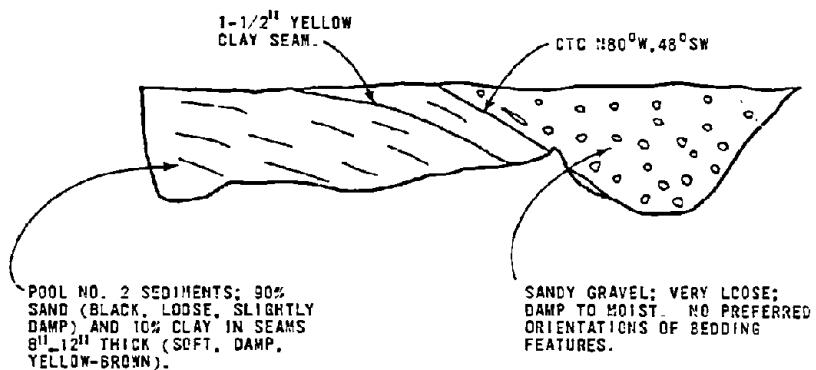
SEE SHEET 3 FOR NOTES AND ABBREVIATIONS.

W. A. WAHLER & ASSOCIATES	COAL REFUSE DAM FAILURE SAUNDERS, WEST VIRGINIA	BACKHOE PIT LOGS			28
		PROJECT NO.	DATE	FIGURE NO.	
PALO ALTO	NEWPORT BEACH	CALIF	O700	NOVEMBER 1972	A-6

SHEET 1 OF 3

PIT NO. 5 EAST WALL

N20°E ←



S55°E ←

PIT SOUTHWALL

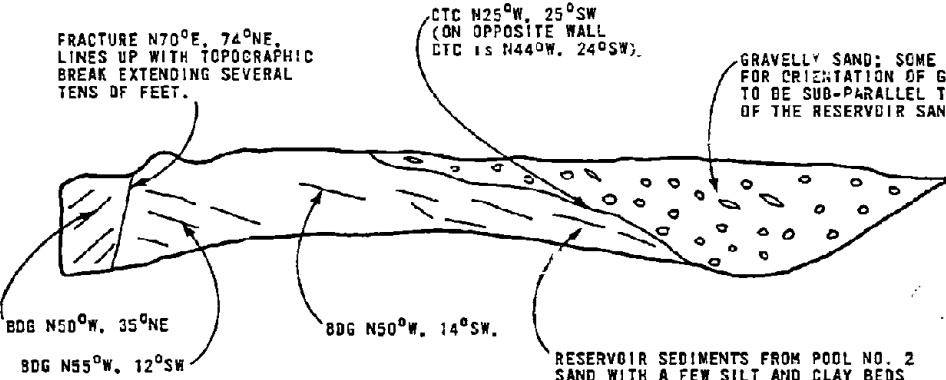
BOD. IN GRAVEL N55°E, 10°SE. ←

GRAVELLY SAND; SLIGHTLY DAMP; VERY LOOSE. SOME TENDENCY FOR SE DIPS AT 10°-20°.

N19°E ←

PIT NO. 6 SOUTHEAST WALL

DUE N ←



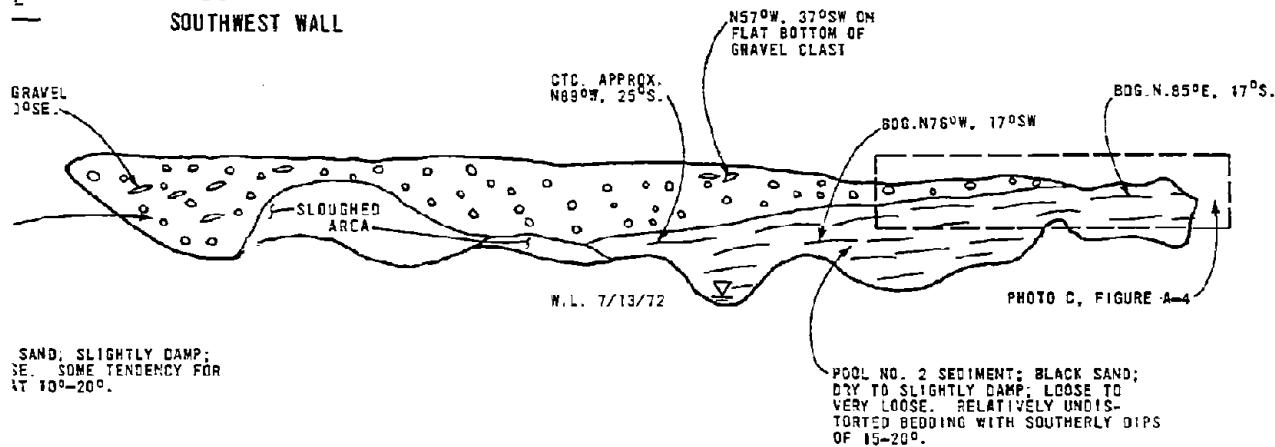
POOL
BLACK
DAMP

RESERVOIR SEDIMENTS FROM POOL NO. 2
SAND WITH A FEW SILT AND CLAY BEDS
(TO 3" THICKNESS). SAND IS BLACK,
LAMINATED TO VERY TRINLY BEDDED,
DRY TO SLIGHTLY DAMP, LOOSE TO VERY
LOOSE. SILTY CLAYS ARE MOIST AND
VERY SOFT, GENERALLY DARK GRAY;
ONE BED IS YELLOW-BROWN.

W.
G.

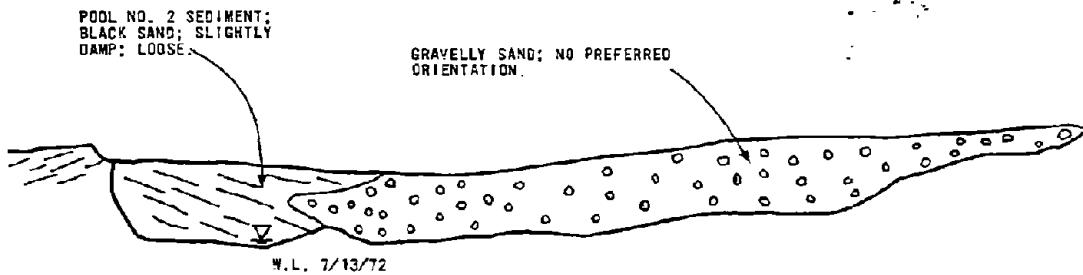
E

PIT NO. 7
SOUTHWEST WALL



DUE N

PIT NO. 8
EAST WALL



SCALE
10 0 10 FEET
HORIZONTAL = VERTICAL

SEE SHEET 3 FOR NOTES AND ABBREVIATIONS.

W. A. WAHLER & ASSOCIATES	COAL REFUSE DAM FAILURE SAUNDERS, WEST VIRGINIA	BACKHOE PIT LOGS		
		PROJECT NO.	DATE	FIGURE NO.
	PALO ALTO NEWPORT BEACH CALIF	0700	NOVEMBER 1972	A-6

SHEET 2 OF 3

S40°E

SANDY GRAVEL; DRY TO SLIGHTLY DAMP; LOOSE TO VERY LOOSE.

POOL NO. 2 SEDIMENT; SLIGHTLY CLAYEY AND SILTY SAND; VERY LOOSE; SLIGHTLY DAMP.

TREE TRUNK OR BRANCH.

SEEP.

BDC N50°E, 34°SE ON YELLOW CLAY LAYER.

PIT NO. 9 SOUTHWEST WALL

N40°W

GRAVEL, SLIGHTLY SANDY AND CLAYEY; GENERALLY HORIZONTALLY BEDDED; LOOSE TO VERY LOOSE; DAMP TO MOIST.

MIDDLE FORK

GRAVEL WITH RED DOG

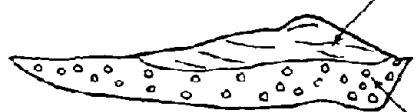
GRAVEL WITH RED DOG

NOTE: PIT IS FREE OF STANDING WATER AND SEEPS EVEN THOUGH MIDDLE FORK IS NEAR

PIT NO. 10 NORTHEAST WALL

EDIMENT; SLIGHTLY
ILTY SAND; VERY
LY DAMP.

N41°W



SAND SLUDGE "RAFT", CONTORTED
BEDDING GENERALLY DIPPING
30° OR LESS. SLIGHTLY DAMP,
LOOSE TO VERY LOOSE.

GRAVEL, CLEAN; NO BLACK SAND;
HORIZONTAL BEDDING; DAMP TO
WET; VERY LOOSE.

PIT NO. 11 NORTHEAST WALL

MIDDLE
FORK

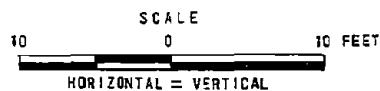
IS FREE OF STANDING
TER AND SEEPS EVEN
OUGH MIDDLE FORK IS NEARBY.

NOTES: 1. SOIL DESCRIPTIONS ARE BASED ON UNIFIED SOIL
CLASSIFICATION (SEE KEY TO DRILL HOLE LOGS
IN THIS APPENDIX).

2. ABBREVIATIONS: BDG = BEDDING ATTITUDE
CTC = CONTACT

3. FIRST FIGURE OF BEDDING ATTITUDE IS THE STRIKE,
SECOND FIGURE IS THE DIP. EXAMPLE:
BDG N50°E, 34°SE = BEDDING ATTITUDE: STRIKE
N50°E, DIP 34°SE.

4. FOR LOCATION OF BACKHOE PITS SEE DRAWING NO. VI-20.



W. A. WAHLER & ASSOCIATES	COAL REFUSE DAM FAILURE SAUNDERS, WEST VIRGINIA PALO ALTO NEWPORT BEACH CALIF.	BACKHOE PIT LOGS			20 FIGURE NO. A-B
		PROJECT NO.	DATE	FIGURE NO.	
		0700	NOVEMBER 1972		

SHEET 3 OF 3

TABLE NO. A-1
DRILL HOLE SUMMARY
[FOR NOTES AND ABBREVIATIONS, SEE SHEET 2 OF 3]

HOLE NO.	DATE(S) DRILLED	TOTAL DEPTH (ft)	DEPTH TO... (ft)			ELEVATION AT COLLAR (ft)	LOCATION
			SLUDGE	SOIL TOP	BEDROCK SURFACE		
S-1	4/5-8/72	41.5	N.E.	29.0	32.5	1764.5	DAM NO. 3, LEFT ABUTMENT
2	4 6-12 72	56.0	N.E.	39.0	43.5	1763.6	DAM NO. 3, LEFT ABUTMENT
3	4. 13-18 72	66.0	N.E.	?	47.0	1762.5	DAM NO. 3, LEFT ABUTMENT
4	4. 19-5 6 72	126.0	58.0	111.0	113.0	1692.0	DAM NO. 2, REFUSE BANK
5	6 25-27 72	111.8	56.0	96.0	100.5	1690.0	DAM NO. 2, NOSE REMNANT
6	5. 8-10 72	51.5	33.0E	34.0E	36.5	1706.0	DAM NO. 3, RIGHT CHANNEL
7	5 12-16 72	106.0	28.0E	80.0E	83.0	1702.0	DAM NO. 3, CENTER CHANNEL
8	5 17-18 72	86.0	32.0	69.0E	70.0	1707.0	DAM NO. 3, LEFT CHANNEL
9	5 10-22 72	105.0	34.0	?	86.0	1704.0	DAM NO. 3, CENTER CHANNEL UPSTREAM
10	5. 24-6 2 72	120.0	75.0	?	109.5	1701.0	DAM NO. 3, CENTER CHANNEL DOWNSTREAM
11	6. 5-9 72	120.5	79.0	108.0	112.0	1703.0	DAM NO. 3, CENTER CHANNEL DOWNSTREAM TOE
12	6 28, 7 10-14 72	174.0	N.E.	N.E.?	28.0	1750.0	DAM NO. 3, RIGHT ABUTMENT
13	7. 13-19 72	115.0	N.E.	94.0	102.0	1657.0	DAM NO. 1, LEFT ABUTMENT REFUSE BANK
14	7 19-24 72	115.5	34.0	104.0	115.5	1692.0	POOL 2
15	7 19-25 72	76.0	27.5	N.E.?	74.0	1657.0	POOL 1
16	7 27 72	81.5	68.0	80.5	81.5	1700.0	DAM NO. 3, CENTER CHANNEL DOWNSTREAM
17	7 24-25 72	70.0	33.0	N.E.	60.0	1700.0	POOL 2, LEFTSIDE
18	7 27-28 72	66.5	65.5	N.E.	N.E.	1695.0	POOL 2, CENTER, UPPER END
19	7 25-26 72	70.0	48.5	N.E.	68.0	1688.0	POOL 2, RIGHT SIDE
20	7 27-28 72	14.0	N.E.	N.E.	N.E.	1763.0	DAM NO. 3, LEFT ABUTMENT
21	7 27 72	85.5	50.0	N.E.	N.E.	1701.0	DAM NO. 3, CENTER CHANNEL DOWNSTREAM
22	7 31 72	41.5	40.0	N.E.	N.E.	1701.0	DAM NO. 3, CENTER CHANNEL DOWNSTREAM
TOTAL		1879.8					
BS-1	5/2/72	31.4	N.E.	~28.0	31.4	1763.4	DAM NO. 3, LEFT ABUTMENT
2	5/2/72	26.5	N.E.	~24.0	26.5	1764.0	DAM NO. 3, LEFT ABUTMENT
3	5/2/72	25.7	N.E.	~22.0	25.7	1764.3	DAM NO. 3, LEFT ABUTMENT
4	5/2/72	26.0	N.E.	~23.0	26.0	1765.0	DAM NO. 3, LEFT ABUTMENT
5	5/2/72	37.0	N.E.	~35.0	37.0	1696.0	DAM NO. 2, REFUSE BANK
6	5/2, 6/23/72	81.0	~60.0	~79.0	~80.0	1694.0	DAM NO. 2, REFUSE BANK
7	5/2, 6/24/72	125.0	~60.0	95E	100E	1693.0	DAM NO. 2, REFUSE BANK
8	5/2/72	15.0	N.E.	N.E.?	10-15E	1705.0	DAM NO. 3, RIGHT CHANNEL AREA
9	5/3, 10/72	37.5	~30.0	?	67.5	1704.0	DAM NO. 3, CENTER CHANNEL AREA
10	5/3, 10/72	89.0	?	?	89.0	1704.0	DAM NO. 3, CENTER CHANNEL AREA
11	5/3/72	58.0	N.E.?	54.0E	58.0	1716.0	DAM NO. 3, LEFT CHANNEL AREA
12	5/2/72	39.5	N.E.	36.0E	39.5	1728.0	DAM NO. 3, LEFT CHANNEL AREA
13	5/2, 11/72	81.0	~30.0	80.5E	81.0	1706.0	DAM NO. 3, CENTER CHANNEL AREA
14	5/3, 11/72	99.5	?	90-96E	99.5	1700.0	DAM NO. 3, CENTER CHANNEL AREA
15	5/3/72	40.5	N.E.?	?	40.5	1702.0	DAM NO. 3, RIGHT CHANNEL AREA

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& ASSOCIATES

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TABLE A-1
Sheet 1 of 3

TABLE NO. A-1 — CONTINUED

DRILL HOLE SUMMARY

HOLE NO.	DATES(S) DRILLED	TOTAL DEPTH (ft)	DEPTH TO... (ft)			ELEVATION AT COLLAR (ft)	LOCATION
			SLUDGE	SOIL TOP	BEDROCK SURFACE		
BS-16	5/3/72	46.5	?	?	46.5	1709.0	DAM NO. 3, RIGHT CHANNEL AREA
17	5/3, 11/72	64.5	?	?	64.0E	1698.0	DAM NO. 3, LEFT CHANNEL AREA
18	5/3/72	38.5	N.E.?	?	38.5	1720.0	DAM NO. 3, LEFT CHANNEL AREA
19	7/18/72	20.5	----	?	20.5E	1500.0	TOE OF REFUSE BANK AT BUFFALO CREEK.
TOTAL		1012.5					
P-1	5/4/72	65.0				1692.0	5' WEST OF S-4
2	5/23/72	35.0				1702.0	ADJACENT TO S-7
3	5/23/72	35.0				1707.0	ADJACENT TO S-8
4	5/23/72	35.0				1702.0	ADJACENT TO S-7
5	5/23/72	35.0				1707.0	ADJACENT TO S-8
TOTAL		205.0					

NOTES

1. FOR LOCATION OF DRILL HOLES, EXCEPT BS-19 SEE FIGURE VI-20
BS-19 IS SHOWN ON FIGURE III-2A
2. ELEVATIONS ARE APPROXIMATE; THEY MAY NOT MATCH THE INDICATED ELEVATION ON FIGURE VI-20 DUE TO PAD CUT OR FILL.
3. ABBREVIATIONS AND SYMBOLS: N.E. = NOT ENCOUNTERED;
E = ESTIMATED; ~ = APPROXIMATE; ? = NOT DETECTED OR UNKNOWN
4. SEE FOLLOWING PAGE FOR FP SERIES HOLES.

W.A. WAHLER
& ASSOCIATES

TABLE A-1
Sheet 2 of 3

TABLE NO. A-1 — CONTINUED
DRILL HOLE SUMMARY

HOLE NO.	DATE(S) DRILLED	TOTAL DEPTH (ft)	$K_{20^{\circ}C}$ (cm/sec)	LOCATION
FP-1A	5/12/72	20.0	2.42×10^{-4}	ALL FP-SERIES HOLES ARE ON THE LEFT ABUTMENT REMNANT OF DAM NO. 3 AND THEIR LOCATIONS ARE PLOTTED ON FIGURE VI-20.
2A	5/15/72	40.0	---	
3A	5/24-25/72	10.5	---	
4A	5/31/72	25.0	---	
5A	6/2/72	35.5	---	
6A	7/17/72	15.0	*	
7A	7/18/72	15.0	2.17×10^{-4}	
7A	7/20/72		1.79×10^{-4}	
8A	7/21/72	15.2	1.35×10^{-4}	
9A	7/26-27/72	4.9	**	
10A	7/25-26/72	4.5	4.64×10^{-5}	
11A	7/24-25/72	4.0	4.83×10^{-5}	
12A	7/27/72	6.8	*	
13A	7/28/72	4.9	2.85×10^{-4}	
14A	7/31/72	4.2	4.15×10^{-4}	
TOTAL	-----	205.5		
GRAND TOTAL	-----	3302.9		

* NO USEFUL DATA OBTAINED. SEE FIELD PERMEABILITY TEST RESULTS IN THIS APPENDIX FOR DETAILS.

** STANDARD TEST NOT RUN, BUT A TRAVEL-TIME TEST WAS MADE. SEE FIELD PERMEABILITY TEST RESULTS HEREIN.

W. A. WAHLER
& ASSOCIATES

TABLE A-2
SUMMARY
OF
FIELD DENSITY TEST RESULTS

TEST NO.	LOCATION**	DEPTH (ft)	SAMPLE DESCRIPTION	FIELD		LABORATORY*		FIELD DENSITY AS % OF LAB. MAX.
				MOISTURE CONTENT (%)	DRY DENSITY (pcf)	OPTIMUM MOISTURE CONTENT(%)	MAXIMUM DRY DENSITY(pcf)	
1	BC-3, 155' UPSTREAM FROM C. FROM LEFT ABUTMENT.	0.5	DARK GRAY, SILTY SAND (SM)	7.9	100.6	11.0	96.8	104.0
2	SAME AS ABOVE	1.5	SAME AS ABOVE	7.2	99.8	11.0	96.8	103.0
3	29' UPSTREAM FROM C. FROM LEFT ABUTMENT OF BC-3.	0.5	SAME AS ABOVE	8.4	81.3	11.0	96.8	84.0
4	37' DOWNSTREAM FROM C. FROM LEFT ABUTMENT OF BC-3.	0.5	SAME AS ABOVE	7.6	93.8	11.0	96.8	97.0
5	SAME AS ABOVE	1.5	SAME AS ABOVE	9.4	97.0	11.0	96.8	100.0
6	142' DOWNSTREAM FROM C. FROM LEFT ABUTMENT OF BC-3.	0.5	SAME AS ABOVE	8.0	88.6	11.0	96.8	92.0
7	SAME AS ABOVE	1.5	SAME AS ABOVE	9.6	80.2	11.0	96.8	83.0
8	GOB PILE AT BC	0.5	DARK GRAY, SILTY SAND (SM)	9.0	99.2	7.5	106.2	93.0
9	SAME AS ABOVE	1.5	SAME AS ABOVE	7.6	100.6	7.5	106.2	95.0
10	TAILS BY LEFT ABUTMENT OF BC-2***	0.5	BLACK, SANDY SILT (ML)	36.8	50.1	9.0	56.4	89.0
11	NATURAL MATERIAL ON SLOPE ABOVE BC-2.	0.3	LIGHT BROWN, GRAVELLY, SANDY SILT (ML)	20.7	60.0	12.5	118.2	51.0
12	SMALL REMNANT OF BC-1	1.0	DARK GRAY, SILTY SAND (SM)	6.8	96.6	7.7	106.2	91.0
13	TAILS AT BC-2 LEFT ABUTMENT 25' UPSTREAM OF HOLE #4. ***	0.8	BLACK, SANDY SILT (ML)	35.2	37.6	9.0	56.0	67.0

* COMPACTIVE ENERGY = 20,000 FT.LB./FT.³

** SEE FIG. VI-20 FOR TEST LOCATION.

*** POSSIBLY DISTURBED - TEST TAKEN IN
TRANSLATED MASS.

TABLE A-2
Sheet 1 of 4

W. A. WAHLER
& ASSOCIATES

TABLE A-2--CONTINUED
SUMMARY
OF
FIELD DENSITY TEST RESULTS

TEST NO.	LOCATION**	DEPTH (ft)	SAMPLE DESCRIPTION	FIELD		LABORATORY*		FIELD DENSITY AS % OF LAB. MAX.
				NO. STORE CONTENT (%)	DRY DENSITY (pcf)	OPTIMUM MOISTURE CONTENT(%)	MAXIMUM DRY DENSITY(pcf)	
14	TAILS AT BC-2 LEFT ABUTMENT, 25' UPSTREAM OF HOLE #4***	0.8	BLACK, SANDY SILT (ML)	45.0	45.6	9.0	56.0	81.0
15	GOB PILE, LOWER SECTION	1.0	DARK GRAY, SILTY SAND (SM)	13.4	64.1	7.5	106.2	60.0
16	NATURAL MATERIAL ABOVE LEFT ABUTMENT BC-3.	0.4	LIGHT BROWN, GRAVELY, SANDY SILT (ML)	18.9	82.5	12.5	118.2	70.0
1A	BC-4 TAILS, 50' UPSTREAM FROM CREST.	0	BLACK, SILTY SAND (SM)	32.1	77.4	20.0	74.3	104.0
2A	BC-4 TAILS, 100' UPSTREAM, 10' FROM RIGHT ABUTMENT.	0	SAME AS ABOVE	24.3	58.4	20.0	74.3	79.0
3A	BC-4 CREST, C., 25' IN FROM LEFT ABUTMENT.	1.0	LIGHT GRAY, SILTY GRAVEL (GM)	7.5	99.8	10.0	110.2	91.0
4A	BC-4 CREST, C., 10' IN FROM RIGHT ABUTMENT.	1.0	SAME AS ABOVE	10.4	107.6	10.0	110.2	98.0
5A	BC-3 RIGHT ABUTMENT, 15' UPSTREAM FROM C..	1.0	LIGHT GRAY, SILTY SAND (SM)	5.5	98.4	11.0	104.2	94.0
6A	BC-3 RIGHT ABUTMENT, 20' DOWNSTREAM FROM C..	1.0	SAME AS ABOVE	6.9	91.4	11.0	104.2	88.0
7A	BC-3 DOZER CUT TRENCHES IN CHANNEL EMBANKMENT.	5.1	LIGHT GRAY, SILTY, SANDY GRAVEL (GM-GP)	9.5	84.2	10.0	118.3	71.0
8A	SAME AS ABOVE	6.8	SAME AS ABOVE	6.8	104.7	10.0	118.3	89.0
9A	SAME AS ABOVE	4.3	SAME AS ABOVE	7.9	96.8	10.0	118.3	82.0
10A	SAME AS ABOVE	3.9	SAME AS ABOVE	5.8	90.5	10.0	118.3	77.0
11A	SAME AS ABOVE	3.5	SAME AS ABOVE	6.0	100.6	10.0	118.3	85.0

* COMPACTIVE ENERGY = 20,000 FT LBS./FT³

** SEE FIG. VI-20 FOR TEST LOCATIONS.

*** POSSIBLY DISTURBED - TEST TAKEN IN
TRANSLATED MASS.

TABLE A-2
Sheet 2 of 4

TABLE A-2--CONTINUED
SUMMARY
OF
FIELD DENSITY TEST RESULTS

TEST NO.	LOCATION**	DEPTH (ft)	SAMPLE DESCRIPTION	FIELD		LABORATORY*		FIELD DENSITY AS % OF LAB. MAX.
				MOISTURE CONTENT (%)	DRY DENSITY (pcf)	OPTIMUM MOISTURE CONTENT (%)	MAXIMUM DRY DENSITY (pcf)	
12A	BC-3 DOZER CUT TRENCHES IN CHANNEL EMBANKMENT.	3.3	LIGHT GRAY, SILTY, SANDY GRAVEL (GM-GP) SAME AS ABOVE	4.7	96.7	10.0	118.3	82.0
13A	SAME AS ABOVE	3.1	SAME AS ABOVE	5.2	87.3	10.0	118.3	74.0
14A	BC-3 DOZER CUT TRENCH IN LEFT ABUTMENT.	5.0	LIGHT GRAY, SILTY, GRAVELLY SAND (SM-SP)	9.3	80.5	9.6	115.4	70.0
15A	SAME AS ABOVE	10.0	SAME AS ABOVE	8.2	93.5	9.0	115.4	81.0
16A	SAME AS ABOVE	15.0	SAME AS ABOVE	6.3	103.8	9.0	115.4	90.0
17A	SAME AS ABOVE	20.0	SAME AS ABOVE	5.0	88.8	9.0	115.4	77.0
18A	SAME AS ABOVE	35.0	LIGHT GRAY, SILTY, GRAVELLY SAND (SM)	11.4	84.0	9.0	94.6	89.0
19A	SAME AS ABOVE	30.0	BLACK, SILTY, SANDY GRAVEL (GM)	12.1	89.4	12.5	96.2	93.0
20A	SAME AS ABOVE	25.0	LIGHT GRAY, SILTY, GRAVELLY SAND (SM)	11.0	98.0	9.0	94.6	104.0
21A	SAME AS ABOVE	20.0	BLACK, SILTY, SANDY GRAVEL (GM)	10.5	92.0	12.5	96.2	96.0
22A	SAME AS ABOVE	15.0	LIGHT GRAY, SILTY, GRAVELLY SAND (SM)	9.4	83.4	9.0	94.6	88.0
23A	SAME AS ABOVE	10.0	BLACK, SILTY, SANDY GRAVEL (GM)	8.9	82.6	12.5	96.2	86.0
24A	BC-2 DOZER CUT TRENCH IN LEFT ABUTMENT.	22.0	LIGHT GRAY, WELL GRADED, SILTY GRAVEL (GW-GH)	11.1	89.4	7.8	128.5	84.0

* COMPACTIVE ENERGY = 20,000 FT. LB./FT.³.

** SEE FIG. VI-20 FOR TEST LOCATION.

W.A. WAHLER
 & ASSOCIATES

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TABLE A-2
 Sheet 3 of 4

W.A. WAHLER
& ASSOCIATES

TABLE A-2--CONTINUED
SUMMARY
OF
FIELD DENSITY TEST RESULTS

TEST NO.	LOCATION**	DEPTH (ft)	SAMPLE DESCRIPTION	FIELD			LABORATORY*			FIELD DENSITY AS % OF LAB. MAX.
				WATER CONTENT (%)	DRY DENSITY (pcf)	OPTIMUM MOISTURE CONTENT (%)	MAXIMUM DRY DENSITY (pcf)			
25A	BC-7 DOZER TRENCH IN LEFT ABUTMENT	17.0	LIGHT GRAY, WELL GRADED, SILTY GRAVEL (GW-GH)	14.3	107.0	7.8	128.5	84.0		
26A	SAME AS ABOVE	12.0	SAME AS ABOVE	4.0	111.9	7.8	128.5	87.0		
27A	SAME AS ABOVE	7.0	SAME AS ABOVE	7.4	102.1	7.8	128.5	79.0		
28A	SAME AS ABOVE	2.0	LIGHT GRAY, WELL GRADED, SILTY, GRAVELLY SAND (SW-SM)	6.4	93.4	0.2	97.4	86.0		

* COMPACTIVE ENERGY = 20,000 FT.LB./ft³.

** SEE FIG. VI-20 FOR TEST LOCATION.

TABLE A-2
Sheet 4 of 4

TABLE A-3
PENETRATION AND VANE SHEAR TEST RESULTS

(1) LOCATION OF PROBES

LOCATION	PROBE NUMBER
PRE-DRILLED HOLE @ DAM NO. 2; S-4	V-1
UPPER REACH OF POOL NO. 3	P-1, V-1
UPPER REACH OF POOL NO. 3	P-2, V-2
UPPER REACH OF POOL NO. 3	P-3, V-3
UPPER REACH OF POOL NO. 3	P-4, V-4
PRE-DRILLED HOLE @ DAM NO. 3; S-7	P-5, V-5
PRE-DRILLED HOLE @ DAM NO. 3; S-6	P-6, V-6
POOL BEHIND DAM NO. 4	P-1, V-1
POOL BEHIND DAM NO. 4	P-2, V-2
POOL BEHIND DAM NO. 4	P-3, V-3

NOTE: SEE FIGURE VI-20 FOR FIELD LOCATION.

(2) PENETROMETER TEST RESULTS

PROBE NO.	DEPTH		TOTAL RESISTANCE kg/cm ²	PROBE NO.	DEPTH		TOTAL RESISTANCE kg/cm ²
	M	FT.			M	FT.	
DAM NO. 3							
P-1	0.2	0.7	3	P-1	2.3	7.5	0
	1.0	3.3	3		2.3	7.5	12
	1.3	4.3	2		2.8	9.2	17
	1.8	5.9	6		2.9	9.5	68
	2.0	6.6	1		3.4	11.2	8
	2.2	7.2	10		3.5	11.5	30
	2.4	7.9	4		3.6	11.8	16
	2.6	8.5	7		4.6	15.1	25
P-2	3.0	9.8	80	P-2	5.6	18.4	8
	0.2	0.7	1		5.9	19.4	29
	1.0	3.3	4		6.2	20.4	14
	1.1	3.6	1		6.5	21.3	71
P-3	2.3	7.5	3	P-2	0 - 3.5	0 - 11.5	0
	2.4	7.9	70		3.5 - 7.0	11.5 - 23.0	2
P-4	0.2	0.7	4	P-3	0 - 4.5	0 - 14.8	0
	0.7	2.3	5		4.5	14.8	6
	1.3	4.3	2		5.0	16.4	0
	2.0	6.6	2		5.5	18.0	2
	2.3	7.5	4		5.9	19.4	7
	2.4	7.9	50		6.4	21.0	0
	0.3	1.0	0		6.4	21.0	7
	1.2	3.9	5		7.6	25.0	1
	1.6	5.2	3				
	2.5	8.2	6				
	3.0	9.8	3				
	3.1	10.2	90				

TABLE A-3 — CONTINUED
PENETRATION AND VANE SHEAR TEST RESULTS—CONTINUED

(2) PENETROMETER TEST RESULTS—CONTINUED

PROBE NO.	DEPTH		TOTAL RESISTANCE kg/cm ²	PROBE NO.	DEPTH		TOTAL RESISTANCE kg/cm ²
	M	FT.			M	FT.	
DAM NO. 3			DAM NO. 3—CONTINUED				
P-5	10.1	33.1	20	P-6	10.9	35.8	24
	11.5	37.7	31		12.4	40.7	29
	11.6	38.0	18		12.7	41.7	49
	11.7	38.4	43		13.0	42.6	32
	12.1	39.7	39		13.4	44.0	27
	12.2	40.0	18		13.5	44.3	60
	12.4	40.7	19		13.7	45.0	23
	12.5	41.0	46		14.1	46.2	21
	13.3	43.6	23		14.4	47.3	48
	13.4	43.9	50		14.6	47.9	47
	13.6	44.6	36		14.7	48.2	29
	14.2	46.6	35		15.1	49.5	28
	14.3	46.9	20		15.4	50.5	41
	15.4	50.5	47		15.6	51.2	29
	15.5	50.8	20		16.4	53.8	21
	15.9	52.2	19		16.7	54.8	40
	16.0	52.5	52		17.0	55.8	19
	16.2	53.1	45		17.3	56.8	19
	16.3	53.5	20		17.4	57.1	42
	16.5	54.1	19		17.7	58.1	42
	16.9	55.4	55		17.8	58.4	22
	17.1	56.1	32		18.2	59.7	26
	17.2	56.4	53		18.5	60.7	46
	17.9	58.7	22		18.7	61.4	22
	18.1	59.4	45		19.1	62.7	20
	19.0	62.3	22		19.2	63.0	32
	20.0	65.6	41		20.2	66.3	18
	20.5	67.3	26		21.0	68.9	23
	21.8	71.5	50		21.1	69.2	36
	22.0	72.2	25		21.6	70.9	18
	22.2	72.8	20		21.8	71.5	80
	22.3	73.1	45				
	22.7	74.5	75				

(3) VANE SHEAR TEST RESULTS

PROBE NO.	TEST NO.	DEPTH		"A" VALUE IN.	VANE COEF. psf/in.	SHEAR STRENGTH* psf
		M	FT.			
DAM NO. 2						
V-I	S-1	20.0	65.6	2.59	1300	3370
	S-2	21.0	68.9	2.79	1300	3620
	S-3	21.9	71.9	2.98	1300	3870
	(REMOLDED)	21.9	71.9	1.40	1300	1820
	S-4	23.1	75.8	1.75	1300	2270
	S-5	24.0	78.8	1.69	1300	2200
	S-6	24.9	81.7	1.05	1300	1360
	(REMOLDED)	24.9	81.7	0.82	1300	1070

* SHEAR STRENGTH = "A" VALUE × VANE COEFFICIENT. SEE APPENDIX A, SECTION E FOR INTERPRETATION.

W.A. WAHLER
& ASSOCIATES

TABLE A-3 -- CONTINUED
PENETRATION AND VANE SHEAR TEST RESULTS—CONTINUED

(3) VANE SHEAR TEST RESULTS—CONTINUED

PROBE NO.	TEST NO.	DEPTH		"A" VALUE IN.	VANE COEF. PSI/IN.	SHEAR STRENGTH*	
		M	FT.				
DAM NO. 2—CONTINUED							
V-1 CONT.	S-7	26.0	85.3	1.10	1300	1430	
	S-8	27.0	88.6	1.24	1300	1610	
	S-9	28.0	91.9	1.34	1300	1740	
	(REMOLDED)	28.0	91.9	1.08	1300	1400	
		29.0	95.2	1.87	1300	2430	
	S-10	29.0	97.5	3.14	1300	4080	
	S-11	29.7					
DAM NO. 3							
V-1	S-1	1.0	3.3	0.44	1300	570	
	S-2	2.0	6.6	0.73	1300	950	
	S-3	3.0	9.8	3.26	1300	4240	
	(REMOLDED)	3.0	9.8	2.87	1300	3730	
		3.5	11.5	4.03	1300	5250	
	V-2	S-1	1.0	3.3	0.39	1300	510
		S-2	1.9	6.2	0.78	1300	1010
		S-3	2.2	7.2	0.62	1300	810
		(REMOLDED)	2.2	7.2	0.45	1300	590
V-3	S-1	1.0	3.3	0.66	1300	860	
	S-2	2.0	6.6	0.69	1300	900	
	S-3	2.9	9.5	4.25	1300	5520	
	(REMOLDED)	2.9	9.5	4.07	1300	5280	
		S-1	1.0	3.3	0.55	1300	720
	S-2	1.8	5.9	0.81	1300	1050	
	V-4	S-3	2.8	9.2	3.13	1300	4070
		(REMOLDED)	2.8	9.2	2.52	1300	3280
			S-1	36.1	3.65	1300	4750
V-5	S-2	13.2	43.3	1.83	1300	2380	
	S-3	15.0	49.2	2.89	1300	3760	
	(REMOLDED)	15.0	49.2	1.70	1300	2210	
		S-4	16.5	54.1	2.02	1300	2620
		S-5	17.8	58.4	3.5 +	1300	4550+
		S-6	18.1	59.3	3.5 +	1300	4550+
		(REMOLDED)	18.1	59.3	3.5 +	1300	4550+
V-6	S-1	11.2	36.7	3.40	1300	4420	
	S-2	12.5	41.0	1.53	1300	1990	
	S-3	14.9	48.9	3.48	1300	4530	
	(REMOLDED)	14.9	48.9	2.04	1300	2650	

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* SHEAR STRENGTH = "A" VALUE X VANE COEFFICIENT. SEE APPENDIX A., SECTION E FOR
INTERPRETATION.

TABLE A-3—CONTINUED
PENETRATION AND VANE SHEAR TEST RESULTS—CONTINUED

(3) VANE SHEAR TEST RESULTS—CONTINUED

PROBE NO.	TEST NO.	DEPTH		"A" VALUE IN.	VANE COEF. PSI/IN.	SHEAR STRENGTH *
		M	FT.			
DAM NO. 3—CONTINUED						
V-6 CONT.	S-4	16.0	52.5	3.55	1300	4620
	S-5	18.1	59.4	2.42	1300	3150
	S-6	19.3	63.3	3.44	1300	4470
	(REMOLDED)	19.3	63.3	1.65	1300	2150
DAM NO. 4						
V-1	S-1	2.0	6.6	0.21	1300	270
	S-2	2.4	7.9	1.41	1300	1830
	S-2 (REMOLDED)	2.4	7.9	0.25	1300	340
	S-3	1.0	3.3	0.16	650	100
V-2	S-2	2.0	6.6	0.11	650	70
	S-3	4.4	14.4	0.32	650	210
	S-3 (REMOLDED)	4.4	14.4	0.19	650	120
	S-4	6.1	20.0	0.61	650	400
V-3	S-5	7.5	24.6	3.93	650	2560
	S-1	2.0	6.6	0.10	1300	130
	S-2	4.2	13.8	0.25	1300	325
	S-3 (REMOLDED)	6.0	19.7	0.60	1300	1040
	S-4	6.9	22.6	2.48	1300	3220

* SHEAR STRENGTH = "A" VALUE \times VANE COEFFICIENT. SEE APPENDIX A, SECTION E FOR INTERPRETATION.

DRILL RIG CME MODEL 65 HOLE ELEVATION 1763.6 LOGGED BY RPT
GROUNDWATER DEPTH DATE DRILLED 4/16 - 12/72
TABLES STAND SURFACE.

DRILL RIG CME MODEL 65	HOLE ELEVATION 1763.6	LOGGED BY RPT	HOLE ELEVATION 1763.6	LOGGED BY RPT
GROUNDWATER DEPTH	DATE DRILLED 4/16 - 12/72	HOLE DIAMETER 6 inches max.	HOLE DIAMETER 6 inches max.	DATE DRILLED 4/6 - 12/72
TABLES STAND SURFACE.				
EL. (depth)	DESCRIPTION	SAMPLE NUMBER	FOOT	REMARKS
EL. (depth)	FIELD IDENTIFICATION			
4/6/72 GP-SP	EMBANKMENT FILL.	D-1	3/5/5	1-10
	About 30% gravel, 60% sand, and 10% fines, with local concentrations of sand and/or gravel. Dark gray to black.	D-2	5/11/1	N=26
(5)	Gravel is largely carbonaceous.	B-3	19/23/22	N=65
4/7/72	Gravel is largely carbonaceous; siltstone and impure coal, with minor shale and slate. Gravel sizes tend to be angular and blocky, sand size material is flaky. Damp near the surface becoming dry to slightly damp at 15 feet and below. Minor pyrite present in some of the shale and coal fragments.	B-4	16/13/13	N=26
(10)		AH		
4/10/72		S-1	P	Recovery 2.0/2.0
4/11/72		P-1	P	Recovery 0.5/2.0
	Sample extended from tube on site			
(15)		-	AH	-
		S-2	P	Recovery 1.8/2.0
		D-5	O	2/8/7 N=15
		S+J	P	Recovery 1.5/2.0
(20)		D-6	5 1/4/2	N=6
		D-7	D	4 1/5/4 N=9
		S-4	P	Recovery 2.0/2.0
(25)		D-8	D	13/13/10 N=25
		D-9	D	6/6/6 N=8
(30)		S-5	P	Recovery 1.9/2.0
		D+10	D	4/4/7 N=11
		D-11	D	6/1/5 N=12
		S+6	P	Recovery 2.0/2.0
(35)		D-12	D	5/6/5 N=11
		D-13	D	4/7/5 N=12
4/12/72	-	S-7	P	Recovery 2.0/2.0
(40)	SOIL			
	Silty sand, yellow-brown, moist, firm, scattered gravel and silt concentrations.	-	D	3/5/8 N=13
		D-15	D	10/5/5 N=10
(45)	BEDROCK - NANAHDA SERIES	S-6	P	Recovery 0.5/0.5
	SANDSTONE (6.3.5-6.2)	-	NK	Recovery 0.7/2.5
	TABA-BEDROCK, hard, strong /	Box 1	Core	Run 46.0-51.0
	MUDSTONE (6.6.2-51.0)		Barrel	Recovery 2.6/5.0
	Tan, weak, severely fractured.			
(50)	COAL REFUSE DAY FAILURE	DRILL HOLE LOG	HOLE NO	SOIL EXPLORATION
	Saunders, W. Va.	FEET	SPACES	DRILL HOLE LOG
	PROBING • REPROBING	ft	ft	PROJECT NO.
		0700	0700	0700
		APRIL 1972	APRIL 1972	APRIL 1972
				2 ft 2
	WA WHITIR & ASSOCIATES	COM. REFUSE DAY FAILURE	WA WHITIR & ASSOCIATES	HOLE NO.
		SAUNDERS, W. Va.	PROBING • REPROBING	S-2

ELEVATION (feet)	CLASS.	DESCRIPTION FIELD IDENTIFICATION	SAMPLE NUMBER	REMARKS	NET DEPTH	LOGGED BY	DATE DRILLED	HOLE ELEVATION 1162.5	HOLE DIAMETER 6 inches max.	LOGGED BY	RBT
4/13/72		EMBANKMENT FILL	D-1		5/13/14 N=27						
		Mixture of about 30% gravel and minor oversize (over 3 inches maximum dimension), 60% sand, and up to 10% (fine) sand and gravel are locally each concentrated above the percentages given above.	D-2	D	11/11/11 N=22						
(5)		Gravel is largely carbonaceous siltstone, impure coal, and shilite, with minor slate and sandstone. Gravel and oversize are blocky and slabby; subangular. Sand is generally flaky. Damp near the surface, dry to slightly damp at 5-62 feet, wet to moist at 42-46. Dark gray to black.	S-1	P	Recovery 1.2/1.3 (Note 1)	All					
(10)			D-3	D	3/2/3 N=5						
			D-4	D	4/5/3 N=8						
(15)			S-2	P	Recovery 1.3/1.3	All					
(20)			S-3	P	Recovery 1.5/2.0						
			D-5	D	4/4/2 N=6						
			D-6	D	2/2/3 N=5						
			S-4	P	Recovery 2.0/2.0						
			D-7	D	2/1/2 N=5						
			D-8	D	2/2/3 N=5						
			S-5	P	Recovery 1.8/2.0						
(25)			D-9	D	7/6/5 N=11						
4/13/72			D-10	D	4/3/3 N=6						
			S-6	P	Recovery 2.0/2.0						
(30)			D-11	D	14/13/6 N=9						
			D-12	D	6/6/11 N=17						
			S-7	P	Recovery 1.6/2.0						
			D-13	D	7/5/5 N=10						
			D-14	D	4/5/3 N=8						
			S-8	P	Recovery 1.0/2.0 (Note 1)						
			D-15	D	4/1/6 N=11						
			D-16	D	5/6/6 N=10						
(35)			S-9	P	Recovery 2.0/2.0						
			D-17	D	6/6/13 N=7						
			D-18	D	5/4/7 N=11						
			S-10	P	Recovery 0.2/0.7 (Note 1)						
(40)			D-19	D	4/6/6 N=8						
			S-11	P	Recovery 1.0/3.0						
			BEDROCK - KAMAHIA SERIES SEDIMENTARY (48.0-52.2) Tall, arched, c., due to	Core - Box 1	Run 48.0-51.0 Recovery 1.0/3.0	All					
(50)			WA WAHIA COAL, REFUSE, DAM FAILURE Saunders, W. Va.	SOIL EXPLORATION 0 FT. TO HOLE 1 or 2	WA WAHIA SOIL EXPLORATION 0 FT. TO HOLE 1 or 2						
			WA ASSOCIATES PROPS - SUPPORTS - 1111 0700 APRIL 1972	SOIL EXPLORATION 0 FT. TO HOLE 1 or 2	WA ASSOCIATES PROPS - SUPPORTS - 1111 0700 APRIL 1972						

ELEVATION (feet)	CLASS.	DESCRIPTION FIELD IDENTIFICATION	SAMPLE NUMBER	REMARKS	NET DEPTH	LOGGED BY	DATE DRILLED	HOLE ELEVATION 1162.5	HOLE DIAMETER 6 inches max.	LOGGED BY	RBT
4/13/72		GROUNDWATER, 0 FT. NOT ENCOUNTERED GALLERIES, 10 FT. DEEP	D-1		5/13/14 N=27						
			D-2	D	11/11/11 N=22						
(5)			S-1	P	Recovery 1.2/1.3 (Note 1)	All					
			D-3	D	3/2/3 N=5						
			D-4	D	4/5/3 N=8						
(10)			S-2	P	Recovery 1.3/1.3	All					
			S-3	P	Recovery 1.5/2.0						
			D-5	D	4/4/2 N=6						
			D-6	D	2/2/3 N=5						
			S-4	P	Recovery 2.0/2.0						
			D-7	D	2/1/2 N=5						
			D-8	D	2/2/3 N=5						
			S-5	P	Recovery 1.8/2.0						
(25)			D-9	D	7/6/5 N=11						
4/13/72			D-10	D	4/3/3 N=6						
			S-6	P	Recovery 2.0/2.0						
			D-11	D	14/13/6 N=9						
			D-12	D	6/6/11 N=17						
			S-7	P	Recovery 1.6/2.0						
			D-13	D	7/5/5 N=10						
			D-14	D	4/5/3 N=8						
			S-8	P	Recovery 1.0/2.0 (Note 1)						
			D-15	D	4/1/6 N=11						
			D-16	D	5/6/6 N=10						
(35)			S-9	P	Recovery 2.0/2.0						
			D-17	D	6/6/13 N=7						
			D-18	D	5/4/7 N=11						
			S-10	P	Recovery 0.2/0.7 (Note 1)						
(40)			D-19	D	4/6/6 N=8						
			S-11	P	Recovery 1.0/3.0						
(50)			BEDROCK - KAMAHIA SERIES SEDIMENTARY (48.0-52.2) Tall, arched, c., due to	Core - Box 1	Run 48.0-51.0 Recovery 1.0/3.0	All					

HOLE S-3 WATER PRESSURE TESTS

Test #1

I. Data Compilation

A. Interval 65.0-66.0
Gravity Head: 70 feet

PSIG = 25

<u>Minute No.</u>	Gallons <u>Taken</u>	Cumulative <u>Gallons</u>
1	0.5	0.5
2	0.7	1.2
3	0.7	1.9
4	0.7	2.6
5	0.5	3.1
6	0.6	3.7
7	0.5	4.2
8	0.6	4.8
9	0.6	5.4
10	0.5	5.9

PSIG = 100, other data same as above

<u>Minute No.</u>	Gallons <u>Taken</u>	Cumulative <u>Gallons</u>
1	2.6	2.6
2	2.6	5.2
3	2.4	7.6
4	2.5	10.1
5	2.5	12.6
6	2.4	15.0
7	2.4	17.4
8	2.3	19.7
9	2.4	22.1
10	2.3	22.4

Test #2

B. Interval 60.0-65.0
Gravity Head: 72.5 feet

PSIG 25

<u>Minute No.</u>	Gallons <u>Taken</u>	Cumulative <u>Gallons</u>
1	5.9	5.9
2	6.0	11.9
3	5.6	17.5
4	5.6	23.1
5	5.7	28.8
6	5.5	34.3
7	6.6	40.9
8	5.4	46.3
9	5.5	51.8
10	5.3	57.1
11	5.4	62.5
12	5.3	67.8

Interval 65.0-66.0
Gravity Head: 70 feet
PSIG = 50

<u>Minute No.</u>	Gallons <u>Taken</u>	Cumulative <u>Gallons</u>
1	0.7	0.7
2	0.7	1.4
3	0.9	2.3
4	0.7	3.0
5	0.7	3.7
6	0.9	4.6
7	0.6	5.2
8	0.7	5.9
9	0.8	6.7
10	0.7	7.4

PSIG = 25, other data same as above

<u>Minute No.</u>	Gallons <u>Taken</u>	Cumulative <u>Gallons</u>
1	0.4	0.4
2	0.4	0.8
3	0.6	1.4
4	0.6	2.0
5	0.7	2.7
6	0.6	3.3
7	0.7	4.0
8	0.6	4.6
9	0.6	5.2
10	0.6	5.8

Test #2 Continued: PSIG = 50, Gravity Head: 72.5 feet, Interval 60.0-65.0 Attempted test at 50 PSIG but packer would not hold - or injected water travelled from the test interval through fractures to enter the drill hole above the top packer. Test terminated, packers reset for Test #3.

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0700

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HOLE S-3, WATER PRESSURE TESTS--Continued

Test #3

C. Interval 60.0-66.0
Gravity Head: 73 feet

PSIG = 25

Minute No.	Gallons Taken	Cumulative Gallons
1	8.8	8.8
2	8.0	16.8
3	9.5	26.3
4	8.5	34.8
5	8.6	43.4
6	8.6	52.0
7	8.5	60.5
8	8.4	68.9
9	8.3	77.2
10	8.4	85.6

Interval = 60.0-66.0
Gravity Head = 73 feet
PSIG 50

Minute No.	Gallons Taken	Cumulative Gallons
1	10.3	10.3
2	10.7	21.0
3	10.1	31.1
4	10.5	41.6
5	10.3	51.9
6	10.6	62.5
7	10.5	73.0
8	10.6	83.6
9	10.8	94.4
10	10.6	105.0

PSIG = 75, other data same as above

Minute No.	Gallons Taken	Cumulative Gallons
1	13.3	13.3
2	13.6	26.9
3	13.7	40.6
4	13.7	54.3
5	13.5	67.8
6	14.0	81.8
7	13.9	95.7
8	14.0	109.7
9	13.0	122.7
10	13.6	136.3

Interval 60.0-66.0
Gravity Head: 73 feet
PSIG = 25

Minute No.	Gallons Taken	Cumulative Gallons
1	6.5	6.5
2	6.3	12.8
3	5.6	18.4
4	6.3	24.7
5	6.5	31.2
6	6.4	37.6
7	6.5	44.1
8	6.4	50.5
9	6.5	57.0
10	6.4	63.4

Note: 75 PSIG = Max. pressure
obtainable with this pump for
the interval.

Test #4

Interval 54.0-59.0

Attempted test, but packer would not hold.
Since there were no other potentially testable
intervals in the hole, the water pressure
test program for hole 3 was terminated.

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& ASSOCIATES

0700

NOVEMBER 1972

DRAIL RIG LINE NUMBER 55		HOLE ELEVATION 1692		LOGGED BY R.E. & N.P.	
GROUNDRIG OPEN CHARGE STATION NO. 4511		HOLE DIAMETER 6 inches		DATE DRILLED 5/19 - 5/5/12	
ELEVATION (depth)	CLASS	DESCRIPTION	FIELD IDENTIFICATION	SAMPLE NUMBER	TEST
4/19/72	GP	ROAD SURFACING (RED DICE)	D-1	1/8/20/12	N=12
	SP.	ENBANKMENT FILL	D-2	9/8/9	N=17
(5)	Mixed gravel and sand with minor fines. Overall about 30% gravel, 60% sand, 5% over-size.	D-3	10/4/5	N=9	
	5% fines. Local concentration of sand or gravel exist. Material is largely coal processing refuse and the gravel & over-size fragments are largely carbonaceous slate, shale, and minor coal. Sand and fines are angular and blocky; sand is flaky. Dark gray to black, consistency given by blow counts.	Air			
(10)		Largely coal. Gravel and over-size fragments are generally angular and blocky; sand is	S-1	P	Recovery 2, 0/2, 0
		6/6	D	7/6/5	N=11
(15)		6/7	D	7/5/5	N=10
		6/7/4			
(20)		5-3	P	P	Recovery 2, 0/2, 0
		6/8	D	6/7/5	N=12
		6/9	D	6/7/4	N=11
		6/10	D	6/3/3	N=6
(25)		6/11	D	3/2/6	N=8
		6/12	D	3/2/5	N=11
		6/13	D	3/2/4	N=11
		6/14	D	3/2/3	N=8
		6/15	D	3/2/2	N=10
		6/16	D	3/2/1	N=12
		6/17	D	3/2/0	N=12
		6/18	D	3/2/1	N=12
		6/19	D	3/2/0	N=12
		6/20	D	3/2/1	N=12
		6/21	D	3/2/0	N=12
(35)		6/22	D	3/2/1	N=12
		6/23	D	3/2/0	N=12
		6/24	D	3/2/1	N=12
		6/25	D	3/2/0	N=12
		6/26	D	3/2/1	N=12
		6/27	D	3/2/0	N=12
		6/28	D	3/2/1	N=12
		6/29	D	3/2/0	N=12
		6/30	D	3/2/1	N=12
(40)		7/1	D	5/7/8	N=15
		7/2	D	8/6/6	N=8
		7/3	D	8/6/5	N=8
		7/4	D	8/6/4	N=8
		7/5	D	8/6/3	N=8
		7/6	D	8/6/2	N=8
		7/7	D	8/6/1	N=8
		7/8	D	8/6/0	N=8
		7/9	D	8/6/1	N=8
		7/10	D	8/6/0	N=8
		7/11	D	8/6/1	N=8
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		7/26	D	8/6/0	N=8
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		7/5	D	8/6/0	N=8
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		7/17	D	8/6/0	N=8
		7/18	D	8/6/1	N=8
		7/19	D	8/6/0	N=8
		7/20	D	8/6/1	N=8
		7/21	D	8/6/0	N=8
		7/22	D		

DRILL RIG CME. MODEL 45	GROUNDWATER DEPTH (feet below surface) 140.0	HOLE ELEVATION 1692	LOGGED BY R.E.T.
		HOLE DIAMETER 6 inches	DATE DRILLED 4/19 - 5/5/72
ELEVATION (depth)	CLASS, FIELD IDENTIFICATION	SAMPLE NUMBER	NOTES
(100)	M.L. SILT, gray, laminated, moist, soil to firm, changing to pale yellow-brown sandy silt @ 107.5. Wood fragments @ 108.0.	S-17 D-35 D-36 S-18 D-17 D-18	Recovery 1.0/2.0 N=13 Recovery 0.0/2.0 N=16 Recovery 0.0/2.0 N=19
5/4/72 5/5/72	SH SOIL, yellow-brown silty sand,	PST-6 D-19	Recovery 1.3/1.5 (Note 5), N=11
(115)	BEDROCK - KANAMHA SERIES Sandstone, arkosic, uni, fine to medium grained, hard, strong. Bedding nearly hori- zontal, locally cross bedded. Very closely fractured.	-	All
(120)		B-60	D 22.6/52 N=97
(125)		Core Box 1 Barrel	No Run 116.5/119.5 Recovery 1.0/3.0 Run 119.5-126.0 Recovery 1.2/6.5
(130)	HOLE TERMINATED @ 126.0 FEET NOTES: 1. SAMPLE REMOVED FROM SAMPLE TUBE FOR ON SITE EXAMINATION; NOT SAVED.		
	2. THE SERIES S-16, S-15, POORLY DRILLED AS POLLARS; S-14 WAS PUSHED 9.0-92.0 WITH NO RECOVERY. S-15 FOUND THE HOLE BOTTOM AT 91.0 AND WAS AS AN EXPERIMENT DRIVEN WITH THE 160-lb. HARPER DRILL TO 93.0 WITH NO RECOVERY. POORLY (A DISCARDED 15-ft. SS INNER MASTIC) WAS PUSHED FROM 91.0 TO 95.0 WITH RECOVERY OF 3.7 FEET.		
	3. PST-6 REFUSED AT 110.5.		
		SPIN EXPLORATION LOG	HOLE NO. S-4
	COAL REFUSE DAM FAILURE Saunders, W. Va.	DRILL LOG RECOVERIES 0700 AM APRIL 1972 J or J	
	W.A. WALTER & ASSOCIATES P.O. BOX 1111 • MURFREESBORO • TN 37130		

DRILL RIG	CME-45	HOLE ELEVATION	1690	LOGGED BY	REF	DATE DRILLED	6/25-27/72
GROUNDWATER DEPTH	See Notes Water level 3 ft.	HOLE DIAMETER	6 inches	HOLE NUMBER		HOLE ELEVATION	1690
ELEVATION (feet)	CLASS. Gr- SP	DESCRIPTION FIELD IDENTIFICATION	SAMPLE NUMBER	HOLE	REMARKS		
(0)	GR- SP	EMBANKMENT FILL.					
(5)	SP	Coal processing refuse; sun- dry gravel and gravelly sand. Of the gravel-sized clasts, about 60% are siltstone, 35% carbon- aceous shale, and the remainder coal and sandstone. Gravel clasts tend to be blocky or subangular; and angular, and poorly graded (v. fine to medium grained). Dry to slightly damp @ 0-25 ft. Consistency given by blow counts.	-	AH	Hard auger borng. Wood @ 23 ft.		
(10)	D-1	D	6/5/77	N=12			
(15)	D-2	D	7/8/77	N=5	AH	Hard auger borng.	
(20)	D-2	D	7/8/77	N=5	AH	Hard auger borng. Wood @ 23 ft.	
(25)	D-1	D	7/4/77	N=9	AH		
(30)	D-1	D	7/4/77	N=9	AH		
(35)	D-1	D	7/4/77	N=9	AH		
(40)						Measured water level 3 ft. ft. depth when auger bit was at 50 ft. depth.	
(45)							
(50)							

DRILL RIG	CME-45	HOLE ELEVATION	1690	LOGGED BY	REF	DATE DRILLED	6/25-27/72
GROUNDWATER DEPTH	See Notes Water level 3 ft.	HOLE DIAMETER	6 inches	HOLE NUMBER		HOLE ELEVATION	1690
ELEVATION (feet)	CLASS.	DESCRIPTION	SAMPLE NUMBER	HOLE	REMARKS		
(50)	GP SP	EMBANKMENT FILL. (Cont'd.)					
(55)	-	RESERVOIR SEDIMENTS.	-				
(60)	SP-SM	Sediments from pool #1. Sand fine to medium-grained, black, with silty sand. Minor thin layers of silt and clay below about 70 ft. depth. Moist to saturated. Consistency given by blow counts.	-		All		
(65)	-	Composition largely coal with some siltstone and carbon- aceous shale.	S-5	P	Recovery 2.0/2.0		
(70)	-		S-6	P	Recovery 2.0/2.0		
(75)	-		S-7	P	Recovery 2.0/2.0		
(80)	-		S-B	P	Recovery 1.9/2.0		
(85)	-		D-6	D	0/2/4 N=6		
(90)	-		S-9	P	Recovery 2.0/2.0		
(95)	-		-				
(100)	-		D-7	D	4/7/14 N=21		

COAL REFUSE DAY FAILURE	WA. WALTER SAUNDERS, W. Va.	WA. WALTER & ASSOCIATES	COAL REFUSE DAY FAILURE	WA. WALTER SAUNDERS, W. Va.	WA. WALTER & ASSOCIATES	COAL REFUSE DAY FAILURE	WA. WALTER SAUNDERS, W. Va.	WA. WALTER & ASSOCIATES
FIELD NO. • REPORT DATE • FILE	PROJECT NO. • REPORT DATE • FILE	FIELD NO. • REPORT DATE • FILE	FIELD NO. • REPORT DATE • FILE	PROJECT NO. • REPORT DATE • FILE	FIELD NO. • REPORT DATE • FILE	FIELD NO. • REPORT DATE • FILE	PROJECT NO. • REPORT DATE • FILE	FIELD NO. • REPORT DATE • FILE

DRILL HIG		WELL NO.	HOLE ELEVATION	LOGGED BY	LOGGED BY	RENT.
GROUNDWATER DEPTH		HOLE DIAMETER	6 INCHES	DATE DRILLED	6/25-22/77	
SANDERSON, SAUNDERS & ASSOCIATES						
ELEVATION feet	CLASS.	DESCRIPTION	SAMPLE NUMBER	WEIGHT	REMARKS	
(100)	SM	ALLUVIUM (Continued)	D-8	0	70/0.5 ft. N.W. Intre	
		BEDROCK - KANANHA SERIES			Run 100.5 - 106.8	
		LOG 5-111-8 Arkosic sandstone little fractured, hard, generally fresh. tan where weathered (near top and along fractures) very fine to fine grained, very thinly bedded, locally cross-bedded, bedding dips about 1-4°. Fractures dip 80°.			Core Recovery 6.3/6.3 barrel	
					Run 106.8-111.8 Recovery 4.7/5.0	
(105)						
(110)						
(115)		HOLE TERMINATED @ 111.8 FEET.				
		NOTES:				
		1. Sample extruded from tube for on-site examination. 2. Water level @ 32.8 ft. depth 15 minutes after coring operations stopped.				
		COAL REFUSE DAM FAILURE	SOIL TESTER ON	DRILL HOLE LOG	HOLE NO.	
		Saunders, W. Vn.	RECEIVED	DATE	INTER. NO.	
		WA. WEAVER	0700	JUNE 1972	3	3
		& ASSOCIATES				

DRILL RIG ONE - 45 GROUNDRIG DEPTH CEILED ABOVE SURFACE				HOLE ELEVATION 1706 HOLE DIAMETER 6 inches				LOGGED BY RET DATE DRILLED 5/8 - 10/72				HOLE ELEVATION 1706 HOLE DIAMETER 6 inches				LOGGED BY RET DATE DRILLED 5/8 - 10/72			
ELEVATION (feet)	CLS.	DESCRIPTION FIELD IDENTIFICATION	SAMPLE NUMBER	HOE	REMARKS	ELEVATION (feet)	CLASS.	DESCRIPTION FIELD IDENTIFICATION	SAMPLE NUMBER	HOE	REMARKS	ELEVATION (feet)	CLS.	DESCRIPTION FIELD IDENTIFICATION	SAMPLE NUMBER	HOE	REMARKS		
(0)		ENRICHMENT FILT.	B-1		17/74 N= 7	5/10/72		BEDROCK (cont.)	-			5/10/72			-				
5/8/72		General processes refuse of variable size range and composition, hummocky fill. Estimated overall size distribution: 10% fines, 20% gravel and +10% sand.	B-2	D	5/3/2 N= 5												RESULTS OF WATER PRESSURE TESTS ON FOLLOWING SHEETS.		
(5)			B-3		3/6/3 N= 7														
5/9/72		Minor carbonaceous shale. Gravel and overlying largely carbonaceous shale and silt- stone. Dark gray to black. Damp to moist @ 0-15 ft., moist to saturated @ 15-17.5 ft. Consistency given by hole counts.	B-4	D	1/5/4 N= 9														
(10)																			
(15)			B-5	D	3/7/2 N= 6														
(20)			B-6	D	4/2/1 N= 3														
(25)			B-7	D	1/2/3 N= 5														
(30)		Note: a small interval of Reservoir sediments is prob- ably located between 31.5 and 35.0 ft., based on a projec- tion from hole S-7. (See note 1 for explanation of this symbol)																	
(35)	SN	SOLID Vol. -burn shiny sand, moist.	B-8	D	4/2/2 N= 4														
5/9/72		BEDROCK - KANAWHA SHIRES	B-9	D	4/11/23 N= 24														
		Sandstone, arkosic, pale gray, locally iron-stained. Medium grained, well indur- ated. Moderately hard and strong, fresh. Fracture space- ding 0.2 to 4.0 ft. Fractures dip 5°-15°, parallel to bed- ding planes. Composition about 75% quartz, 2% feld- spar, 2% mica, dark minerals, and coal.	CORE - BOX 1	NX	Set 4" casting to core 38.0 feet. Run 38.0-41.5 Recovery 3.5/3.5														
(40)																			
(45)																			
(50)																			
	WA WALTER & ASSOCIATES	COAL REFUSE DAM FAILURE Saunders, W. Va.	DRILL HOLE LOG	HOLE NO. 5-6	SPUD DATE 0700	SETTER NO. 1 or 2	PROJECT NO. 0700	DRILL HOLE LOG	HOLE NO. S-6	SPUD DATE MAY 1972	SETTER NO. 2 or 2	PROJECT NO. 0700	DRILL HOLE LOG	HOLE NO. S-6	SPUD DATE MAY 1972	SETTER NO. 2 or 2			

HOLE S-6 WATER PRESSURE TESTS

5/10/72

Series I

Interval 49.0-51.5 Gravity Head 55.75 Ft.

<u>Ia</u> Minute	<u>PSIG 25</u> Gals.	Cum.	<u>Ib</u> Minute	<u>PSIG 50</u> Gals.	Cum.
No.	Taken	Total	No.	Taken	Total
1	0.15	0.15	1	0.45	0.45
2	0.15	0.30	2	0.35	0.80
3	0.10	0.40	3	0.40	1.20
4	0.12	0.52	4	0.55	1.75
5	0.06	0.58	5	0.30	2.05
6	0.04	0.62	6	0.40	2.45
7	0.05	0.67	7	0.01*	2.46
8	0.03	0.70	8	0.34	2.80
9	-	-	9	0.45	3.25
10	-	-	10	0.20	3.45

Note: guage pressure fluctuated
@ 25-30

* Guage pressure gradually built
to 60 psi; was cut back to 50 psi
at beginning of minute no. 7.

<u>Ic</u> Minute	<u>PSIG 100</u> Gals.	Cum.	<u>Id</u> Minute	<u>PSIG 25</u> Gals.	Cum.
No.	Taken	Total	No.	Taken	Total
1	10	10	1	0.6	0.6
2	9	19	2	0.7	1.3
3	11	30	3	0.7	2.0
4	10	40	4	0.7	2.7
5	10.5	50.5	5	0.6	3.3

Holding Test

Pressure, psig	Time, sec.
100	0
50	5
25	30
10	70
5	150
0	210

W.A. WAHLER
& ASSOCIATES

0700

NOVEMBER 1972

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HOLE S-6, WATER PRESSURE TESTS—Continued

Series II

Interval 41.0-49.0 Gravity Head 50.0 Ft.

<u>IIIa</u> PSIG 25			<u>IIIb</u> PSIG 50		
Minute	Gals.	Cum.	Minute	Gals.	Cum.
No.	Taken	Total	No.	Taken	Total
1	0.0	0	1	0.5	0.5
2	0.0	0	2	0.0	0.5
3	0.0	0	3	0.0	0.5
4	0.0	0	4	0.0	0.5
5	0.0	0	5	0.0	0.5

<u>IIIc</u> PSIG 100			<u>IIId</u> PSIG 25		
Minute	Gals.	Cum.	Minute	Gals.	Cum.
No.	Taken	Total	No.	Taken	Total
1	0.0	0	1	0.0	0
2	0.0	0	2	0.0	0
3	0.0	0	3	0.0	0
4	0.0	0	4	0.0	0
5	0.0	0	5	0.0	0

Holding Test

Pressure, PSIG	Time, Minutes
110	0
100	1/4
95	1
85	2
82	3
77	4
75	5 end test.

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& ASSOCIATES

0700

NOVEMBER 1972

DRILL RIG	CME = 45	HOLE ELEVATION	1702	LOGGED BY	KET	DRILL RIG	CME = 45	HOLE ELEVATION	1702	LOGGED BY	KET
GROUNDWATER DEPTH (LITER STATION, FEET)		HOLE DIAMETER	6 inches	DATE DRILLED	5/12 - 16/72	GROUNDWATER DEPTH (LITER STATION, FEET)		HOLE DIAMETER	6 inches	DATE DRILLED	5/12 - 16/72
(0)	SP, ENRICHMENT SEDIMENT	DESCRIPTION	SAMPLE NUMBER	WEIGHT	REMARKS	(depth)	ELEVATION (depth)	CORE CLASS.	FIELD IDENTIFICATION	RESERVOIR SEDIMENT(S)	NOTES
5/12/72	SP, ENRICHMENT SEDIMENT	Bumped coal processing refuse, about 30% gravel and +3-inch material, and 70% sand, with minor fines.	-	AH	-	5/12/72 5/15/72	SP, SN, CL.. (55)	SP, SN, CL.. (55)	RECOVERY 1.3/2.0	-	P
(5)	Gravel and oyster shell, siltstone carbonaceous shale, siltstone and clay shale. Sand and silt, remainder largely carbonaceous shale. Dark gray to black.	D-1	1/5in.	N = 9	-	-	-	-	All sand below 35 feet.	-	AN
(10)	Hoist at 0-10, saturated below 10 feet. Consistency given by blow counts.	-	-	AH	-	(60)	-	-	P	RECOVERY 1.0/1.3	P
(15)	Top 2-5 feet may be re-worked by flooding after failure of the dam.	D-2	D	2/2/2	N = 4	(65)	-	-	-	RECOVERY 0.0/2.0	-
(20)	-	-	AH	-	-	(70)	-	-	-	Sand flowing into auger	-
(25)	-	AH	-	-	-	(75)	-	-	-	-	AH
(30)	See Note 1 for explanation of symbol.	D-J	D	5/6/11	N=17	(80)	-	-	SOIL AND (OR) STREAM CHANNEL ALLUVIUM	RECOVERY 1.7/2.0	P
(35)	RESERVOIR SEDIMENT(S)	-	AH	-	-	(85)	-	-	Gravelly-clayey sand, yellow brown, moist, dense.	-	AN
(40)	Sand, fine to medium grained, angular, clayey. Hostly coal and carbonaceous shale, minor clay shale. Black, saturated to locally very moist.	S-3	P	Recovery 2.0/2.0	-	(90)	-	-	DEELOCK-KAMMIA SERIES	Run 85.0-91.0	AN
(45)	Scattered silt and clay (?) untilts a few inches thick are present but sparse.	D-4	D	1/1/2	N = 3	(95)	-	-	85.0-97.3 Sandstone, l.m., medium to coarse grained, hard, strong, closely fractured, fractures follow bedding, which dips 5° to 10°, locally cross-bedded, locally porous.	core box 1 barrel	core rods
(50)	Silt & clay in D-5 recovery	D-5	D	0/1/2	N = 3	(100)	-	-	Composition 90% + quartz, minor feldspar, dark minerals and mica.	Run 91.0-97.0, Recovery 1.9/6.0	AN
WA WAIHUA & ASSOCIATES	COAL REFUSE DAM FAILURE Saunders, W. Va.	SKILL EXPLORATION Drill Hole Log	HOLE NO S-7	Drill Date 07/00	SAFETY Date JAN 1972	SAFETY Date 07/00	SOIL EXPLORATION Drill Date 07/00	Drill Date JAN 1972	SOIL EXPLORATION Drill Date 07/00	HOLE NO S-7	

DRILL RIG	CME = 45	HOLE ELEVATION	1702	LOGGED BY	KET	DRILL RIG	CME = 45	HOLE ELEVATION	1702	LOGGED BY	KET
GROUNDWATER DEPTH (LITER STATION, FEET)		HOLE DIAMETER	6 inches	DATE DRILLED	5/12 - 16/72	GROUNDWATER DEPTH (LITER STATION, FEET)		HOLE DIAMETER	6 inches	DATE DRILLED	5/12 - 16/72
(0)	SP, ENRICHMENT SEDIMENT	DESCRIPTION	SAMPLE NUMBER	WEIGHT	REMARKS	(depth)	ELEVATION (depth)	CORE CLASS.	FIELD IDENTIFICATION	RESERVOIR SEDIMENT(S)	NOTES
5/12/72	SP, ENRICHMENT SEDIMENT	Bumped coal processing refuse, about 30% gravel and +3-inch material, and 70% sand, with minor fines.	-	AH	-	5/12/72 5/15/72	SP, SN, CL.. (55)	SP, SN, CL.. (55)	RECOVERY 1.3/2.0	-	P
(5)	Gravel and oyster shell, siltstone carbonaceous shale, siltstone and clay shale. Sand and silt, remainder largely carbonaceous shale. Dark gray to black.	D-1	1/5in.	N = 9	-	(60)	-	-	-	RECOVERY 1.0/1.3	P
(10)	Hoist at 0-10, saturated below 10 feet. Consistency given by blow counts.	-	-	AH	-	(65)	-	-	-	RECOVERY 1.0/1.3	P
(15)	Top 2-5 feet may be re-worked by flooding after failure of the dam.	D-2	D	2/2/2	N = 4	(70)	-	-	-	RECOVERY 1.0/1.3	P
(20)	-	AH	-	-	-	(75)	-	-	-	RECOVERY 1.0/1.3	P
(25)	-	AH	-	-	-	(80)	-	-	-	RECOVERY 1.0/1.3	P
(30)	See Note 1 for explanation of symbol.	D-J	D	5/6/11	N=17	(85)	-	-	-	RECOVERY 1.0/1.3	P
(35)	RESERVOIR SEDIMENT(S)	-	AH	-	-	(90)	-	-	-	RECOVERY 1.0/1.3	P
(40)	Sand, fine to medium grained, angular, clayey. Hostly coal and carbonaceous shale, minor clay shale. Black, saturated to locally very moist.	S-3	P	Recovery 2.0/2.0	-	(95)	-	-	-	RECOVERY 1.0/1.3	P
(45)	Scattered silt and clay (?) untilts a few inches thick are present but sparse.	D-4	D	1/1/2	N = 3	(100)	-	-	-	RECOVERY 1.0/1.3	P
(50)	Silt & clay in D-5 recovery	D-5	D	0/1/2	N = 3	(105)	-	-	-	RECOVERY 1.0/1.3	P
WA WAIHUA & ASSOCIATES	COAL REFUSE DAM FAILURE Saunders, W. Va.	SKILL EXPLORATION Drill Hole Log	HOLE NO S-7	Drill Date 07/00	SAFETY Date JAN 1972	SAFETY Date 07/00	SOIL EXPLORATION Drill Date 07/00	Drill Date JAN 1972	SOIL EXPLORATION Drill Date 07/00	HOLE NO S-7	

DRILL RIG CME -45
CROWNTOP DEPTH
CALOR
SAND & SHALE

HOLE DIAMETER 6 inches

LOGGED BY RET

DATE DRILLED 5/12 - 16/72

CLASS.	FIELD IDENTIFICATION	SAMPLE NUMBER	NOTE	REMARKS
(105)	(CONT.) thin-bedded, locally cross-bedded, moderately hard and stony.	CORE - Box 1	Nx	See previous page for run recovery information.
(105)	102.0-106.0 Siltstone, locally sandy and clayey, faint, weak bedding horizon.			

HOLE TERMINATED @ 106.0 FEET.

Notes:

1. The horizontal dashed line indicates the estimated elevation/depth of the contact between the two units it separates. The inclined dashed lines show the possible range in elevation/depth of the contact.
2. USG-2 refused at 70.5 on large piece of gravel. Washed hole to 71.1 to clean sand from augers.

COAL REFUSE DAM FAILURE	SOIL EXPLORATION	DRILL HOLE LOG	HOLE NO.
W.A. Wampler & Associates Saunders, W. Va. Date and Report No.: May 1972	Method No.: 0700	Date: MAY 1972	No. 3 or J S-7

DRILL RIG GROUNDRIG DEPTH SITES	CORE - 4.5 GROUNDRIG DEPTH SITES	HOLE ELEVATION 1/07	LOGGED BY RET	HOLE DIAMETER 6 inches	DATE DRILLED 5/17 - 18/72	HOLE ELEVATION 1707	LOGGED BY RET
(0)	(GW, GP, SP.)	EMBANKMENT FILL					
(5)		Sandy Gravel, locally Grav- ely sand. Gray to black. About 5 $\frac{1}{2}$ - 5 $\frac{1}{2}$ " material (cobble- Gravel and +31" material are mostly carbonaceous shale and slate, with minor clay shale, sandstone, and coal. Sand is mostly carbonaceous shale and coal.	All				
(10)		Damp to moist @ 0-15 feet, very moist to saturated below 15 feet. Consistency given by blow counts.	All				
(15)			All				
(20)			All				
(25)			All				
(30)			All				
(35)	SP, SM, Hl., Cl.	Hostly sand, with scattered areas of silt and clay (?). Sand is largely (75%) coal, with the remainder carbon- aceous shale and siltstone or slate.	All				
(40)		Black, saturated, fine to medium-grained.	All				
(45)			All				
(50)			All				

ELEVATION (depth)	CLASS. FIELD IDENTIFICATION	DESCRIPTION FIELD IDENTIFICATION	SAMPLE NUMBER	NOTE	REMARKS	ELEVATION (depth)	CLASS. FIELD IDENTIFICATION	DESCRIPTION FIELD IDENTIFICATION (cont.)	SAMPLE NUMBER	NOTE	REMARKS
(0)						(50)		RESERVOIR SEDIMENTS (cont.)	D-7	D	3/3/6
(5)						(55)			-	All	-
(10)						(60)			PST-2	P	Recovery 1,2/2,0
(15)						(65)			-	All	-
(20)						(70)			D-8	D	2/1/1
(25)						(75)			-	All	-
(30)						(80)			SS-1	P	Recovery 0,0/4,0
(35)						(85)			-	All	-
(40)						(90)			-	All	-
(45)						(95)			-	D	12/10/16
(50)											N=26

1. Sample removed from tube for core-site examination.
- Notes:

COAL REFUSE DAN FAILURE Saunders, W. Va.	WA WAHL & ASSOCIATES Project # 0700 Date 10/10/72	SOIL EXPLORATION ORILL HOLE 06 Project # 0700 Date 10/10/72	DRILL EXPLORATION HOLE NO S-8 Project # 0700 Date 10/10/72
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DRILL RIG	CME - 45	HOLE ELEVATION 1704	LOGGED BY RET	
GROUNDWATER DPTH	FEET	DATE DRILLED 5/18-23/72	HOLE DIAMETER 6 inches	
<u>DATA FROM DRILLING SECTION</u>				
(ELEVATION (depth))	CLASS.	DESCRIPTION FIELD IDENTIFICATION	SAMPLE NUMBER	
(0)	PAN FAIL		NOKE KEY;	
(5)	GP, SP,	INDUSTRIAL FILL. Coal processing refuse. About 60% gravel and 40% sand with local concentrations of each. Minor fines, dark gray to black; damp to moist at 2-15 feet, very moist to sat- urated below 15 feet. Nodular carbonaceous shale and dolomite, minor clay shale and coal. Consistency given by blow counts.	All D 3/4/5 N= 9	AIH P Recovery 1.6/2.0
(10)			All	
(15)			All	
(20)	D 4/3/4	N= 7		
(25)	D 4/9/11	N=20		
(30)				
(35)	S-3	P Recovery 1.0/11.0 Motel		
(40)	D 9/18/15	N=33		
(45)				
(50)				
<u>RESERVOIR SEDIMENTS</u>				
SP	SP	Fine to medium sand, with a few scattered layers of silty sand, silt, and clay.	S-4	P Recovery 1.2/2.0
SH	SH	Black. About 50% coal re- mained carbonaceous shale, silstone, and clay shale.	D-5	D 1/6/5 N= 9
CH				
SS-1		P Recovery 3.0/3.0		
WA WALTER & ASSOCIATES	COAL REFUSE DAM FAILURE Saunders, W. Va.	SOIL EXPLORATION Drill Hole Log	HOLE No S-9	GEOL. REFL. DAM FAILURE Saunders, W. Va. Explor. & Recon. Work Date : May 1972 Or J

DRILL RIG	CME - 45	HOLE ELEVATION 1704	LOGGED BY RET
GROUNDWATER DPTH	FEET	DATE DRILLED 5/18-23/72	HOLE DIAMETER 6 inches
<u>DATA FROM DRILLING SECTION</u>			
(ELEVATION (depth))	CLASS.	DESCRIPTION FIELD IDENTIFICATION	SAMPLE NUMBER
(50)		RESERVOIR SEDIMENTS (cont.)	11-6
		RESERVOIR SEDIMENTS	D 1/6/7 N=13
			-
			All
			Sand flowing into anglers.
			SS-2 P Recovery 4.0/4.0
			-
			All
			D-7 D 1/3/6 N= 9
			-
			All
			S-5 P Recovery 2.0/2.0
			-
			All
			D-8 D 1/5/9 N=14
			-
			All
			D-9 D 2/6/7 N=13
			-
			All
			D-10 D 10/6 N= 6
			-
			All
			D-11 D 1/9/21/19 N=40
			-
			All
			D-12 D 1/6/27/3 N=50
			-
			Core Recovery 8.0/10.0 barrel (some stuck-up left in hole).
			W A WALTER & ASSOCIATES
			GEOL. REFL. DAM FAILURE Saunders, W. Va. Explor. & Recon. Work Date : May 1972 Or J
			GEOL. REFL. DAM FAILURE Saunders, W. Va. Explor. & Recon. Work Date : May 1972 Or J
			GEOL. REFL. DAM FAILURE Saunders, W. Va. Explor. & Recon. Work Date : May 1972 Or J
			GEOL. REFL. DAM FAILURE Saunders, W. Va. Explor. & Recon. Work Date : May 1972 Or J

DRILL NO. CME - 45	GROUNDARL DEPTH (below ground surface)	HOLE ELEVATION 1704	LOGGED BY REEF
		HOLE DIAMETER 6 inches	DATE DRILLED 5/18/23/72
ELEVATION (depth)	CLASS.	DESCRIPTION FIELD IDENTIFICATION	SAMPLE NUMBER
(100)		102.0-103.0 Silty sandstone. Local siltstone, gray, soft. Siltstone laminated, bedding horizontal.	CORE - Box 1
(105)		HOLE TERMINATED @ 105.0 FEET	
(110)		NOTE: 1. SAMPLE EXTRUDED FROM TUBE FOR ON-SIGHT EXAMINATION.	
COAL REFUSE DAM FAILURE Saunders, W. Va. May 1972			DRILL HOLE LOG
W.A. WALKER & ASSOCIATES P.O. BOX 4000 - MELTON, W. VA.			HOLE NO. S-9
SAMPLING MATERIALS			DATE
0700			MAY 1972
0700			JULY 3

DRILL RIG CME-45		HOLE ELEVATION 1701	LOGGED BY RET	HOLE ELEVATION 1701	LOGGED BY RET & KP
GROUNDWATER DEPTH 6 INCHES		HOLE DIAINTER 6 INCHES	DATE DRILLED 5/25-6/2/72	HOLE DIAMETER 6 INCHES	DATE DRILLED 5/26-6/2/72
ELEVATION (feet)	CLASS	DESCRIPTION FIELD IDENTIFICATION	SWELL NUMBER	REMARKS	
(0)		EMBANKMENT MATERIALS	-	AH	
(5)		May be slide material from the downstream face of Dam No. 3. Top few feet are flood deposits.	D-1	2 1/2 N=4	
		Gravelly sand, dark grey to black. Estimate 25% gravel, 75% sand, minor fines. Coal processing waste; about 1/3 coal (mostly in the sand), remainder largely siltstone and clay shale, locally saturated below 15 feet.	-	AH	
(10)		Riven by blow counts, local concentrations of both gravel and sand are present.	S-1	P Recovery 0.6/2.0 SOIL 1	
(15)			D-1	3 1/2 N=6	
(20)			-	AH	
	S-2	P Recovery 1.5/2.0			
D-2	D	2 1/2 N=5			
D-4	D	1 1/4 N=7			
S-3	P	Recovery 1.6/2.0			
D-5	D	1 1/2 N=19			
D-6	D	3 1/4 N=6			
S-4	P	Recovery 2.0/2.0			
D-7	D	5 1/2 N=10			
D-8	D	6 1/17 N=21			
S-5	P	Recovery 1.4/2.0			
D-9	D	5 1/5 N=10			
D-10	D	4 1/2 N=4			
S-6	P	Recovery 0.9/2.0 WITH 1			
D-11	D	9 1/8 N=17			
D-12	D	9 1/2 N=16 N=28			
S-7	P	Recovery 1.7/2.0			
		EMBANKMENT FILLS, INCORPORATING SLUDGE OR RESERVOIR SEDIMENTS			
(50)		COAL REFUSE DAM FAILURE Saunders, W., Va.			
	D-13	D 4 1/6 N=10			
	D-14	D 6 8/9 N=17			
		SOIL EXPLORATION DRAIL HOLE LOG			
		0.000 0.000 0.000 MW 1972			
		S-10			
		WA WAHLA & ASSOCIATES			
		SAUNDERS, W., Va. 0.000 0.000 0.000 MW 1972			
		WA WAHLA & ASSOCIATES			
		COAL REFUSE DAM FAILURE Saunders, W., Va. 0.000 0.000 0.000 MW 1972			
		SOIL EXPLORATION DRAIL HOLE LOG			
		0.000 0.000 0.000 MW 1972			
		S-10			

DRILL RIG CME-65	GROUNDWATER DEPTH CALLING SPOTS	HOLE ELEVATION	1701.	LOGGED BY	REI
		HOLE DIAMETER	6 INCHES	DATE DRILLED	S/24-6/2/72
(100)		ELEVATION (depth)	CLASS	DESCRIPTION FIELD IDENTIFICATION	SAMPLE NUMBER
				RESERVOIR SEDIMENTES (cont'dued)	S-15
6/1/72					P Recovery 0/1.6
(105)					D 15/10/10 N=20
6/2/72					NOTE 1
					Hole drilled 105.0 at end of work 6/1/72.
					All
					At beginning of work 6/2/72, penetrometer was put in hole and went directly to 109.0.
(110)		112.0-115.5 Sandstone, light gray, very fine to fine grained. Thin-bedded and thinly cross-bedded, moderately hard and strong.		CORE- BOX 1	D 578078 N=80+
(115)		115.5-120.0 Shiltstone, locally sandy or clayey. Thin-bedded to laminated. Dark grey. Some- what soft and weak.			Run 110.0-115.0 Recovery 2.0/5.0
(120)		HOLE TERMINATED @ 120.0 FEET.			Run 115.0-120.0 Recovery 4.3/5.0
(125)		NOTES:			
		1. Sample extruded from tube for on-site examination.			
		2. Excess recovery represents disturbed material which flowed into the auger stem.			
(130)		3. With no recovery in S-1, the penetrometer was lowered into the hole. It was driven from 100.7 to 103.1. The blows recorded are for the interval 101.6-103.1			
(135)					
(140)					
(145)					
(150)	WA WALTERS & ASSOCIATES	COAL REFUSE DAM FAILURE Sandstone, No. 4a. PROTOTYPE - Water Well - 2411	DRILL HOLE No. 106 0700	DRILL HOLE No. 106 0700	HOLE NO. S-10 3 in 3

DRILL RIG	CME 45	HOLE ELEVATION	170.1	LOGGED BY	RET
GROUNDWATER DEPTH		HOLE DIAMETER	6 INCHES	DATE DRILLED	6/5/97/2
SAMPLING SITES					
(0)	SP, GR, (Coal Processing Refuse)	SAMPLE NUMBER	NO:	REMARKS	
(5)	SP, SN- SS- about 30%	D	2/1/1	N=2	
(10)	SS- minor fines, Slightly damp to damp at 0-11 feet. Below 11 feet moisture content varies from damp to saturated, locally in intervals of 5 feet or less.	-	All	Easy augering - one or two hard cobbles.	
(15)	Top few feet are reworked by flood.	D-2	1/2/2	N=6	
(20)	-	-	All	-	
(25)	S-2	P	Easy push,		
	-	-	All	Recovery 0/2.0	
(30)	SS-1	P	Recovery 0/4.5		
	-	-	All	Sample fell from tube as tube was pulled up hole	
(35)	D-3	D	1/2/4	N=6	
	-	All	0 approx. 20 ft. White drilling fluid interval.	Recovery 2/0/2.0	
(40)	PST-1	P	Pushed 3/4-3/2.0		
	-	All	-		
(45)	D-4	D	5/5/10	N=15	
	-	All	-	Recovery 0/4.5	
(50)	SS-2	P	PST-2	6/7/2	
	TST-2	T	Recovery 0/4.5	6/8/2	
SOIL EXPLORATION					
WA WAHLER & ASSOCIATES	COAL REFUSE DAN FAILURE	DRILL	HOLE LOG	HOLE NO	HOLE NO
SAUNDERS, H., V.A.	Project No.	Date	Interval No.	Start No.	End No.
Phase I • Nitrogen Rich	0700	JUNE 1972	1 in 1	0700	2 ap 3
SOIL EXPLORATION					
WA WAHLER & ASSOCIATES	COAL REFUSE DAM FAILURE	DRILL	HOLE LOG	HOLE NO	HOLE NO
SAUNDERS, W., Va.	Project No.	Date	Interval No.	Start No.	End No.
Phase II • Nitrogen Rich	0700	JUNE 1972	1 in 1	0700	2 ap 3

DRILL RIG	CME 45	HOLE ELEVATION	170.1	LOGGED BY	RET
GROUNDWATER DEPTH		HOLE DIAMETER	6 INCHES	DATE DRILLED	6/5-9/72
SAMPLING SITES					
(0)	SP, SS- (Coal Processing Refuse)	ELEVATION (feet)	CLASS.	DESCRIPTION FIELD IDENTIFICATION	SAMPLE NUMBER
(5)	SP- SN- SS-	6/5/72 (50)	SP- S4 (Continued)	Embankment Materials	SP- S4
(10)	SS- about 30%	6/6/72	SP- S4	Gravelly sand mixed or interbedded with local, black sand in layers up to a few feet thick. The black sand is similar to the "typical" reservoir sediments found deeper in this hole and beginning at depths of 10-35 feet in holes upstream of this one.	-
(15)	SS- minor fines, Slightly damp to damp at 0-11 feet. Below 11 feet moisture content varies from damp to saturated, locally in intervals of 5 feet or less.	(55)	SP- S4	-	All
(20)	Top few feet are reworked by flood.	(60)	SP- S4	-	All
(25)	-	(65)	SP- S4	-	All
(30)	-	6/6/72 6/7/72	SP- S4	Cleaned hole with water before taking PST-1	6/9/11
(35)	-	(70)	SP- S4	-	All
(40)	-	(75)	SP- S4	-	All
(45)	-	(80)	SP- S4	RESERVOIR SEDIMENTS Ni, Cl,	PST-4
(50)	-	(85)	SP- S4	Black fine to very fine sand, mostly coal with local silt, and clayey silt layers. A few scattered areas of gravelly material. Generally moist to very moist, locally saturated.	Recovery 0/2.0/1.3 D-10 N=10
(55)	-	(90)	SP- S4	-	Cleaned hole w/ water to 85.0', after auger bit SS-3
(60)	-	(95)	SP- S4	-	Pushed 85.0-89.1 Recovery 4.0/4.1 D-11 N=6
(65)	-	6/7/72	SP- S4	-	All
(70)	-	6/8/72	SP- S4	-	All
(75)	-	6/8/72	SP- S4	-	All
(80)	-	6/8/72	SP- S4	-	All
(85)	-	6/8/72	SP- S4	-	All
(90)	-	6/8/72	SP- S4	-	All
(95)	-	6/8/72	SP- S4	-	All

DRILL RIG CME 45	GROUNDHOLE DIAH. 6 INCHES	HOLE ELEVATION 1703	LOGGED BY PFT
(Depth)		HOLE DIAMETER 6 INCHES	DATE DRILLED 6/5/972
ELEVATION (Depth)	CLASS.	DESCRIPTION FIELD IDENTIFICATION	SAMPLE NUMBER
(100)		REServoir SEDIMENTS (Continued)	D-13
(105)			-
(110)		SOL. AND MUDWASH SILTY clay soil, gravelly alluvium with scattered fragments of coal waste.	PST-6
(115)		BEDROCK KANAMIA SERIES 112.0-117.0 Sandstone, tan, arkosic, medium-grained 117.0-118.0 Black Carbonaceous shale. 118.0-118.6 Coal, black, hard bedding, weak fracture.	D-14
(120)		118.6-120.5 Siltstone, gray, thin-bedded to laminated, bedding nearly horizontal.	Core Box 1
(125)		HOLE TERMINATED @ 120.5 FT.T.	BBL
(130)			
(135)			
(140)			
(145)			
(150)			
WA. WAIKU & ASSOCIATES	COAL REFUSE DAM FAILURE Saunders & Va	SOIL EXPLORATION Drill Hole Log	HOLE NO S-11 S-1
	PALO ALTO • REPUBLIC	Project no. 07000	JUNE 1972
		Reprint date 3	3 or 3

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DRILL RIG CME-45	GROUNDWATER DEPTH (feet) 144.1	HOLE ELEVATION 1750	LOGGED BY RETRIEVAL DATE DRILLED 6/28&7/10-7/14/72		
ELEVATION (feet)	CLASS	DESCRIPTION FIELD IDENTIFICATION	SAMPLE NUMBER	WEIGHT lb/cu ft	REMARKS
(0)		EMBANKMENT FILL	D-1	277.8	N=15
		Coal Processing waste 30-10' Mixed coal processing waste and road cut derived fill 0- 10-28 feet.	-	-	AH
(5)		Coal waste is about equal parts sand and gravel. The same is largely coal and shale;	D-2	172.2	N=4
		The gravel mostly siltstone and carbonaceous shale with minor coal and sandstone. The road cut derived is mostly hard sandstone gravel and cobbles with a blinder of clayey sand and soil, and minor coal waste.	-	-	AH
(10)		D-3	D 127.8/6	N=26	
		-	-	-	AH
(15)		D-4	D 54/4.5	N=9	
		-	-	-	AH
(20)		D-5	D 172/4	N=6	
		-	-	-	AH hole is cased with hollow stem auger
(25)		D-6	D 67.12/8	N=20	
		-	-	-	Very hard augering below 28'
(30)		BEDROCK-KANAMIA SERIES	-	-	AH
		28.0-42.0	D-7	60	blows/0.0 ft N = very large core box
		Mudstone; olive gray; low hardness; crushed to 40.5'; closely fractured 40.5'-42.0'; Red, yell, brn, clay in all fractures.	1	1	Recovery difficult to measure because of crushed material
(35)		6/28/72 LAR	(10.0- 45.0)	(85)	
(40)		42.0-45.5	D-8	7/13/72	Run 36.9-42.0 Recovery 4.5/5.2
		Sandstone; Silty; fine- grained; irregularly mottled lt. & dk. gray; mod. hard.	2	(90)	Run 42.0-47.0 Recovery 5.0/5.0 Casing set to 40.5
(45)		45.5-46.8	Core Box		
		SS Dips 3° 16.8-47.8 Cont.	(45.0- 60.2)		Run 47.0-52.0 Recovery 4.7/5.0
(50)	WA WAHLA & ASSOCIATES	COAL REFUSE DAN FAILURE Sandstone, W. Va.	DRILL HOLE NO.	SOIL EXPLORATION DATE	WA WAHLA & ASSOCIATES
		Sample # 1000 # of Holes 1000	100	JUN 1972	WA WAHLA & ASSOCIATES
		Sample # 1000 # of Holes 1000	100	JUN 1972	WA WAHLA & ASSOCIATES
		Sample # 1000 # of Holes 1000	100	JUN 1972	WA WAHLA & ASSOCIATES

DRILL RIG CME-45	GROUNDWATER DEPTH (feet) 144.1	HOLE ELEVATION 1750	LOGGED BY LAR		
ELEVATION (feet)	CLASS	DESCRIPTION FIELD IDENTIFICATION	HOLE DIAMETER 6 INCHES	HOLE ELEVATION 1750 6 INCHES	LOGGED BY LAR DATE DRILLED 6/28&7/10-7/14/72
(0)		CLAYSTONE: Ned. dk. Gray; internally silkened in random directions. Bedding is 16' from horizontal.	(50)	47.8-51.6	Core Box
		7/12/72	(55)	51.6-52.5	Core Box
(5)		SANDSTONE: Ned. lt. Gray; fine to med. Grained; hard; 80% angular quartz grains; remains as dark minerals, mica, and some feldspar. Dark materials are concentrated in streaks showing cross bedding with most fractures being on these bands.	(60)	52.0-52.0	Core Box
		7/12/72	(65)	52.5-53.1	Core Box
(10)		MUDSTONE: clayey; med. dk. gray; low hardness.	(70)	53.1-109.2	Core Box
		7/12/72	(75)	54.6-52.5;	Core Box
(15)		LITTLE FRACTURING; fresh. 1" Mudstone band 0.57.5 1/2" Sandstone Band 062.0	(80)	55.0-100.5	Core Box
		7/12/72	(90)	56.0-57.5	Core Box
(20)			(95)	57.0-58.8	Core Box
		7/12/72	(100)	58.0-59.8	Core Box
(25)		CONTAINS SANDSTONE & D detrital coal lens @ 39.8			
		7/12/72			
(30)		BECOMES medium grained @ 86.0-100.5			
		7/12/72			
(35)		CONTAINS SANDSTONE & D detrital coal lens @ 39.8			
		7/12/72			
(40)		Many irregular siltstone lenses 91.0-92.0			
		7/12/72			
(45)		Core Box			
		7/12/72			
(50)	WA WAHLA & ASSOCIATES	COAL REFUSE DAM FAILURE Sandstone, W. Va.	DRILL HOLE NO.	SOIL EXPLORATION DATE	WA WAHLA & ASSOCIATES
		Sample # 1000 # of Holes 1000	100	JUN 1972	WA WAHLA & ASSOCIATES
		Sample # 1000 # of Holes 1000	100	JUN 1972	WA WAHLA & ASSOCIATES
		Sample # 1000 # of Holes 1000	100	JUN 1972	WA WAHLA & ASSOCIATES

DRILL RIG CNE-45		LOGGED BY LAR		HOLE ELEVATION 1750		HOLE ELEVATION 1750		LOGGED BY LAR	
GROUNDWATER DEPTH 6"		DATE DRILLED 6/28/67/07/14/77		POLE DIAMETER 6 INCHES		POLE DIAMETER 6 INCHES		DATE DRILLED 6/28/67/07/14/77	
CNE-45		CNE-45		CNE-45		CNE-45		CNE-45	
ELEVATION (feet) (100)	CLASS	DESCRIPTION FROTH IDENTIFICATION	SAMPLE NUMBER	WEIGHT lb/ft	REMARKS	ELEVATION (feet) (150)	CLASS	DESCRIPTION FROTH IDENTIFICATION	SAMPLE NUMBER
(100)		55.1-109.2 SANDSTONE: (Cont. from) coal filled fractures 100.4-106.4 ft.	Core Box 5	Sx	Run 97.0-107.0 (Continued)	131.7-150.6 SANDSTONE: (Continued) Grades into	Core Box 9	Nx Core RBI.,	Ran 167.0-157.0 (Continued) Recovery 10.0/10.0
(105)		6-100.7 dip for 32°; and many irregular fine lenses of siltstone and coal from 100.7 to 102.1	Core Box 6	Sx	-	150.6-153.9 SILTSTONE: Med. dk. gray; mod. hard; little fractured; fresh; horizontal bedding.	Core Box 10	Nx Core RBI.,	Run 157.0-164.0 Recovery 7.0/7.0
		-Bedding dips 20° at 103.0-118.6	Core Box 7	Sx	Run 107.0-117.0 Recovery 10.0/10.0	153.9-156.0 CLAYSTONE: Med. dk. gray; mod. hard; w/1/20' considerate breaks dipping 35°; horizontal bedding; contact w/ siltstone horiz. Grades into:	Core Box 10	Nx Core RBI.,	Run 164.0-174.0 Recovery 9.8/10.0
(110)		-Many small lenses of siltstone from 105-107'	Core Box 8	Sx	Run 117.0-127.0 Recovery 10.0/10.0	156.0-159.3 SILTSTONE: Med. dk. gray; mod. hard; containing fine sand & crushed below 158.8.	Core Box 11	Nx Core RBI.,	Run 165.0-175.0 Recovery 10.0/10.0
		Coal filled fractures @ 105.3 and 105.7	Core Box 9	Sx	-	159.3-160.8 COAL: Clayey 0159.6-160.3; pyritic-rich lens 0160.6	Core Box 12	Nx Core RBI.,	Run 166.0-176.0 Recovery 10.0/10.0
(115)		Siltstone lenses from 108.2-109.2 derived from shale below	Core Box 10	Sx	Run 127.0-137.0 Recovery 10.0/10.0	159.3-174.0 SILTSTONE: Sility; fine; hard; mortified lt. and dk. gray below 161', w/ coal filled fracture (clastic dike) dipping 38° @ 162.2-163.1	Core Box 13	Nx Core RBI.,	Run 167.0-177.0 Recovery 10.0/10.0
		SHALE: Med. dk. gray; low hardness; fresh; little fracturing; horiz. bedding	Core Box 11	Sx	-	-Beds dips 45° from 164.0-165.3, otherwise horizontal - 1/2" clay seam @ 166.6' and 165' - Sandstone 1/2" siltly from 167-168'.	Core Box 14	Nx Core RBI.,	Run 168.0-178.0 Recovery 10.0/10.0
(120)		Contact w/S is irregular - fracture dipping 75° at 112.0-112.9 coated with tabular (barite?) crystals	Core Box 12	Sx	Run 127.0-137.0 Recovery 10.0/10.0	160.0-161.3 SILTSTONE: Sility; fine; hard; mortified lt. and dk. gray below 161', w/ coal filled fracture (clastic dike) dipping 38° @ 162.2-163.1	Core Box 15	Nx Core RBI.,	Run 169.0-179.0 Recovery 10.0/10.0
		-1/2" coal seam @ 113.0	Core Box 13	Sx	-	-Beds dips 45° from 164.0-165.3, otherwise horizontal - 1/2" clay seam @ 166.6' and 165' - Sandstone 1/2" siltly from 167-168'.	Core Box 16	Nx Core RBI.,	Run 170.0-180.0 Recovery 10.0/10.0
(125)		-Coal lenses 311.0-311.5.0	Core Box 14	Sx	Run 127.0-137.0 Recovery 10.0/10.0	160.0-161.3 SILTSTONE: Sility; fine; hard; mortified lt. and dk. gray below 161', w/ coal filled fracture (clastic dike) dipping 38° @ 162.2-163.1	Core Box 17	Nx Core RBI.,	Run 171.0-181.0 Recovery 10.0/10.0
		-Massive from 115.0-123.0	Core Box 15	Sx	-	-Beds dips 45° from 164.0-165.3, otherwise horizontal - 1/2" clay seam @ 166.6' and 165' - Sandstone 1/2" siltly from 167-168'.	Core Box 18	Nx Core RBI.,	Run 172.0-182.0 Recovery 10.0/10.0
(130)		-Detrital coal lens @ 122.3 and 122.8	Core Box 16	Sx	Run 127.0-137.0 Recovery 10.0/10.0	160.0-161.3 SILTSTONE: Sility; fine; hard; mortified lt. and dk. gray below 161', w/ coal filled fracture (clastic dike) dipping 38° @ 162.2-163.1	Core Box 19	Nx Core RBI.,	Run 173.0-183.0 Recovery 10.0/10.0
		Becomes finer grained and darker with depth below 12.2'	Core Box 17	Sx	-	-Beds dips 45° from 164.0-165.3, otherwise horizontal - 1/2" clay seam @ 166.6' and 165' - Sandstone 1/2" siltly from 167-168'.	Core Box 20	Nx Core RBI.,	Run 174.0-184.0 Recovery 10.0/10.0
(135)		129.2-131.2 COAL: Horizontal bedding and contacts.	Core Box 18	Sx	Run 137.0-147.0 Recovery 10.0/10.0	160.0-161.3 SILTSTONE: Med. dk. gray; fine grained; hard; fissile, mottled lt. & dk. gray w/minor cross bedding in coal mineral to 139'. Bedding is mostly horizontal below 139'.	Core Box 21	Nx Core RBI.,	Run 175.0-185.0 Recovery 10.0/10.0
		131.7-131.7 CLAYSTONE: dk. gray grad to intro	Core Box 19	Sx	-	160.0-161.3 SILTSTONE: Med. dk. gray; fine grained; hard; fissile, mottled lt. & dk. gray w/minor cross bedding in coal mineral to 139'. Bedding is mostly horizontal below 139'.	Core Box 22	Nx Core RBI.,	Run 176.0-186.0 Recovery 10.0/10.0
(140)		131.7-150.6 SANDSTONE: Med. olive gray; fine grained; hard; fissile, mottled lt. & dk. gray w/minor cross bedding in coal mineral to 139'. Bedding is mostly horizontal below 139'.	Core Box 20	Sx	Run 167.0-157.0 Recovery 10.0/10.0	160.0-161.3 SILTSTONE: Med. dk. gray; fine grained; hard; fissile, mottled lt. & dk. gray w/minor cross bedding in coal mineral to 139'. Bedding is mostly horizontal below 139'.	Core Box 23	Nx Core RBI.,	Run 177.0-187.0 Recovery 10.0/10.0
		WA WALTER & ASSOCIATES	Core Box 21	Sx	WA WALTER & ASSOCIATES	160.0-161.3 SILTSTONE: Med. dk. gray; fine grained; hard; fissile, mottled lt. & dk. gray w/minor cross bedding in coal mineral to 139'. Bedding is mostly horizontal below 139'.	Core Box 24	Nx Core RBI.,	Run 178.0-188.0 Recovery 10.0/10.0
(150)		WA WALTER & ASSOCIATES	Core Box 22	Sx	WA WALTER & ASSOCIATES	160.0-161.3 SILTSTONE: Med. dk. gray; fine grained; hard; fissile, mottled lt. & dk. gray w/minor cross bedding in coal mineral to 139'. Bedding is mostly horizontal below 139'.	Core Box 25	Nx Core RBI.,	Run 179.0-189.0 Recovery 10.0/10.0

DRILL RIG ACKER AD-2			HOLE ELEVATION 1657			LOGGED BY GJA			HOLE ELEVATION 1657			LOGGED BY GJA					
GROUNDBREAKER 6 INCH CAL. 1000 ft. 101.8			HOLE DIAMETER 6 INCHES			DATE DRILLED 7/13-14/72			HOLE DIAMETER 6 INCHES			DATE DRILLED 7/14-18/72					
ELEVATION LOCATION	CLASS	DESCRIPTION FIELD IDENTIFICATION	SAMPLE NUMBER	HOLE	REMARKS	ELEVATION (Depth)	CLASS	DESCRIPTION FIELD IDENTIFICATION	SAMPLE NUMBER	HOLE	REMARKS	ELEVATION (Depth)	CLASS	DESCRIPTION FIELD IDENTIFICATION	SAMPLE NUMBER	HOLE	REMARKS
(0)		EMBANKMENT FILL	-	All	-	(50)	SIP GP	EMBANKMENT FILL (Continued)	S-5	P	recovery 1.71.9	-	-	-	-	-	-
(5)		REFUSE BANK	-	All	-	1/16/72 7/15/72 7/16/72	-	-	-	All	-	-	-	-	-	-	
(10)		Coal processing waste of mixed sand and gravel with local concentrations of each. Sand is 50% coal. The remainder is shale and minor red-ocher.	D-1	D	7/9/8 N=17	(6.)	D-6	D	7/16/19	N=35	-	-	D-7	D	24/25/26	N=51	
(15)		Generally coarse grained, angular and blocky fragments.	-	All	Drilling Rapid	-	-	-	-	All	-	-	D-8	D	28/27/28	N=51	
(20)		Gravel is mixed coal, carbonaceous shale, light gray shale, and red-ocher. The fragments are angular, blocky to platy and are 1" to greater than 1" in size. A few cobbles from 3" to 12" or more in diameter are present.	-	All	-	(65)	D-9	refusal, tube rutted	-	All	-	-	D-10	D	5/4/79	N=13	
(25)		Moisture content slightly damp to moist.	S-2	P	Recovery 1.8/2.0	(70)	D-10	D	5/10/7	N=17	-	-	D-11	D	5/10/7	N=17	
(30)		Consistency given by blow counts.	-	All	Rapid Drilling	(75)	D-12	D	5/10/9	N=19	-	-	D-13	D	5/11/8	N=79	
(35)		-	D-3	D	7/2/3 N=5	(80)	D-13	D	5/11/8	N=79	-	-	D-14	D	12/9/10	N=19	
(40)		-	-	All	-	(85)	D-14	D	12/9/10	N=19	-	-	D-15	D	12/9/10	N=19	
(45)		S-3	P	Recovery 1.9/2.0	7/17/72	(90)	D-16	D	12/9/10	N=19	-	-	D-17	D	12/9/10	N=19	
(50)		-	D-4	D	5/3/3 N=6	(95)	D-18	D	12/9/10	N=19	-	-	D-19	D	12/9/10	N=19	
		-	-	All	-	(100)	D-20	D	12/9/10	N=19	-	-	D-21	D	12/9/10	N=19	
		-	S-4	P	Recovery 1.6/2.0	(90)	D-22	D	12/9/10	N=19	-	-	D-23	D	12/9/10	N=19	
		-	D-5	D	5/10/17 N=27	(95)	D-24	D	12/9/10	N=19	-	-	D-25	D	12/9/10	N=19	
		-	-	All	Rapid drilling	(100)	D-26	D	12/9/10	N=19	-	-	D-27	D	12/9/10	N=19	
		WA WAHLER & ASSOCIATES	COAL REFUSE DAM FAILURE Saunders, W. A.	SOIL EXPLORATION DATE JULY 1972 PROJECT NO. 0100	DRILL HOLE L.G. NO S-13	WA WAHLER & ASSOCIATES	COAL REFUSE DAM FAILURE Saunders, W. A.	SOIL EXPLORATION DATE JULY 1972 PROJECT NO. 0100	DRILL HOLE L.G. NO S-13	WA WAHLER & ASSOCIATES	COAL REFUSE DAM FAILURE Saunders, W. A.	SOIL EXPLORATION DATE JULY 1972 PROJECT NO. 0100	DRILL HOLE L.G. NO S-13	WA WAHLER & ASSOCIATES	COAL REFUSE DAM FAILURE Saunders, W. A.	SOIL EXPLORATION DATE JULY 1972 PROJECT NO. 0100	DRILL HOLE L.G. NO S-13

DRILL RIG	ACKER AD-2	HOLE ELEVATION	1657	LOGGED BY	GJA
GROUNDWATER DEPTH	101.8	HOLE DIAMETER	6 INCHES	DATE DRILLED	7/18-7/19/72
LOGGED BY	SAUNDERS, W.	PROJECT NO.	0700	SHOT NO.	3 or 3
(100)		DESCRIPTION	SAMPLE NUMBER	WEIGHT	REMARKS
	CLASS.	FIELD IDENTIFICATION			
(100)		SOIL (Continued)	D-15	b	13/16/72 N=27
7/18/72	BEDROCK				
-(105)	KANAMIA SERIES				
7/19/72	102.0-106.8 Silty Shale	Light gray, moderately hard, slightly weathered shale with horizontal thin to laminated bedding.	D-16		0.178 N=51 refusal
(110)	106.8-109.2 Coal Seam	Coal layer with carbonaceous shale interbed at 107.2-108.0 coal has pitchy luster, bucky fracture, and is moderately hard and horizontally bedded. Shale interbed is soft, dark gray, clayey carbonaceous, and laminated.	CORE BOX	Nx	
7/19/72	-(115)				Hole terminated at desired depth.
(120)	109.2-115.0 Shaly, fine to medium grained, light gray sandstone which is moderately hard, fresh, and cross-bedded. It contains thin medium grain 1/10 inch thick interbeds of medium gray shale. These stone beds are approximately 0.8' to 1.5' thick.				
					hole terminated at 115.0 feet.
WA WAHLER ASSOCIATES	COAL REFUSE DAM FAILURE	DRILL HOLE LOG	HOLE NO.		
	Project No. Date Drilled • Shot No.	Shot No. Date	Shot No. Date		
		0700	JULY 1972	3 or 3	S-13

DRILL RIG C-45		BOLE ELEVATION 1692	LOGGED BY LAR	DATE DRILLED 7/19-24/72
GROUNDWATER DPH		HOLE DIAMETER 6 INCHES		
ELAVATION (feet) (50)	CLASS	DESIGN PITCH FIELD IDENTIFICATION	SAMPLE NUMBER	REMARKS
	SM	16'-104'	D-16	D 0/1/2 N=3
		BEDROCK/Sediments (Cont'd)	D-17	D 0/1/2 N=3
(55)	SP -	lens of predominantly red, grained coal fragments (.66") few fines.	-	All
(60)	SS		D-18	D 1/2/1 N=5
			-	All
			D-19	D 2/4/4 N=8
			-	All
			D-20	D 2/3/5 N=8
			-	All
(70)	SL	70'-104' SLCT: With very fine carbonaceous sand; grayish black. -Sampler usually drops under weight of rods for 2' then must be driven to retain sample.	D-21 D-22	D 1/2/2 N=0 N=6 ---
7/20/72			-	All
7/21/72			D-23 D-24	D 1/1/1 N=0 N=2 ---
(75)			-	All
			-	-
(80)			-	All
			D-25 D-26	D 1/1/1 N=1 Held at bottom of sum.
			-	All
(85)			-	-
(90)			-	-
(95)			D-27 D-28	D 1/6/5 N=0 N=11 ---
(100)			-	All
WA WAHLER AND ASSOCIATES	COAL REFUSE DAH FAILURE Samples, W. Wahl Field 410 - Meridian Mine - 1410	DRILL HOLE LOG 0700	SOIL EXPLORATION MATERIAL JULY 1972 2' x 3'	HOLE NO S-14

DRILL RIG CHT-65 FRANCONIER OPEN PIT, SAUSALITO, CALIF.		HOLE ELEVATION feet	1692	LOGGED BY LAR
		HOLE DIAMETER 6 INCHES	DATE DRILLED 7/19-26/72	
ELEVATION (feet)	CLASS	DESCRIPTION FIELD IDENTIFICATION	SAMPLE NUMBER	LOG
(0)		0-10' BANKMENT FILL. Dam embankment materials made up of coal processing waste, mostly sandy gravel with the gravels being pre- dominantly med.-dk. gray sili- stones and shales, fine to coarse and angular with some coal and sandstone fragments. There are occasional stabs of shale to 1' in diam. The sand is fine to medium grained and silty from coal sludge.	D-1	All 3/2/2 N=4
(5)	CM		-	All -
(10)			D-2	D 1/2/2 N=4
(15)			D-3	D 1/1/2 N=3
			D-4	D 2/3/1 N=6
			-	All -
(20)			S-1	P 0.2' silty 1.8' 2' 0' in hole
			D-5	D 2/3/3 N=6
			-	All -
(25)			D-6	D 1/2/2 N=4
			D-7	D 2/3/3 N=6
			-	All -
(30)			D-8	D 1/2/2 N=4
			D-9	D 3/5/5 N=10
			-	All -
			D-10	D 1/2/2 N=4
			D-11	D 3/4/5 N=9
			-	All -
7/19/72 7/20/72		34'-104' RESERVOIR SEDIMENTS 34'-70'	D-12	D 0/1/1 N=2
		SN SAND: silty; fine to medium grained, brownish black; carbonaceous.	D-13	D 1/1/2 N=3
		SG Clayey lens @ 41.5'.	-	All -
(45)			D-14	D 0/1/1 N=2
			D-15	D 2/1/5 N=8
(50)			-	All -
COAL REFUSE DAM FAILURE Saunders, W. Va.		SOIL EXPLORATION LOG		
PROD ID: 41000000000000000000		DRILL NO.	DATE	HOLE NO.
		0700	JULY 19/72	1 on 3 S-1

DRILL RIG CH-45		HOLE ELEVATION 165'2"	LOGGED BY LAR
GROUNDWATER DEPTH Water second surface		HOLE DIAMETER 6"	DATE DRILLED 7/19-24/72
ELEVATION (feet)	CLASS.	DESCRIPTION FIELD IDENTIFICATION	SAMPLE NUMBER
(100)	M.	70-104.0' SILT (Continued)	All
(105)	SG-	104.0(approx.)-115.5' SAND: Gravelly; medium to coarse granular subangular to subrounded quartz sand with approx. 40-50% fine to coarse subrounded gravels of various types; II. olive gray clay binder (approx. 10%)	D 115A
7/21	OC		Sampler dropped under own wt. 0.5 5/9/14 N-23
7/24			
(110)			All
(115)		HOLE TERMINATED @ 115.5 FEET.	Auger refusal at 115.5' Hole left uncased.
WA WAHLER & ASSOCIATES		COAL REFUSE DAM FAILURE Saunders, W. Va. Project no. 1000 Field no. 1000	DRILLING TIME 0700 JULY 1972 HOLE NO S-14 1 or 3 S-14

DRILL RIG		ACKER AD-2		HOLE ELEVATION	1657	LOGGED BY	GJA
GROUNDSWATER DEPTH		8 FT.		DATE DRILLED		7/19/72-7/20/72	
GROUNDSWATER DEPTH (F.T.)		HOLE DIAMETER 4 INCHES		HOLE DIAMETER		4 INCHES	
ELEVATION (Depth)	CLASS	DESCRIPTION FIELD IDENTIFICATION	SAMPLE NUMBER	WTG	REMARKS		
(0)	G6 SP	STREAM GRAVEL Poorly sorted stream gravel and interbedded gravelly mud. To coarse, black sand.	-	All	Boring easy		
(5)		Gravel consists of shale, coal and minor red clay up to 12" or more in diameter. Sand is angular, blocky, poorly sorted and full of coal Beds are nearly horizontal and 3 to 5 ft. thick (?) .	-		Hit water at 8'.		
(10)		Saturated bottom depth of 8 ft.	-	All	Installed 4" casing		
7/19	D-1	D	2/5/6	No-9			
(15)	D-2	D	3/3/6	No-7			
7/20	-	All	-				
(20)	D-3	D	4/7/6	No-13			
	-	All	-				
(25)	D-4	D	7/7/9	No-16			
					Attempted to clean hole at 30 ft. to sample. Casing began to sink ahead of bit.		
(30)	SM M	RESERVOIR SEDIMENT Saturated silty, black laminated coaly sand with clayey lens. Fine to medium grained.	-	RD	Caught casing and drilled to 36 ft. Took Shelby at this depth.		
(35)							
(40)		S-1	P	Recovery 2/0/2/0			
		-	RD	Casing pushed into hole.			
(45)		S-2	P	Recovery 1/7/2/0			
				Top of S-2 is reser- voir sediment. Bottom is red clay gravel.			
(50)		D-5	D	10/9/12 No-21			
		-	RD	D-5 is red clay gravel.			
		(100)					
	COAL REFUSE DAM FAILURE	SOIL EXCAVATION	DRILL HOLE LOG	HOLE NO	ORILL HOLE LOG	HOLE NO	
WA WAHLER & ASSOCIATES	SAUNDERS, W. Va.	Project no July 1972	Sample no July 1972	Project no July 1972	Sample no July 1972	Project no July 1972	Sample no July 1972

DRILL RIG		ACKER AD-2		HOLE ELEVATION	1657	LOGGED BY GJA	
GROUNDSWATER DEPTH		8 FT.		DATE DRILLED		7/20/72-7/25/72	
GROUNDSWATER DEPTH (F.T.)		HOLE DIAMETER 4 INCHES		HOLE DIAMETER		4 INCHES	
ELEVATION (Depth)	CLASS	DESCRIPTION FIELD IDENTIFICATION	SAMPLE NUMBER	WTG	REMARKS		
(50)	GP	REFUSE BANK (RED DOG) (CONTINUED) Red dog brevet 1/4" to 4". Most appears to be 2" in diameter. In poorly sorted, black, coarse silty sand. No clay. Gray shale and places of coal rare, saturated.	(50)	GP	REFUSE BANK (RED DOG) (CONTINUED) Red dog brevet 1/4" to 4". Most appears to be 2" in diameter. In poorly sorted, black, coarse silty sand. No clay. Gray shale and places of coal rare, saturated.	-	-
7/20			7/20			RD	-
			7/21			-	D 9/8/5 N=13
(60)							
(65)						D-7	D 15/15/15 N=30
(70)							
(75)							D 12/35/0 N=85
(80)							Refusal D-8 consists of weathered silty sandstone. Pounded casing to 76 feet and met with refusal. This point. Casing when piled also had about 1 foot of wea- thered sandstone in it.
(85)							
(90)							
(95)							
(100)							
WA WAHLER & ASSOCIATES	SAUNDERS, W. Va.	Project no July 1972	Sample no July 1972	Project no July 1972	Sample no July 1972	Project no July 1972	Sample no July 1972

DRILL RIG	CME-45	HOLE ELEVATION	1700	LOGGED BY	LAR
GROUNDWATER DEPTH		DATE DRILLED	7/27/72	HOLE DIAMETER	6 INCHES
(called ground surface)					
ELEVATION (feet)	CLASS.	DESCRIPTION FIELD IDENTIFICATION	SAMPLE NUMBER	NOTE	REMARKS
(0)	GS	0-68' EMBANKMENT FILL:		Hole cased with 6"	
		Dam embankment materials made up of coal processing waste; mostly sandy gravels with the gravels being med., gray siltstones and shale, fine to coarse and angular with coal and sandstone frag- ments. Approx. 30% fine to med. Grained silty sand.		hole stem niger.	
(5)				All	
(10)				All	
(15)				All	
(20)				All	
(25)	GC			All	
(30)				All	
(35)	GN			All	
(40)				All	
(45)				All	
(50)				All	
CLAYEY SAMPLE 025'					
(10)					
(30)					
(40)					
(50)					

DRILL RIG	CME-45	HOLE ELEVATION	1700	LOGGED BY	LAR
GROUNDWATER DEPTH		DATE DRILLED	7/27/72	HOLE DIAMETER	6 INCHES
(called ground surface)					
ELEVATION (feet)	CLASS.	DESCRIPTION FIELD IDENTIFICATION	SAMPLE NUMBER	NOTE	REMARKS
(0)	GS	0-68' EMBANKMENT FILL:		Hole cased with 6"	
		Dam embankment materials made up of coal processing waste; mostly sandy gravels with the gravels being med., gray siltstones and shale, fine to coarse and angular with coal and sandstone frag- ments. Approx. 30% fine to med. Grained silty sand.		hole stem niger.	
(5)				All	
(10)				All	
(15)				All	
(20)				All	
(25)				All	
(30)				All	
(35)				All	
(40)				All	
(45)				All	
(50)				All	
SOIL FORMATION					
COAL REFUSE DAM FAILURE					
Saunders, W. Va.					
W.A. WHITLER & ASSOCIATES					
PALEO SITE • MASTRIAN STRATUM					
PROJECT TO 0700 JUNE 1972					
HOLE NO. S-16					
SOIL EXPLORATION					
DRILL HOLE LOG					
PROJECT TO 0700 JULY 1972					
HOLE NO. S-16					

DRILL RIG	CME-45	HOLE ELEVATION	1700	LOGGED BY	LAR
GROUNDWATER DEPTH		HOLE DIAMETER	6 INCHES	DATE DRILLED	7/24-25/72

DRILL RIG	CME-45	GROUNDRIGE DEPTH		HOLE ELEVATION	1700	LOGGED BY	LAR
DATE DRILLED	7/24-25/72	HOLE DIAMETER	6 INCHES	HOLE NUMBER	6	DATE DRILLED	7/24-25/72

ELEVATION (feet)	CLASS.	DESCRIPTION FIELD IDENTIFICATION	SAMPLE NUMBER	NOTES	NOTES	ELEVATION (feet)	CLASS.	DESCRIPTION FIELD IDENTIFICATION	SAMPLE NUMBER	NOTES	NOTES
(0)		0-33' EMBANKMENT FILL: Dun embankment materials made up of coal processing waste. Mostly sandy gravels consisting of med. dk. gray silty and shale; fine to coarse with coal fragments; approx. 30% fine to medium grained silty sand.		All	Hole cased with 6" hollow stem auger.	(50)		33'-60' RESERVOIR SEDIMENTS: (Cont'd from 1)		-	AH
(5)						(55)		SM			D-7
(10)						(60)		DRBK 60'-70' ADDICKS-KAINMA SERIES: SANDSTONE: Yellowish gray; weathers to mod. yell. brn.; mostly fine to medium, sub- rounded quartz grains and alc.		-	All D-60'.
(20)					Saturated at 12'	(65)				D-8	14/16/17 N=33
(25)						(70)		HOLE TERMINATED @ 70.0 FEET.		-	All Auger refusal @ 70'.
(30)						(75)					Hole left uncased.
(35)						(80)					
(40)						(85)					
7/24	(45)					(90)					
7/25	(50)					(95)					
						(100)					

DRILL RIG	CME-45	GROUNDRIGE DEPTH		HOLE ELEVATION	1700	LOGGED BY	LAR
DATE DRILLED	7/24-25/72	HOLE DIAMETER	6 INCHES	HOLE NUMBER	6	DATE DRILLED	7/24-25/72
WA WAHLER & ASSOCIATES							
WA WAHLER	COAL REFUSE DAM FAILURE	SOIL EXPLORATION	HOLE NO	DRILL HOLE LOG	DRILL HOLE LOG	HOLE NO	
WA WAHLER & ASSOCIATES	SAUNDERS, W. V.	PROJECT NO.	DATE	PROJECT NO.	DATE	DATE	DATE
PALO ALTO	VIRGINIA / TEXAS	0100	JULY 1972	1 or 2	5-17	0700	JULY 1972

DRILL RIG	CME-45	HOLE ELEVATION	1695	LOCATED BY	LAR	LOGGED BY	LAR
GROUNDWATER DEPTH (Gauge reading)		HOLE DIAMETER	6 INCHES	DATE DRILLED	7/27-28/72	DATE DRILLED	7/27-28/72
EL. (feet)	CLASS.	DESCRIPTION FIELD IDENTIFICATION	SAMPLE NUMBER	HOLE	RETURNS	HOLE	1695
(0)		0-65' 5'		Hole cased with 6"		D-6	D
(5)		DAM ENBANKMENT MATERIALS: GRAVEL: Silty; coal processing waste. Mostly red, dk. gray silicates and siltone with conk fragments and fine to coarse sands varying from 20-50%; sands are carbonaceous.		AH	-	All	N=6
(10)					-	-	
(15)	GN				-	-	
(20)					-	-	
(25)					-	-	
7/27 (30)					-	-	
7/28					-	-	
(35)					-	-	
(40)	GN				-	-	
(45)					-	-	
(50)					-	-	
WA. WALTER & ASSOCIATES	COAL REFUSE DAM FAILURE Saunders, W., Va. Date Rec'd. - July 1972 Page No. - 1 or 2	Drill Information Date - 0700 Stratigraphic Section - 1 or 2	Spill Information Date - 0700 Stratigraphic Section - 1 or 2	HOLE NO. S-18	SOIL CORROSION SAUNDERS, W., VA. Project No. Date - JULY 1972 Page No. - 1 or 2	Drill Information Date - 0700 Stratigraphic Section - 1 or 2	HOLE NO. S-18

DRILL RIG	CME-45	HOLE ELEVATION	1695	LOCATED BY	LAR	LOGGED BY	LAR
GROUNDWATER DEPTH (Gauge reading)		HOLE DIAMETER	6 INCHES	DATE DRILLED	7/27-28/72	DATE DRILLED	7/27-28/72
EL. (feet)	CLASS.	DESCRIPTION FIELD IDENTIFICATION	SAMPLE NUMBER	HOLE	RETURNS	HOLE	1695
(0)		0-65' 5'		Hole cased with 6"		D-6	D
(5)		DAM ENBANKMENT MATERIALS: (Continued)			-	All	-
(10)		Becomes clayey @ 50'			-	-	
(15)					-	-	
(20)					-	-	
(25)					-	-	
7/27 (30)					-	-	
7/28					-	-	
(35)					-	-	
(40)	GN				-	-	
(45)					-	-	
(50)					-	-	
WA. WALTER & ASSOCIATES	COAL REFUSE DAM FAILURE Saunders, W., Va. Date Rec'd. - July 1972 Page No. - 1 or 2	Drill Information Date - 0700 Stratigraphic Section - 1 or 2	Spill Information Date - 0700 Stratigraphic Section - 1 or 2	HOLE NO. S-18	SOIL CORROSION SAUNDERS, W., VA. Project No. Date - JULY 1972 Page No. - 1 or 2	Drill Information Date - 0700 Stratigraphic Section - 1 or 2	HOLE NO. S-18

DRILL RIG ACER AD-2		HOLE ELEVATION	1638	LOCATED BY	GJA
GROUNDRIG DRILL AD-2 (8 ft.)		HOLE DIAMETER	4 INCHES	DATE DRILLED	7/25/72-7/26/72
ELEVATION (feet)	CLASS.	GPW SP	FIELD DESCRIPTION	SAMPLE NUMBER	REMARKS
(0)					Drilling easy
(5)			Surface material is coarse silty sand containing gravel and cobbles of gray shale and scattered buff-colored sandstones and coal. Gravel and SP approximately equal in amount.	SA	
(10)					
(15)			Pebby to gravelly dark gray, medium to coarse grained silty, only sand, lenses of pebbles and gravel up to several (?) feet thick contain dark gray shale and coal fragments, plasticity of sand is low. Consistency is given by blow counts. The sand is very moist to wet.	D-1	N=17
(20)				SA	D-1 is dark gray, coarse SP with about 10% pebbles.
(25)				D-2	N=9
(30)				-	1/3/4
(35)				SA	-
(40)				D-3	N=16
(45)				-	5/7/9
(50)				D-4	N=18
				-	D-4 Few pebbles - mainly SP
				D-5	N=36
				-	1/3/16/20
				D-6	N=10
				-	D-6 very pebbly.
				SA	
(Total 2 segments)					
COM. REFUSE DAM FAILURE Soundings, M.		SOIL EXPLORATION GRILL HOLE LOG		HOLE NO	
PAO KAO - KAREN BACH		ASSESSOR'S LOG		S-19	
07/26		07/26		JULY 1972	
7/25		07/26		1	
(0)		07/26		S-19	
WA WAHLER & ASSOCIATES					

DRILL RIG NUMBER AD-2		ROCK BOTTOM WATER DEPTH (8 FEET)	HOLE ELEVATION 1688	LOGGED BY GJA	DATE DRILLED 7/26/72
ELEVATION (feet)	CLASS	DESCRIPTION FLOOR IDENTIFICATION	SAMPLE NUMBER	WEIGHT	REMARKS
(50)	SM	POOL, 2' STENITE. (Confined)	D-7	D 1/2/2	N=4
(55)		Thinly interbedded, silty, medium to coarse-grained, dk. gray to black, coaly poorly sorted sand. Some fine grain- ed sand also present with occasional clayey silt layers with moderate plasticity. Very moist to wet. Consistency given by blow counts.	-	SA	-
(60)	SG6 M.		D-8	D 2/2/3	N=5
(65)			-	SA	Small pebbles scattered in SP
(70)		BEDROCK-KAMMIA SERIES Tan sandstone.	D-9	D 1/1/2	N=3
(75)		HOLE TERMINATED @ 70 FEET.	-	SA	D-9 clayey silt and black sand
		Augered to 68 feet - drilling very hard. Continued to 70 feet and met refusal. Hole terminated.			
WA WALTER & ASSOCIATES		COM. REFUSE DAN FAILURE Saville, Va., Va.	SOIL EXPLORATION DRILL HOLE LOG	TESTING NO.	HOLE NO.
		WELL SITE • STOKE BRICK & TILE	07300	JULY 1972	S-19

DRILL RIG ACKER AD-2 HOLE ELEVATION 176.3 LOGGED BY GJA
 GROUNDWATER DEPTH HOLE DIAMETER 6 INCHES DATE DRILLED 7/22-7/26/72

ELEVATION (top/btm)	CLASS.	DESCRIPTION	FIELD IDENTIFICATION	SAMPLE NUMBER	WEIGHT	REMARKS
(0)	Gt6	ENHANCEMENT MATERIALS:				Pitcher Barrel Hole
	Sp	Surface material is coarse loose, permeable, poorly- sorted sand and gravel. Sand exceeds gravel.		-	AH	
(5)			PB-1		PD	
7/27		The sand is medium to coarse. Grained, dark gray, craggy, and angular.	PB-2		PD	2.0/2.5
7/28		The gravel is 1" to greater than 3" in diameter. Numerous cobble exceed 12". The mater- ial is generally platy, dark gray shale with minor light- gray shale, coal, and buff- colored sandstone fragments.	PB-3		PD	1.8/2.5
(10)			PB-4		PD	1.8/2.5
7/28					PD	1.9/2.5
(15)		The embankment is essential- ly to slightly moist.				HOLE TERMINATED
		HOLE TERMINATED @ 14 FEET.				
			(20)			

W.A. WHITNER
& ASSOCIATES

COAL REFUSE DAH FAILURE Saunders, W. Va.	SOIL EXPLORATION DATE	DRILL HOLE NO.	HOLE NO.
PAO 810 - Report Sheet - 2011	07/00	July 1972	S-20

DRILL #1	CME-45	HOLE ELEVATION	1700	LOGGED BY	LAR	LOGGED	LAR
		GROUNDWATER DEPTH	6 INCHES	DATE DRILLED	7/27/72		
ELEVATION (feet)	CLASS	DESCRIPTION FIELD IDENTIFICATION	SAMPLE NUMBER	#001	REMARKS		
(0)		0-50' ENRICHMENT FILL; Bam enrichment materials made up of coal processing waste. Mostly sandy gravels of medium dk. Gray silstones and shale; fine to coarse; angular with coal and sand- stone fragments; 30% fine to coarse grained silty sand.	All		Hole cased with 6" hollow stem auger.		
(5)							
(10)							
(15)							
(20)							
(25)							
(30)							
(35)							
(40)							
(45)							
(50)							

DRILL RIG	CME-45	GROUNDRIGE DEPTH	6 INCHES	HOLE ELEVATION	1701	LOGGED BY	LAR
				DATE DRILLED	7/27/72		
ELEVATION (feet)	CLASS	DESCRIPTION FIELD IDENTIFICATION	SAMPLE NUMBER	#001	REMARKS		
(30)		50'-66.5 SM RESERVOIR SEDIMENT: SAND: SILTY; fine grained; grayish black; carbonaceous; quick dilatancy in fines.	All	D-3A D-3B	N=0 N=1 N=2 Drills easier after 50'; D-4A D-4B	D D D D	N=0 N=1 N=2
(35)							
(40)							
(45)							
(50)							

DRILL RIG CRH-45	GROUNDWATER DEPTH Gauge reading 40.5 ft.	HOLE ELEVATION 1701	LOGGED BY IAR
(ft.)	(ft.)	(ft.)	DATE DRILLED 7/31/72
ELEVATION (Depth)	CLASS. FIELD IDENTIFICATION	SAMPLE NUMBER	NOTES
(0)	0-40' DAN ENHANCEMENT MATERIALS; GRAVEL: SILTY; COAL PROCESSING WASTES; mostly fine to coarse grained med. dk. gray silts and shale fragments; 20-30% sand and silty fines.	-	Hole cased with 6"
(5)	CN	-	hollow stem auger.
(10)	-	-	All
(15)	-	-	-
(20)	-	-	-
(25)	-	-	-
(30)	-	D-1	4/7/74 N=7
(35)	-	-	All
(40)	-	D-2	3/4/74 N=8
(45)	-	-	All
(50)	-	D-3	3/4/75 N=9
	-	-	All Contact appears to be at 40'
	-	D-4A	7/1/74 N=2
	-	H-2B	Hole terminated @ 41.5' Casing removed.
			HOLE TERMINATED @ 41.5 FEET.
WA WHITR 8 ASSOCIATES	COAL REFUSE DAY FAILURE Saunders, Va., PROJECT NUMBER - 1011	SOIL EXPLORATION DRILL HOLE LOG 0700 JULY 22 1972	HOLE NO. S-22

UNIFIED SOIL CLASSIFICATION SYSTEM (ASTM D-2487)																									
MAJOR DIVISIONS				GROUP SYMBOLS	TYPICAL NAMES																				
COARSE GRAINED SOILS MORE THAN 50% RETAINED ON NO. 200 SIEVE*	50% OR MORE OF COARSE FRACTION RETAINED ON NO. 4 SIEVE	50% OR MORE OF COARSE FRACTION RETAINED ON NO. 4 SIEVE	GRAVELS	GW	WELL-GRADED GRAVELS AND GRAVEL-SAND MIXTURES, LITTLE OR NO FINES.																				
				GP	POORLY GRADED GRAVELS AND GRAVEL-SAND MIXTURES, LITTLE OR NO FINES.																				
				GM	SILTY GRAVELS, GRAVEL-SAND-SILT MIXTURES.																				
				GC	CLAYEY GRAVELS, GRAVEL-SAND-CLAY MIXTURES.																				
				SW	WELL-GRADED SANDS AND GRAVELLY SANDS, LITTLE OR NO FINES.																				
	50% OR MORE PASSES NO. 200 SIEVE	50% OR MORE OF COARSE FRACTION PASSES NO. 4 SIEVE	SANDS	SP	POORLY GRADED SANDS AND GRAVELLY SANDS, LITTLE OR NO FINES.																				
				SM	SILTY SANDS, SAND-SILT MIXTURES.																				
				SC	CLAYEY SANDS, SAND-CLAY MIXTURES.																				
				ML	INORGANIC SILTS, VERY FINE SANDS, ROCK FLOUR, SILTY OR CLAYEY FINE SANDS.																				
				CL	INORGANIC CLAYS OF LOW TO MEDIUM PLASTICITY, GRAVELLY CLAYS, SANDY CLAYS, SILTY CLAYS, LEAN CLAYS.																				
FINE GRAINED SOILS 50% OR MORE PASSES NO. 200 SIEVE	SILTS & CLAYS	LIQUID LIMIT 50% OR LESS	SILTS & CLAYS	OL	ORGANIC SILTS AND ORGANIC SILTY CLAYS OF LOW PLASTICITY.																				
				MH	INORGANIC SILTS, MICACEOUS OR DIATOMACEOUS FINE SANDS OR SILTS, ELASTIC SILTS.																				
				CH	INORGANIC CLAYS OF HIGH PLASTICITY, FAT CLAYS.																				
				OH	ORGANIC CLAYS OF MEDIUM TO HIGH PLASTICITY.																				
				PT	PEAT, MUCK AND OTHER HIGHLY ORGANIC SOILS.																				
	LIQUID LIMIT GREATER THAN 50%	HIGHLY ORGANIC SOILS																							
*BASED ON THE MATERIAL PASSING THE 3-IN. (75-MM) SIEVE.																									
DEFINITION OF TERMS																									
GRAIN SIZES																									
U.S. STANDARD SERIES SIEVES																									
200		50	16	4	3/4"	3"	12"	CLEAR SQUARE SIEVE OPENINGS																	
SILTS & CLAYS DISTIN-		SAND			GRAVEL		COBBLES		BOULDERS																
GUISHED ON BASIS OF		FINE	MEDIUM	COARS	FINE	COARSE																			
MOISTURE CONDITION (INCREASING MOISTURE →)																									
DRY	SLIGHTLY DAMP	DAMP	MOIST	VERY MOIST	WET (SATURATED)	SANDS & GRAVELS																			
(CPL)					(LL)	RELATIVE DENSITY	BLOWS/FOOT*																		
SAMPLE NUMBER COLUMN	MODE COLUMN	REMARKS COLUMN																							
TYPE OF SAMPLE CON-	METHOD OF ADVANCING HOLE: / DRILL	NUMBER OF BLOWS REQUIRED TO DRIVE SAMPLER IS SHOWN FOR EACH 0.5' OF PENETRATION AS FOLLOWS:																							
TAINER:	HOLLOW STEM AUGER..... AH	17/22/29 FOR A TOTAL OF 1.5 FEET; N = 51 BLOW COUNTS SUMMED FOR LAST 1.0 FOOT.																							
BAG	J																								
JAR	SA																								
SHELBY TUBE	RD																								
LINER (TUBE)	CT																								
WRAPPED CORE	D	RECOVERY RATIO INDICATED BY A FRACTION:																							
BOX	PB	1.2 = FOOTAGE RECOVERED																							
PITCHER TUBE	C	1.5 = FOOTAGE SAMPLED																							
PISTON	P	TERMINATED HOLE: SUFFICIENT INFORMATION OBTAINED.																							
CLAYS & SILTS																									
CONSISTENCY		BLOWS/FOOT*		STRENGTH**																					
VERY SOFT	0-2	0-1/2																							
SOFT	2-4	1/2-1																							
FIRM	4-8	1-1 1/2																							
STIFF	8-16	1 1/2-2																							
VERY STIFF	16-32	2-4																							
HARD	OVER 32	OVER 4																							
* NUMBER OF BLOWS OF 140 POUND HAMMER FALLING 30 INCHES TO DRIVE A 2-INCH Ø-Ø. (1-3/8 INCH I-Ø.) SPLIT SPOON (STANDARD PENETROMETER).																									
** UNCONFINED COMPRESSIVE STRENGTH IN TONS/SQ. FT.																									
PALO ALTO - NEWPORT BEACH - CALIF.					KEY FOR EXPLORATION LOGS																				

TABLE A-4

FIELD PERMEAMETER TEST RESULTS

TEST HOLE NO.: FP-1A

LOCATION: Left abutment remnant, Dam No. 3.

HOLE DIAMETER: 4"

TESTED INTERVAL: 10.0 to 20.0 feet

DATE OF TEST: May 12, 1972

CLOCK (hrs)	TIME ACCUM. (min)	WATER VOLUME ACCUM. FLOW (gal)	WATER TEMPERATURE (degrees C)
955	0	0	-
1115	80	48.0	15
1133	-	-	-
1255	168	92.8	17
1305	-	-	-
1405	228	126.8	19
1421	-	-	-
1521	288	161.6	18
1536	-	-	-
1636	348	198.6	17
1648	-	-	-
1718	378	216.0	16

Coefficient of permeability from nomograph:

$$K_{20^{\circ}\text{C}} = 250 \text{ ft/yr or } 2.42 \times 10^{-4} \text{ cm/sec}$$

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FIELD PERMEAMETER TEST RESULTS

TEST HOLE NO.: FP-2A

LOCATION: Left abutment remnant, Dam No. 3.

HOLE DIAMETER: 6"

TESTED INTERVAL: Not run

DATE OF TEST: May 15, 1972

Notes: Hole was set up drilled to 40 feet, gravel @ 20-40, casing @ 0-20. It was abandoned when initial results indicated the interval gravelled was too large for practical testing of a 6" hole. The hole took 6.1 gpm for approximately 1 hr. with the water level stabilized at the top of the gravel. The water did not rise into the casing.

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FIELD PERMEAMETER TEST RESULTS

TEST HOLE NO.: FP-3A
LOCATION: Left abutment, Dam No. 3.
HOLE DIAMETER: 6"
TESTED INTERVAL: 3.6 to 10.5 feet
DATE OF TEST: May 24-25, 1972

The results for two consecutive days of testing were inconsistent. Hole was abandoned and data not processed.

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FIELD PERMEAMETER TEST RESULTS

TEST HOLE NO.: FP-4A

LOCATION: Dam No. 3, left abutment remnant.

HOLE DIAMETER: 4"

TESTED INTERVAL: 19.6 to 25.0 feet

DATE OF TEST: May 31, 1972

Remarks: Could not establish a water level in the casing. Hole took 4 gal/minute from the supply hose for approximately 1/2 hour before efforts to establish water level in casing were abandoned.

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FIELD PERMEAMETER TEST RESULTS

TEST HOLE NO.: FP-5A

LOCATION: Left abutment remnant, Dam No. 3.

HOLE DIAMETER: 4"

TESTED INTERVAL: 30.0 to 35.5 feet

DATE OF TEST: June 2, 1972

Remarks: Could not establish and maintain a water level just above the gravel top at 30.0 feet depth. Weight of float chain too high; when additional counterweights were added to the valve, it would not properly function while carrying the extra weight.
Hole abandoned in favor of additional shallow holes.

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FIELD PERMEAMETER TEST RESULTS

TEST HOLE NO.: FP-6A

LOCATION: Left abutment remnant, Dam No. 3.

HOLE DIAMETER: 4"

TESTED INTERVAL: 10.0 to 15.0 feet

DATE OF TEST: July 17, 1972

Remarks: 900 gallons of water placed in hole in 45 minutes.
Water level maintained at 6" above top of gravel during pouring - no
sign of stabilizing.

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FIELD PERMEAMETER TEST RESULTS

TEST HOLE NO.: FP-7A
LOCATION: Left abutment remnant, Dam No. 3.
HOLE DIAMETER: 4"
TESTED INTERVAL: 7.5 to 15.0 feet
DATE OF TEST: July 18, 1972

CLOCK (hrs)	TIME ACCUM. (min)	WATER VOLUME ACCUM. FLOW (gal)	WATER TEMPERATURE (degrees C)
902	0	0	25
917	15	8.0	25
932	30	17.0	25
947	45	26.5	25
1002	60	35.0	25
1037	95	52.5	26
1107	125	70.0	27
1211	189	105.5	28
1333	271	141.0	29
1520	378	169.0	30
1627	445	196.0	29

Coefficient of permeability from nomograph:

$$K_{200\text{ C}} = 225 \text{ ft/yr} \text{ or } 2.17 \times 10^{-4} \text{ cm/sec}$$

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FIELD PERMEAMETER TEST RESULTS

TEST HOLE NO.: FP-7A (continued)
 LOCATION: Left abutment remnant, Dam No. 3.
 HOLE DIAMETER: 4"
 TESTED INTERVAL: 7.5 to 15.0 feet
 DATE OF TEST: July 20, 1972

CLOCK (hrs)	TIME ACCUM. (min)	WATER VOLUME ACCUM. FLOW (gal)	WATER TEMPERATURE (degrees C)
842	0	0	24
942	60	19.5	25
1042	120	38.5	26
1148	186	57.0	26
1300	258	79.0	29
1406	324	97.0	27
1506	384	115.0	29
1613	451	132.5	29
1645	483	142.0	29

Coefficient of permeability from nomograph:

$$K_{20^\circ \text{ C}} = 185 \text{ ft/yr or } 1.79 \times 10^{-4} \text{ cm/sec}$$

FIELD PERMEAMETER TEST RESULTS

TEST HOLE NO.: FP-8A
 LOCATION: Left abutment remnant, Dam No. 3.
 HOLE DIAMETER: 4"
 TESTED INTERVAL: 9.1 to 15.2 feet
 DATE OF TEST: July 21, 1972

CLOCK (hrs)	TIME	ACCUM. (min)	WATER VOLUME ACCUM. FLOW (gal)	WATER TEMPERATURE
				(degrees C)
1055		0	0	28
1110		15	3.5	28
1125		30	5.5	28
1140		45	8.0	28
1155		60	10.5	29
1255		120	20.0	30
1355		180	30.5	30
1455		240	40.5	31

Coefficient of permeability from nomograph:

$$K_{20^\circ \text{ C}} = 140 \text{ ft/yr or } 1.35 \times 10^{-4} \text{ cm/sec}$$

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FIELD PERMEAMETER TEST RESULTS

TEST HOLE NO.: FP-9A
LOCATION: Left abutment remnant, Dam No. 3.
HOLE DIAMETER: 4"
TESTED INTERVAL: 1.2 to 4.9 feet
DATE OF TEST: July 26-27, 1972

Remarks: Water seep observed in hillside 13' from hole. Elevation of seep is 2.5' below top of water in hole. Amount of flow was about the same as flow into hole. The test was terminated.

Travel time test: The obvious channel-type flow above negated any attempt to run the usual test, but provided an opportunity for a crude travel time test performed on July 27, 1972. Flow to the seep was re-established and a head of 2.45 feet was maintained. Red dye was added to the test hole and the seep was observed for its appearance. Water temperature was 70°F; horizontal distance from the hole to the seep was 13 feet. The first traces of red dye appeared at the seep 14.5 minutes after it was put in the hole; a stronger color appeared 16.0 minutes after the dye was put in the hole, and very strong color appeared at the seep 17.0 minutes after the dye was put in the hole.

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FIELD PERMEAMETER TEST RESULTS

TEST HOLE NO.: FP-10A
LOCATION: Left abutment remnant, Dam No. 3.
HOLE DIAMETER: 4"
TESTED INTERVAL: 0.9 to 4.5 feet
DATE OF TEST: July 25 and 26, 1972

CLOCK (hrs)	TIME ACCUM. (min)	WATER VOLUME ACCUM. FLOW (gal)	WATER TEMPERATURE (degrees C)
926	0	0	25
1026	60	1.4	25
1126	120	2.5	26
1226	180	3.7	27
1326	240	5.3	27
1426	300	6.6	27
1526	360	8.0	28
1626	420	9.4	28
800 (7/26)	1354	29.7	21

Coefficient of permeability from nomograph:

$$K_{20^{\circ}\text{C}} = 48 \text{ ft/yr or } 4.64 \times 10^{-5} \text{ cm/sec}$$

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FIELD PERMEAMETER TEST RESULTS

TEST HOLE NO.: FP-11A
 LOCATION: Left abutment remnant, Dam No. 3.
 HOLE DIAMETER: 4"
 TESTED INTERVAL: 0.7 to 4.0 feet
 DATE OF TEST: July 24 and 25, 1972

	CLOCK (hrs)	TIME ACCUM. (min)	WATER VOLUME ACCUM. FLOW (gal)	WATER TEMPERATURE (degrees C)
	855	0	0	27
	955	60	1.4	27
	1055	120	2.6	27
	1155	180	3.5	28
	1255	240	4.7	29
	1355	300	6.1	30
	1455	360	7.4	30
	1555	420	8.7	31
	1655	480	10.1	32
	805 (7/25)	1390	30.4	25

Coefficient of permeability from nomograph:

$$K_{20^\circ \text{ C}} = 50 \text{ ft/yr} \text{ or } 4.83 \times 10^{-5} \text{ cm/sec}$$

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FIELD PERMEAMETER TEST RESULTS

TEST HOLE NO.: FP-12A

LOCATION: Left abutment remnant, Dam No. 3.

HOLE DIAMETER: 4"

TESTED INTERVAL: 3.8 to 6.8 feet

DATE OF TEST: July 27, 1972

Remarks: Water drained from hole as fast as barrel would empty for 324 gallons.
Could not establish a water level in the casing.

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FIELD PERMEAMETER TEST RESULTS

TEST HOLE NO.: FP-13A
 LOCATION: Left abutment remnant, Dam No. 3.
 HOLE DIAMETER: 4"
 TESTED INTERVAL: 1.3 to 4.9 feet
 DATE OF TEST: July 28, 1972

CLOCK (hrs)	TIME ACCUM. (min)	WATER VOLUME ACCUM. FLOW (gal)	WATER TEMPERATURE
			(degrees C)
1145	0	0	21
1215	30	4.2	21
1215	60	8.1	21
1315	90	12.0	22
1345	120	15.8	22
1415	150	19.5	22
1445	180	23.2	22
1515	210	26.9	22
1545	240	30.6	22
1615	270	34.3	22
1645	300	38.0	22

COEFFICIENT OF PERMEABILITY FROM NOMOGRAPH:

$$K_{20^\circ C} = 295 \text{ ft/yr or } 2.85 \times 10^{-4} \text{ cm/sec}$$

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FIELD PERMEAMETER TEST RESULTS

TEST HOLE NO.: FP-14 A
LOCATION: Left abutment remnant, Dam No. 3.
HOLE DIAMETER: 4"
TESTED INTERVAL: 0.7 to 4.2 feet
DATE OF TEST: July 31, 1972

CLOCK (hrs)	TIME ACCUM. (min)	WATER VOLUME ACCUM. FLOW (gal)	WATER TEMPERATURE (degrees C)
903	0	0	19
918	15	2.4	19
1003	60	9.3	19
1033	90	14.2	19
1133	120	24.1	19
1233	180	34.1	20
1340	247	44.2	20
1440	307	54.2	20
1540	367	64.1	21

Coefficient of permeability from nomograph:
 $K_{20}^o = 430 \text{ ft/yr or } 4.15 \times 10^{-4} \text{ cm/sec}$

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APPENDIX B

LABORATORY INVESTIGATION

A. GENERAL.

This Appendix includes a discussion of test procedures and actual test results for the laboratory investigation performed by W. A. Wahler and Associates on the various embankment and foundation materials for use in the engineering evaluation of the failure of the coal waste dams near Saunders, West Virginia.

The purpose of this investigation was to study the soil engineering characteristics of the various materials in order to determine the in-place soil engineering parameters necessary for use in these analyses. To this end, the laboratory testing was conducted employing currently accepted test procedures of the American Society of Testing and Materials (ASTM).

Various bulk and undisturbed samples used in the laboratory investigation were obtained during the course of the field investigation as discussed in Appendix A of this report. Then, after reviewing the drill hole logs, various undisturbed foundation and embankment samples, contained in 3-inch diameter Shelby tubes, were selected to remain in Logan, West Virginia for testing in our portable laboratory. The remainder of the undisturbed samples, including all 4-inch diameter Shelby-type tubes and the large (50-lb.) bulk samples, were transported to our laboratory in Palo Alto for more extensive examination and testing.

Laboratory testing completed in Logan, West Virginia consisted of 22 triaxial tests, 13 water contents and dry densities, and 8 permeability determinations in conjunction with triaxial tests. All other tests

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reported herein were completed at our main laboratory in Palo Alto, California. All of the various laboratory tests performed during the course of this investigation are described below. Identification of each sample is by hole number and depth or by field density (FD) number if the sample was obtained by means other than rotary drilling. Additionally, a special series of triaxial tests was performed on samples, typical of Dam No. 3 embankment, and materials fabricated in the laboratory. These samples are referenced as Sample A-1.

B. INDEX PROPERTIES TESTING

In the field of soil mechanics and earth dam design, it is advantageous to have a standard method of identifying soils and classifying them into categories or groups that have similar or distinct engineering properties. The most commonly used method at present is the Unified Soils Classification System (USCS) as described by ASTM D2487-69T. The USCS is based on a recognition of the various types and significant distribution of soil constituents, considering individual grain-size, magnitude and type of gradation characteristics, and plasticity of materials.

The index properties tests presented in this report included the determination of natural water content and in-place dry density, specific gravity and absorption, Atterberg Limits and grain-size distribution for both the embankment and foundation materials.

1. Natural Water Content and Dry Density

Natural water content and in-place dry density data were determined in the laboratory on extruded 3-inch diameter Shelby tube samples used for triaxial testing. Moisture content and density data were also determined on additional samples for correlation. Each sample was trimmed

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to obtain a smooth, square face and then accurately measured to obtain volume and wet weight before drying for a period of approximately 48 hours in an oven maintained at a temperature of 110°F. The 110°F temperature, which deviates from the specified 210°F in ASTM, was necessary to prevent spontaneous combustion of the coal waste material and was determined by trial and error methods.

The results of the natural water content and dry density testing are presented on Figure B-1 and also with the individual triaxial results.

2. Grain-Size Distribution

The gradation characteristics of selected samples of embankment and foundation materials were determined in accordance with ASTM designation D422-63 and D1140-54, except as modified below. Representative samples were quartered and/or prepared in accordance with ASTM designation D421-58. The samples were soaked in water until individual soil particles were separated, and then washed on a #200 mesh sieve. That portion of the material retained on the #200 mesh sieve was oven-dried and then mechanically sieved. A hydrometer analysis was performed using a constant temperature hydrometer bath, for those samples with more than approximately 30 percent passing the #200 mesh sieve. Sodium hexametaphosphate was used as a dispersing agent. The grain-size distribution test for samples tested are presented on Figure B-2, sheets 1 through 25.

3. Atterberg Limits

The liquid and plastic limits for selected samples were determined in accordance with ASTM designation D423 and D424. Results of the Atterberg Limits are presented on Figure B-3, sheets 1 through 3. Results of the Atterberg Limits have also been presented on the Gradation and Compaction Sheets and on the triaxial test result sheets, where appropriate, to aid in interpretation of such results.

4. Specific Gravity

Specific Gravity determinations were made primarily on samples used for compaction or triaxial testing in accordance with ASTM designation D854-58. In addition, bulk Specific Gravity determinations were conducted on the Field Density samples containing a substantial amount of plus 3/4-inch size material, using ASTM Method C127. One bulk Specific Gravity was also conducted on the combined sample A-1, used for lab-fabricated 4.0-inch triaxial testing. The specific gravity test results are presented on Figure B-4, sheets 1 and 2, and also on the individual triaxial, gradation and compaction test results.

C. ENGINEERING PROPERTIES TESTING

The engineering properties testing constituted a significant portion of time and budget for the laboratory testing phase of the failure investigation. The engineering properties tests presented in this report include compaction, triaxial shear, and permeability tests.

1. Compaction Tests

Compaction tests were performed to determine the moisture-density relationships of the materials. The tests were performed using a Howard mechanical compactor in accordance with ASTM designation D1557-70, modified to yield a compactive energy of 20,000 foot-pounds per cubic foot ($\text{Ft-lb}/\text{ft}^3$) by reducing the number of layers to 3 and the number of blows per layer of a 10-lb. hammer to 15. For the coarse-grained materials, it was necessary to scalp the total sample on the 3/4-inch sieve prior to performing the compaction tests. Compaction test results, together with gradation characteristics of the materials tested are presented on Figure B-5, sheets 1 through 13.

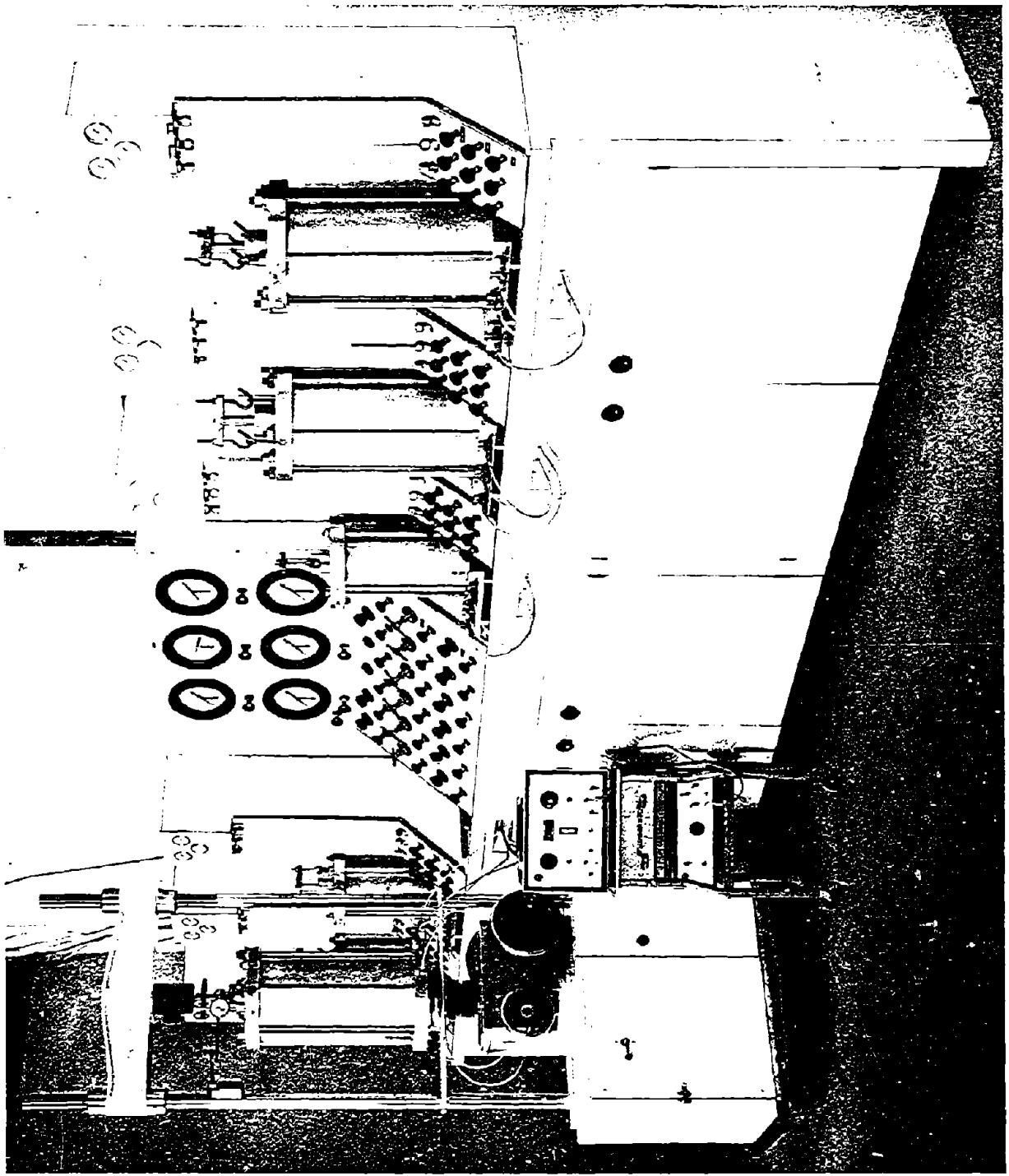
2. Static Triaxial Shear

The triaxial shear testing program was planned to determine the shear strength parameters of both the coarse waste and sludge constituents of the embankment and foundation materials. The program was detailed in scope and consisted of testing undisturbed 3-inch diameter Shelby tube samples and 4.0-inch diameter laboratory-fabricated samples.

Our main laboratory is equipped with a panel of 6 bays, with individual pressure control to each bay, such that the 6 triaxial samples can simultaneously be saturated and/or consolidated at different individual pressures. The portable laboratory trailer contains 3 bays for 3 individual samples. Other than this minor difference, the two laboratories possess the same triaxial testing capabilities. Bleeding air regulators capable of delivering air pressure up to 200 psi are used to control the top, bottom, and chamber lines leading to the triaxial cells. Each saturation bay is also equipped with constant diameter Pyrex sight tubes, each with a cross sectional area of 0.0767 square inches, which connect with the base of the triaxial cell, and thus to the sample. The sight tubes are easily read to the nearest 0.1 inch, which indicates an accuracy of volume change readings of better than 0.01 cubic inch. An overall view of the triaxial saturation bay, triaxial cell and strain control testing machine is shown in Photoplate B-1.

a. Undisturbed Samples - The undisturbed Shelby tube samples selected for testing either in Logan or Palo Alto were extruded using a hydraulically operated ram capable of exerting the minimum force necessary to free the sample from the Shelby tube. With the aid of a special trimming device which completely supported the sample, the possibility of sample disturbance due to handling was significantly reduced. The results of the undisturbed triaxial test results are on Figure B-6, sheets 1 through 15.

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TRIAXIAL SATURATION BAY, STRAIN CONTROLLED 20,000 LB LOADING MACHINE AND STRAIN INDICATOR FOR ELECTRIC READOUT OF LOAD AND PORE PRESSURE. (NOTE THE INDIVIDUAL PRESSURE AND VOLUME CONTROL FOR THE TOP, BOTTOM, AND CHAMBER LINES OF EACH CELL.)

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PHOTOPLATE B-1

b. Fabricated Samples - Due to the large grain size of some of the embankment materials, it was necessary to conduct a series of laboratory-fabricated 4.0-inch diameter triaxial tests. An extensive study was performed to obtain an average gradation, dry density and water content from all of the field and laboratory data. These averages were used as the guide for fabricating samples.

The set-up gradation for the triaxial samples simulated that of the total average gradation except for the exclusion of plus 1-inch material, the weight of which was compensated for by inclusion of 3/4 to 1-inch material so that the percent passing the 3/4-inch sieve was identical to the average total gradation (Figure B-2, sheet 15). This was done so that no more than a 1 to 4 ratio would exist between maximum particle size and diameter of sample.

The sample was then moisture-conditioned to the predetermined average moisture content and allowed to cure for approximately 24 hours. The fabrication of samples was performed in a 4-inch diameter mold with a height-to-diameter ratio of 2.1 to 1, using the rounded end of a 1/2-inch diameter shaft which was routed into the sample until a given weight of soil occupied a known volume. The sample was compacted in five equal layers with care being taken to scarify each compacted surface in order to preclude preferential bonding or laminae developing between layers. These specimens were compacted to the predetermined average dry density obtained as explained previously and were designated Sample A-1. The results of these laboratory fabricated triaxial tests are presented on Figure B-6, sheets 14 and 15. Photographs depicting various stages of the sample fabrication process are shown in Photoplate B-2.

c. Sample Saturation and Consolidation - After fabrication or trimming and initial weight and volume measurements were completed, the samples for triaxial testing were placed in the triaxial cell, encased in a



STAGE 1.—SAMPLE IS FABRICATED BY
KNEADING COMPACTION INTO 2.8"
OR 4.0" DIAMETER MOLD USING FIVE
EQUAL LAYERS.



STAGE 2.—REMOVAL OF MOLD AFTER
COMPLETING SAMPLE FABRICATION.
OVERCOMPACTED ZONES ARE PRE-
VENTED BY SCARIFYING EACH COM-
PACTED LAYER.



STAGE 3.—SAMPLE IS MOUNTED ON
PEDESTAL OF TRIAXIAL CELL. FILTER
STRIPS MAY BE REQUIRED TO SPEED
UP CONSOLIDATION TIME OF IMPER-
VIOUS SOILS.



STAGE 4.—SAMPLE IS ENCASED IN A
RUBBER MEMBRANE AND SECURED TO
BOTTOM PEDESTAL AND TOP CAP
WITH "O" RINGS. DRAINAGE LINES
LEAD FROM TOP AND BOTTOM OF
SAMPLE TO EXTERNAL CELL CONNE-
CTIONS.

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PHOTOPLATE B-2

rubber membrane and sealed to the bottom pedestal and topcap with rubber "O" rings. After securing the triaxial chamber, the cell was filled with water, fitted with a 1-inch diameter stainless steel piston for load application, and transported to the saturation bay. A back pressure of 50 psi was necessary to obtain a sufficient degree of saturation prior to the consolidation phase of the test. In order to determine whether the back pressure applied was causing complete saturation, Skempton's "B" parameter was measured for all samples. A value in excess of 0.95 was considered to represent a fully saturated condition. After achieving complete saturation, the samples were either consolidated isotropically or anisotropically, or failed unconsolidated.

1. I.C.U. Tests - For those samples consolidated isotropically, the chamber pressure was increased to a value in excess of the back pressure by an amount equal to the designated consolidation pressure, the top and bottom drainage lines were simultaneously opened, and the total volume of water expelled from the samples was monitored as a function of time. In some cases, strips of filter paper, placed along the sides of the specimen during set-up, were used to accelerate the consolidation process. Once consolidation was complete, the samples were failed in an undrained condition with pore pressure, axial load and sample strain monitored as described in (d) below. The results for the I.C.U. triaxial shear testing appear on Figure B-6, sheets 1 through 5 and 8 through 14.

2. K_o - Tests - The K_o-anisotropic consolidation was performed in a drained condition using strain control techniques. The K_o-value is an at-rest pressure coefficient defined by the ratio of minor principal effective stress to major principal effective stress. After achieving complete saturation, the samples were consolidated in a drained condition at a sufficiently slow rate of strain to preclude the build-up of pore pressure. During progress of the test, the volume

change was continuously monitored and the chamber pressure increased incrementally as necessary in order to cause the sample volume change to equal the product of the axial deformation times the initial cross sectional area. Once the desired lateral confining pressure (σ_3) was achieved, the top and bottom drainage lines were closed and the sample was failed in an undrained condition. Results for the K_o consolidation and triaxial shear tests appear on Figure B-6, sheet 6 and 15.

3. U.U. Tests - The samples tested under unconsolidated-undrained conditions were not consolidated prior to failure. The samples were failed undrained with pore pressure, axial load and sample strain monitored as described in (d) below. Results for the unconsolidated-undrained triaxial tests appear on Figure B-6, sheet 7.

d. Sample Failure - All triaxial specimens were failed by compression loading at a constant rate of strain while maintaining a constant minor principal stress. The rate of strain selected for sample failure was dependent upon the materials consolidation characteristics. The failure machines used both in Palo Alto and in Logan were geared to fail the undisturbed samples at approximately 4 percent of axial strain per hour. The rate of strain for the taller, fabricated samples varied slightly. The actual rate of strain for each test is presented on each individual data sheet. The axial load and pore pressure readings were obtained during the test at specified axial deformations using a BLH load cell (0-2,000 lbs.) and a Stathom pore pressure transducer (0-200 psi gauge). The adopted failure criterion used for the presentation of the Mohr circle of stress for most triaxial tests was the point of maximum principal effective stress ratio, except for the unconsolidated tests, in which 10 percent strain was used. The point of failure was developed at various strain rates, depending upon material type, method of consolidation and confining pressure.

3. Permeability Tests

Permeability coefficients for selected samples were determined in conjunction with triaxial shear tests by applying a constant head hydraulic gradient to the sample and monitoring the flow of water from bottom to top of sample through the sight tubes. Samples were tested for permeability at initial setup densities or after consolidation. In some cases, the same sample was tested at two or three different densities. Permeability test results are presented on Figure B-7.

a. Special Fabricated Piping Test - An undisturbed Shelby tube of sludge material from Hole 5 at 65 feet was extruded and observed. The coarser SM material in the tube was then separated from the finer ML material (Figure B-2, sheet 6). The coarser material was then compacted into a 4-inch diameter clear lucite tube to the approximate average dry density (51 pcf) of the sludge material. The sample was then saturated by allowing it free access to water at the bottom of the sample. A slight head was then established so that water would flow from bottom to top. When the applied gradient (head loss divided by sample length) exceeded 0.25, the sample began to rise in the tube and the migration of material, through a system of branching "pipes," was clearly visible. The "pipes" continued to enlarge and the moving material had the appearance of boiling.. The condition of piping described above physically substantiated the theoretical critical gradient of 0.26 as discussed in Chapter VII of this report.

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FIGURE B-1
SUMMARY
OF
IN-SITU WATER CONTENT AND DRY UNIT WEIGHTS

HOLE NO	SAMPLE NO	DEPTH (ft)	MATERIAL TYPE	WATER CONTENT (%)	DRY WEIGHT (pcf)
2	S-4	23.0-25.0	EMBANKMENT, DAM NO. 3	3.3	80.3
2	S-4	23.0-25.0	EMBANKMENT, DAM NO. 3	4.2	80.5
2	S-4	23.0-25.0	EMBANKMENT, DAM NO. 3	5.9	77.4
3	S-6	25.0-27.0	EMBANKMENT, DAM NO. 3	9.7	75.9
4	S-2	10.0-12.0	EMBANKMENT, DAM NO. 2	8.7	83.7
4	S-6	30.0-32.0	EMBANKMENT, DAM NO. 2	8.2	106.5
4	S-7	35.0-37.0	EMBANKMENT, DAM NO. 2	10.3	84.2
4	S-7	35.0-37.0	EMBANKMENT, DAM NO. 2	8.5	90.7
4	S-12	68.0-70.0	FOUNDATION, POOL 1 SLUDGE	42.9	49.0
4	S-12	68.0-70.0	FOUNDATION, POOL 1 SLUDGE	26.4	47.7
4	S-12	68.0-70.0	FOUNDATION, POOL 1 SLUDGE	64.8	47.8
4	S-13	70.0-72.0	FOUNDATION, POOL 1 SLUDGE	49.2	51.1
4	S-13	70.0-72.0	FOUNDATION, POOL 1 SLUDGE	50.1	49.8
4	S-13	70.0-72.0	FOUNDATION, POOL 1 SLUDGE	38.2	58.7
4	PST-5	75.0-77.0	FOUNDATION, POOL 1 SLUDGE	38.3	55.6
4	PST-5	75.0-77.0	FOUNDATION, POOL 1 SLUDGE	44.9	62.4
5	S-5	65.0-67.0	FOUNDATION, POOL 1 SLUDGE	57.1	-----
5	S-5	65.0-67.0	FOUNDATION, POOL 1 SLUDGE	45.3	-----
5	S-7	75.0-77.0	FOUNDATION, POOL 1 SLUDGE	41.6	72.0
7	S-1	10.0-12.0	EMBANKMENT, DAM NO. 3	11.6	86.7
7	S-2	20.0-22.0	EMBANKMENT, DAM NO. 3	14.9	67.7
7	S-2	20.0-22.0	EMBANKMENT, DAM NO. 3	14.5	85.9
7	S-2	20.0-22.0	EMBANKMENT, DAM NO. 3	14.0	90.3
7	S-3	30.0-32.0	FOUNDATION, POOL 2 SLUDGE	47.6	48.3
7	S-4	40.0-42.0	FOUNDATION, POOL 2 SLUDGE	46.5	48.6
7	S-5	50.0-52.0	FOUNDATION, POOL 2 SLUDGE	30.7	60.8
7	S-5	50.0-52.0	FOUNDATION, POOL 2 SLUDGE	35.2	58.9
7	PST-1	52.0-53.6	FOUNDATION, POOL 2 SLUDGE	37.3	56.6
7	PST-1	52.0-53.6	FOUNDATION, POOL 2 SLUDGE	40.8	53.3
7	S-7	71.1-73.5	FOUNDATION, POOL 1 SLUDGE	38.1	65.0
7	S-7	71.1-73.5	FOUNDATION, POOL 1 SLUDGE	46.8	48.5
8	S-2	20.0-22.0	EMBANKMENT, DAM NO. 3	13.6	82.0
8	PST-2	55.0-57.0	FOUNDATION, POOL 2 SLUDGE	41.2	49.7
9	S-2	20.0-22.0	EMBANKMENT, DAM NO. 3	9.4	84.6
9	S-4	35.0-37.0	FOUNDATION, POOL 2 SLUDGE	38.9	54.7
9	SS-1	45.0-48.0	FOUNDATION, POOL 2 SLUDGE	41.9	49.6
9	SS-2A	55.0-57.0	FOUNDATION, POOL 2 SLUDGE	42.5	54.1
9	SS-2A	55.0-57.0	FOUNDATION, POOL 2 SLUDGE	67.7	48.5
9	SS-2A	55.0-57.0	FOUNDATION, POOL 2 SLUDGE	38.7	47.4
9	SS-2B	57.0-59.0	FOUNDATION, POOL 2 SLUDGE	40.6	55.8
9	SS-2B	57.0-59.0	FOUNDATION, POOL 2 SLUDGE	41.2	52.2

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FIGURE B-1
Sheet 1 of 2

FIGURE B-1 -- CONTINUED
**SUMMARY
OF
IN-SITU WATER CONTENT AND DRY UNIT WEIGHTS**

HOLE NO.	SAMPLE NO.	DEPTH (ft)	MATERIAL TYPE	WATER CONTENT (%)	DRY WEIGHT (pcf)
10	S-9	60.7-62.7	MIXED EMBANKMENT AND SLUDGE	18.4	73.8
10	S-9	60.7-62.7	MIXED EMBANKMENT AND SLUDGE	15.9	85.0
10	S-9	60.7-62.7	MIXED EMBANKMENT AND SLUDGE	10.7	106.0
10	S-13	77.0-78.5	FOUNDATION, POOL 1 SLUDGE	35.3	67.5
10	S-14	80.0-81.6	FOUNDATION, POOL 1 SLUDGE	34.7	54.5
10	S-14	80.0-81.6	FOUNDATION, POOL 1 SLUDGE	42.9	59.6
11	S-1	10.0-12.0	DISTURBED EMBANKMENT	13.8	77.8
11	PST-1	35.0-37.0	EMBANKMENT, DAM NO. 3	12.0	103.4
11	PST-1	35.0-37.0	EMBANKMENT, DAM NO. 3	10.5	104.6
11	PST-1	35.0-37.0	EMBANKMENT, DAM NO. 3	17.6	90.5
11	SS-3A	85.0-87.0	FOUNDATION, POOL 1 SLUDGE	37.3	58.5
11	SS-3A	85.0-87.0	FOUNDATION, POOL 1 SLUDGE	45.0	48.4
11	SS-3A	85.0-87.0	FOUNDATION, POOL 1 SLUDGE	32.0	65.2
11	SS-3B	87.0-89.0	FOUNDATION, POOL 1 SLUDGE	46.1	59.0
13	S-1	10.0-12.0	GOB PILE, COARSE COAL WASTE	9.3	84.2
13	S-3	30.0-32.0	GOB PILE, COARSE COAL WASTE	11.1	91.8
13	S-3	30.0-32.0	GOB PILE, COARSE COAL WASTE	10.9	87.0
13	S-4	40.0-42.0	GOB PILE, COARSE COAL WASTE	9.9	110.2
13	S-4	40.0-42.0	GOB PILE, COARSE COAL WASTE	10.7	87.7
13	S-5	50.0-52.0	GOB PILE, COARSE COAL WASTE	15.8	74.4
15	S-1	36.0-38.0	FOUNDATION, POOL 1 SLUDGE	55.3	49.5
15	S-2	40.0-42.0	RED DOG, BURNED COAL WASTE	18.5	86.5
15	S-2	40.0-42.0	RED DOG, BURNED COAL WASTE	19.2	91.5
20	PB-1	4.7-6.5	EMBANKMENT, DAM NO. 3	9.7	82.4
20	PB-1	4.7-6.5	EMBANKMENT, DAM NO. 3	12.2	68.8
20	PB-4	11.5-14.0	EMBANKMENT, DAM NO. 3	18.3	83.1
20	PB-4	11.5-14.0	EMBANKMENT, DAM NO. 3	10.4	84.8
FP-9A	S-1	1.9-3.9	EMBANKMENT, DAM NO. 3	9.0	98.9
FP-9A	S-1	1.9-3.9	EMBANKMENT, DAM NO. 3	7.9	87.7
FP-10A	S-2	3.5-4.5	EMBANKMENT, DAM NO. 3	8.6	93.9
FP-11A	S-1	1.2-3.1	EMBANKMENT, DAM NO. 3	8.4	101.4
FP-11A	S-1	1.2-3.1	EMBANKMENT, DAM NO. 3	8.1	94.3
FP-12A	S-1	4.8-6.8	EMBANKMENT, DAM NO. 3	10.1	87.6
FP-14A	S-2	3.5-4.5	EMBANKMENT, DAM NO. 3	6.6	105.3

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FIGURE B-1
Sheet 2 of 2

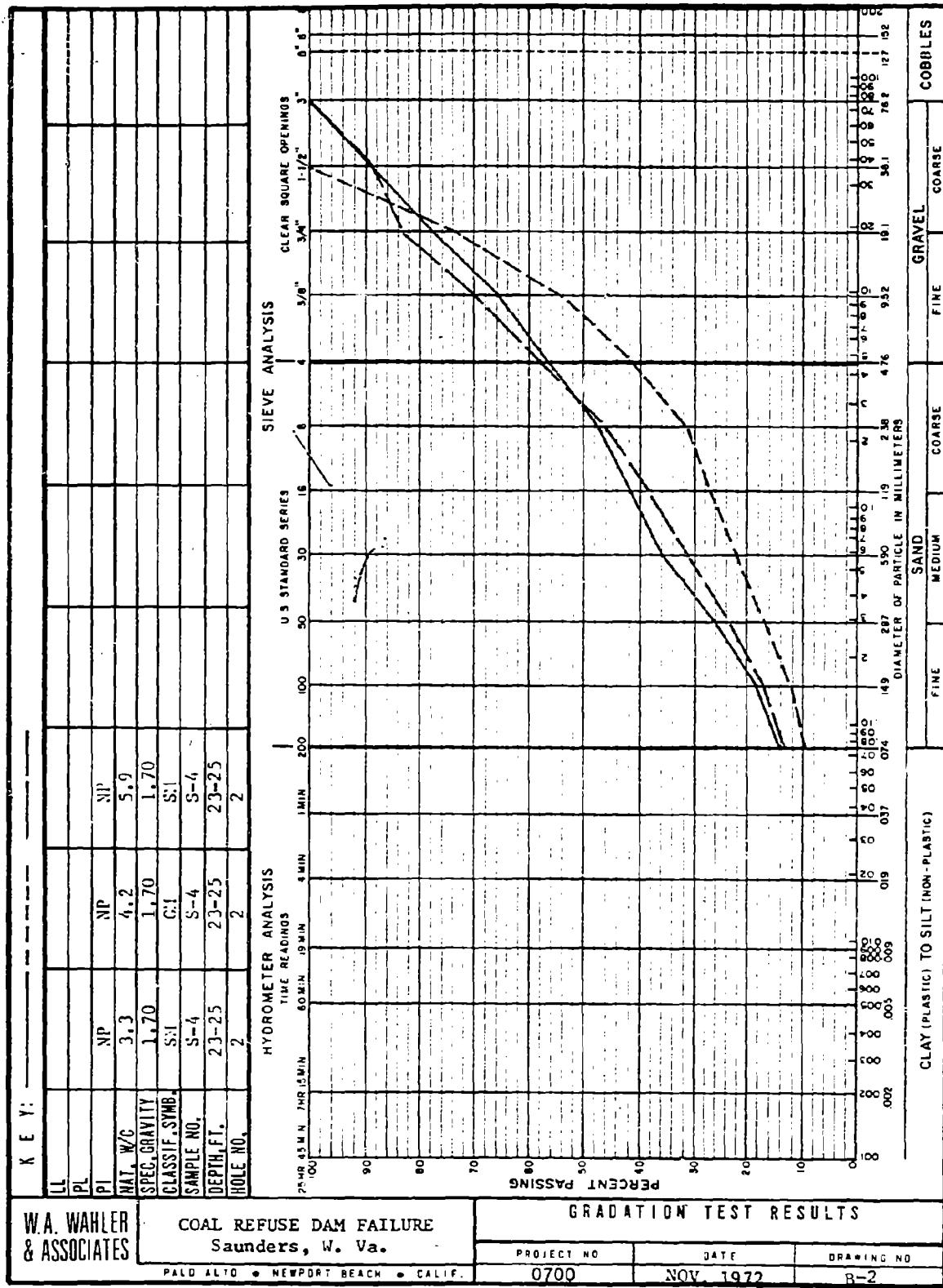
112

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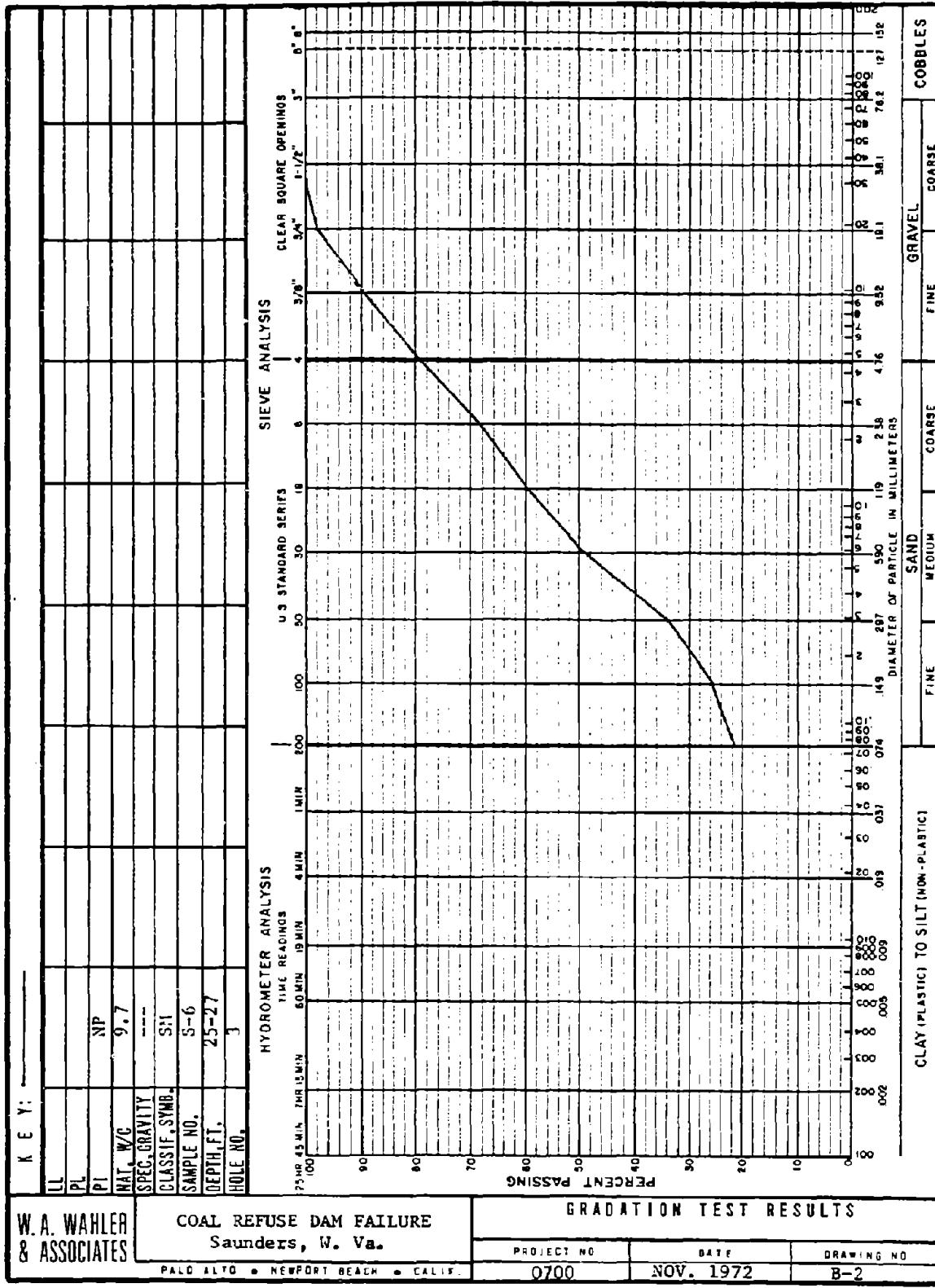
**COAL REFUSE DAM FAILURE
Saunders, W. Va.**

GRADATION TEST RESULTS

PROJECT NO	DATE	DRAWING NO
0700	NOV. 1972	B-2

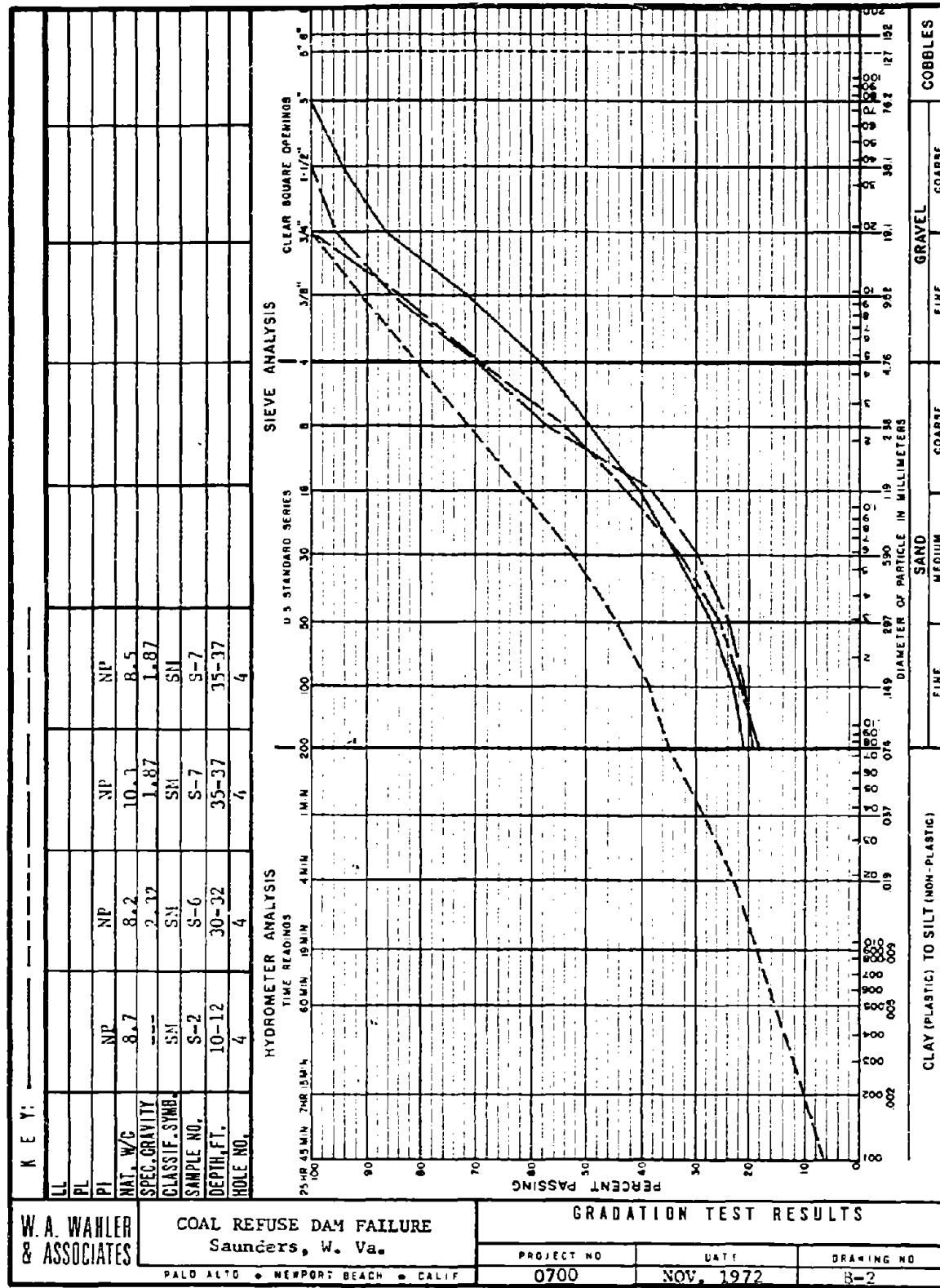


HOLE 3

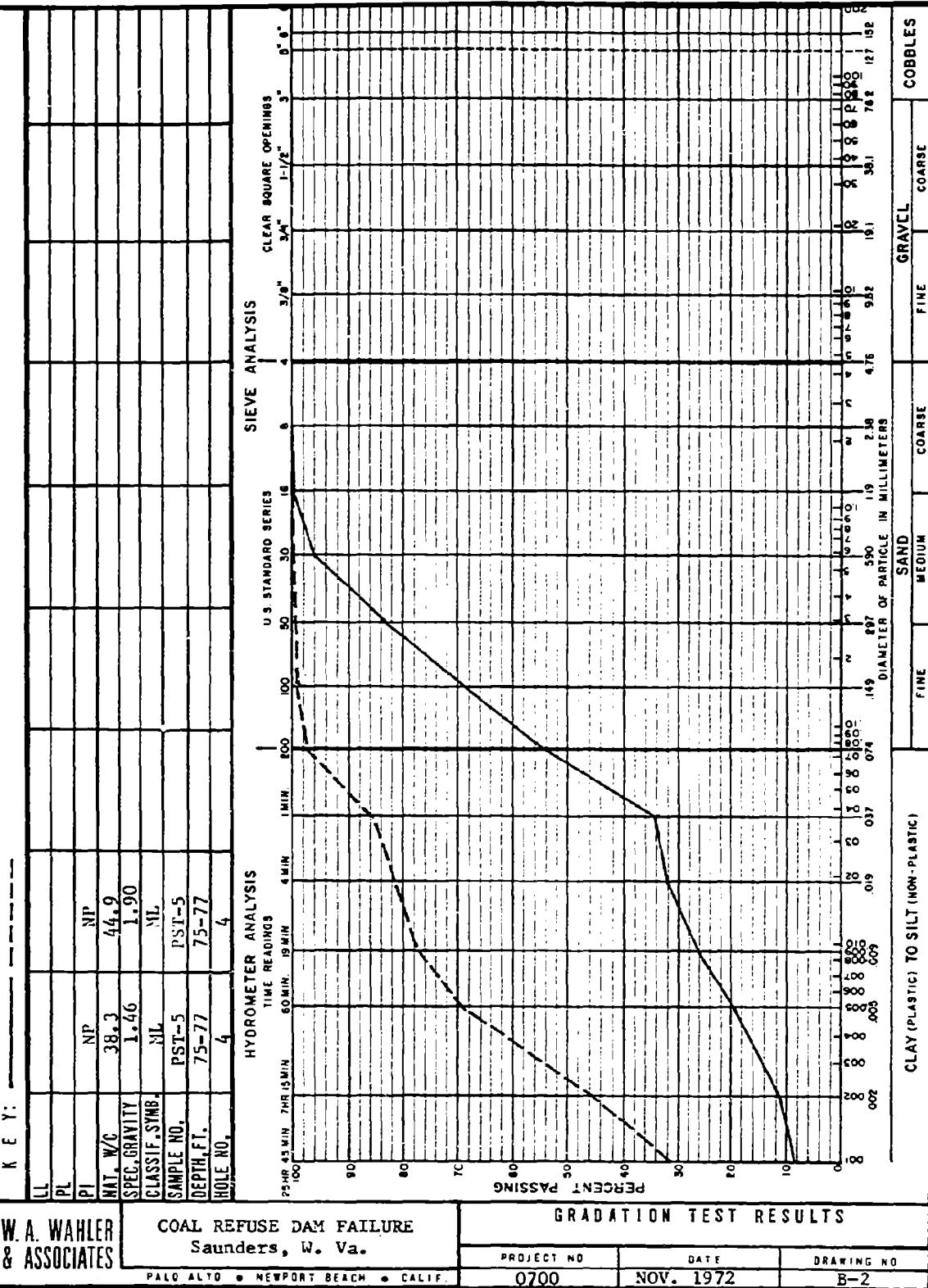


Sheet 2 of 25

HOLE 4



HOLE 4
COARSE FINE
PORTION PORTION

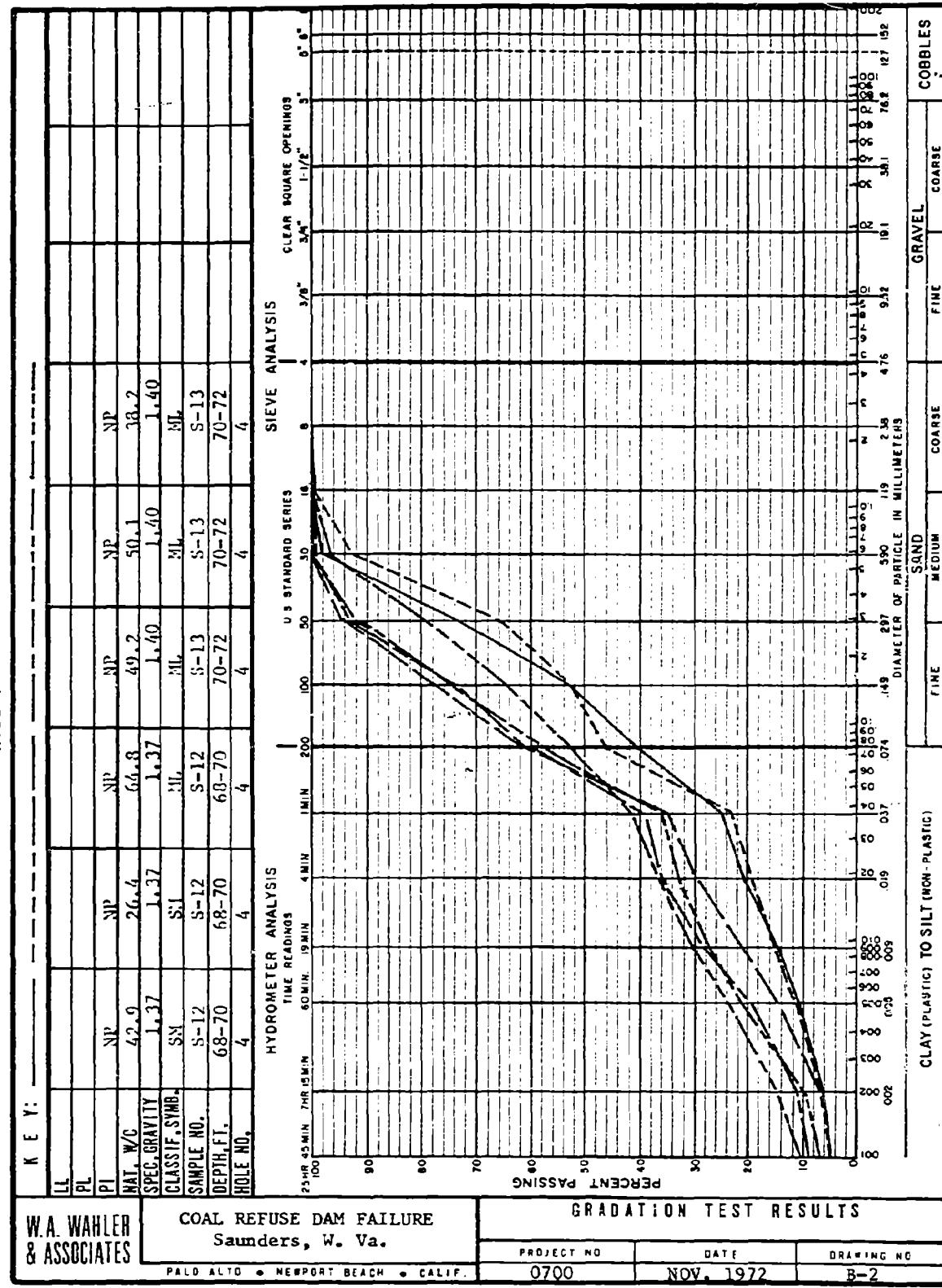


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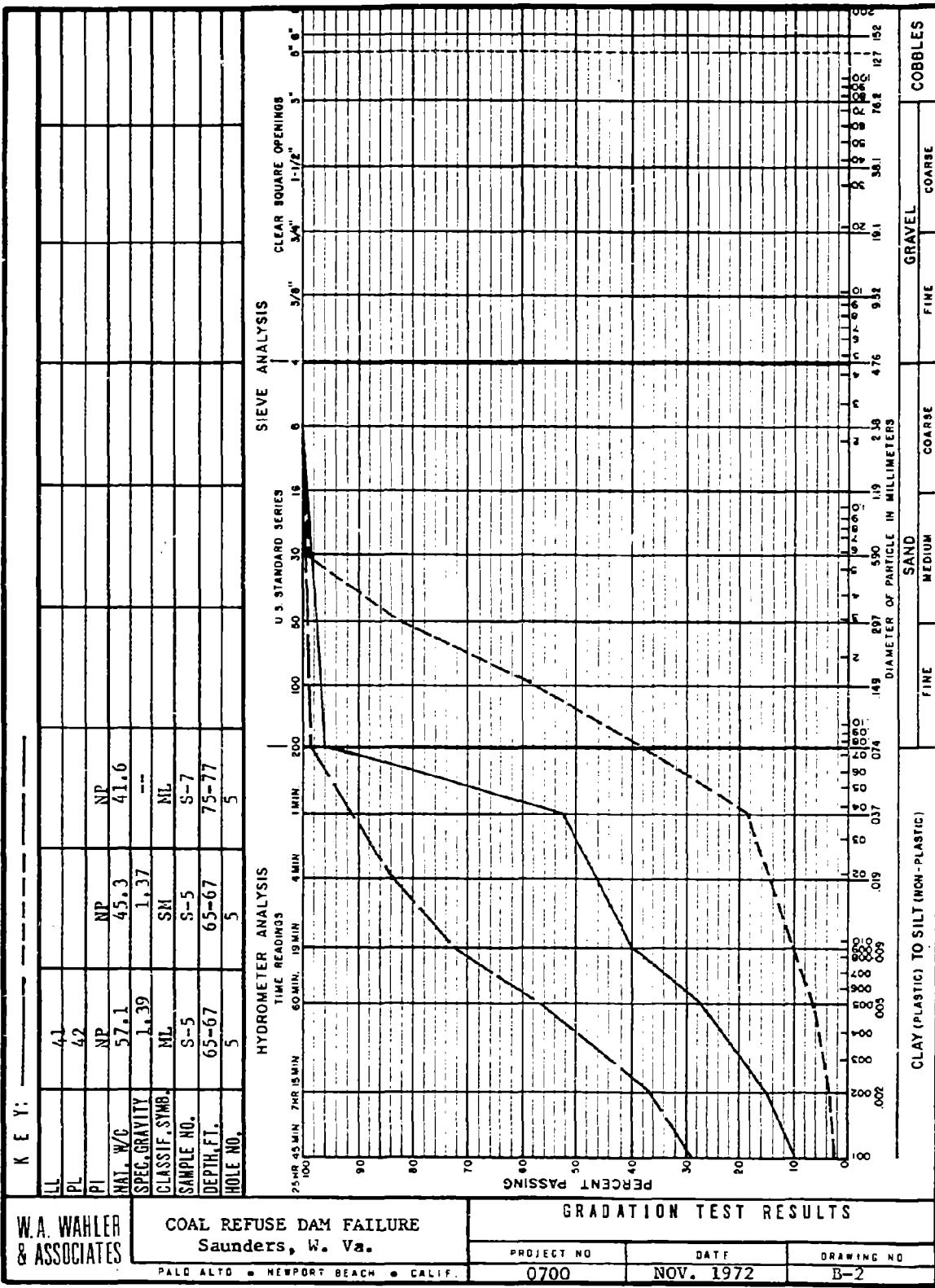
COAL REFUSE DAM FAILURE
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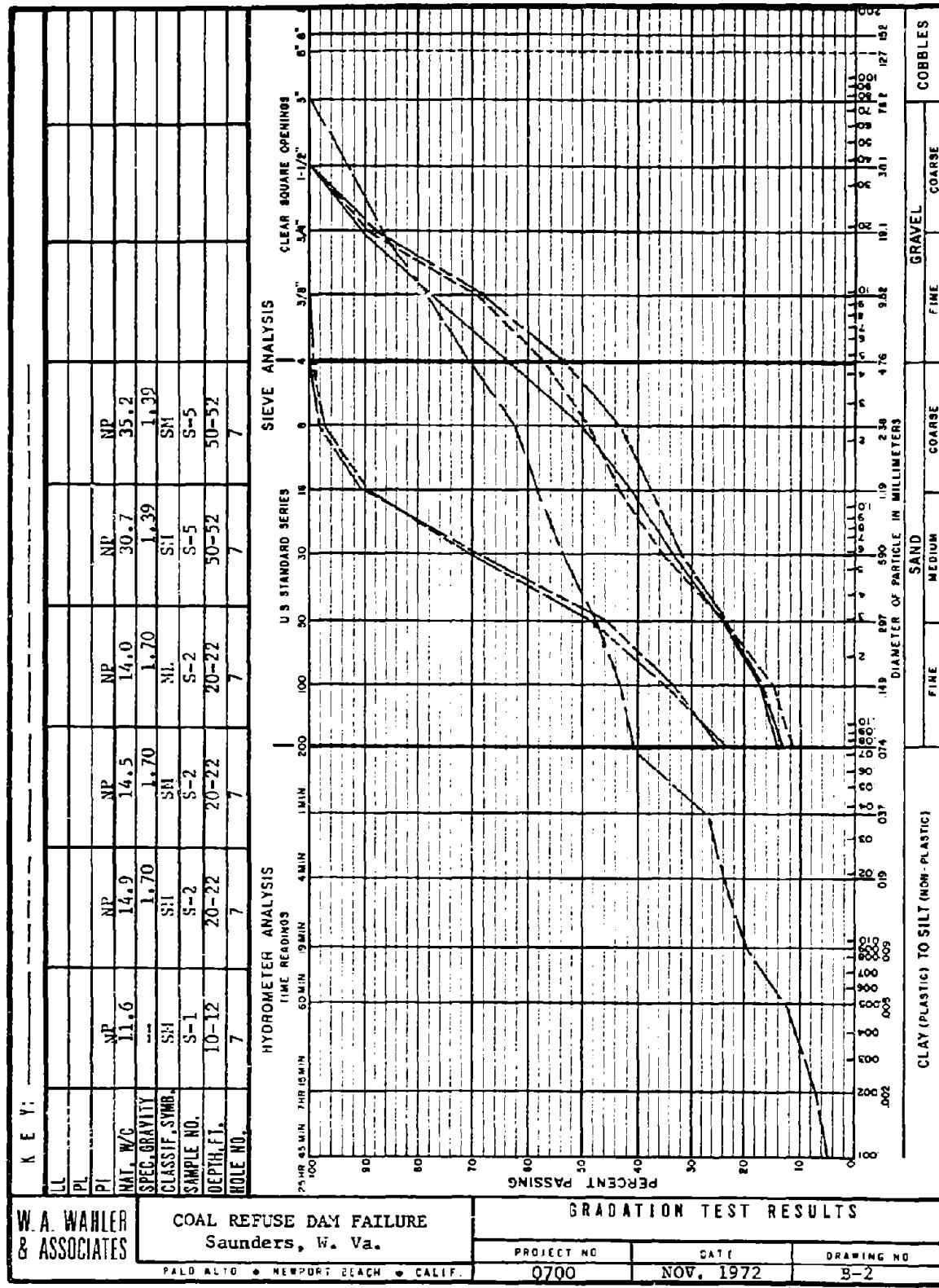
HOLE 4



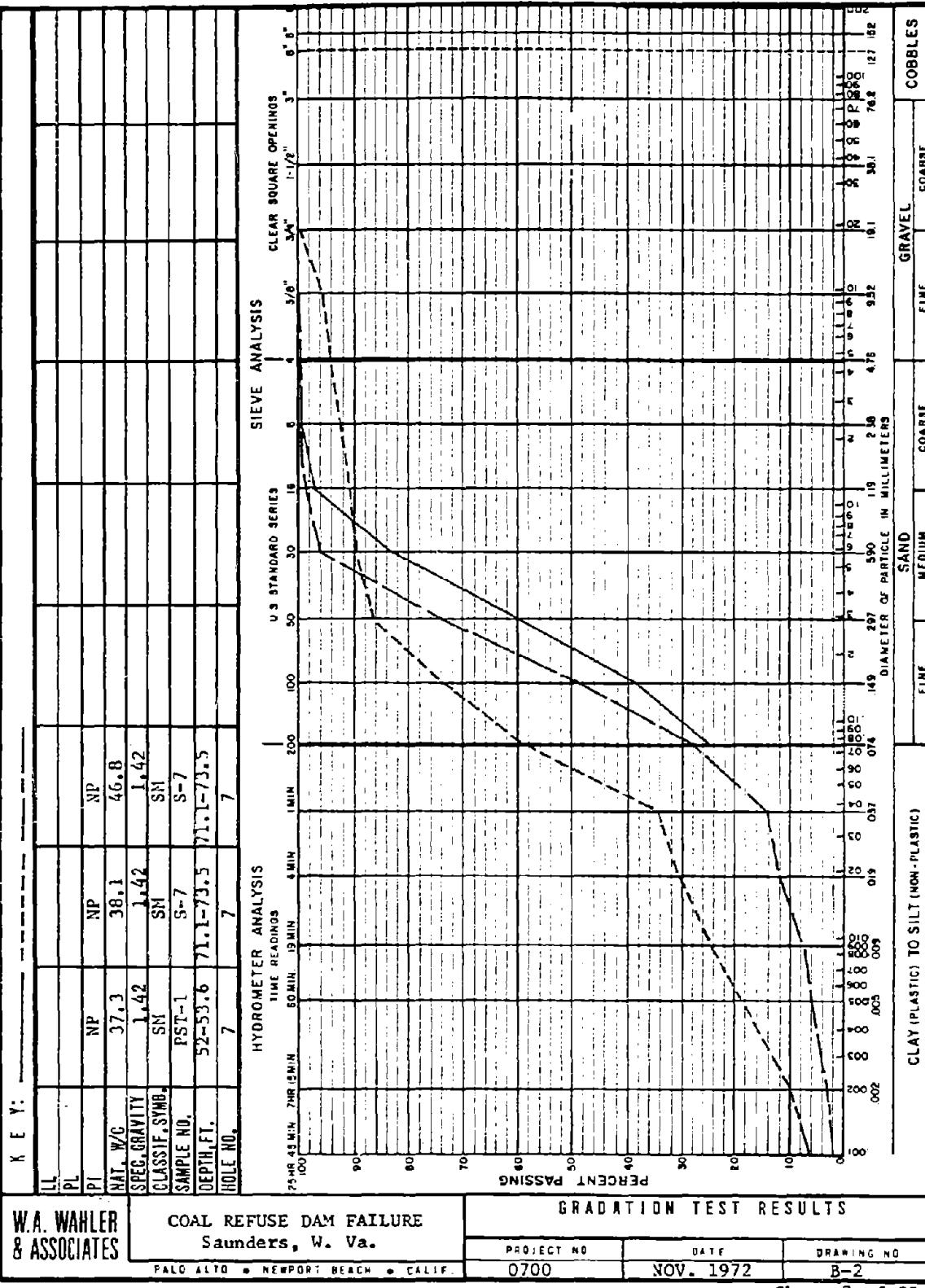
HOLE 5
FINE
COARSE
PORTION



HOLE 7



HOLE 7



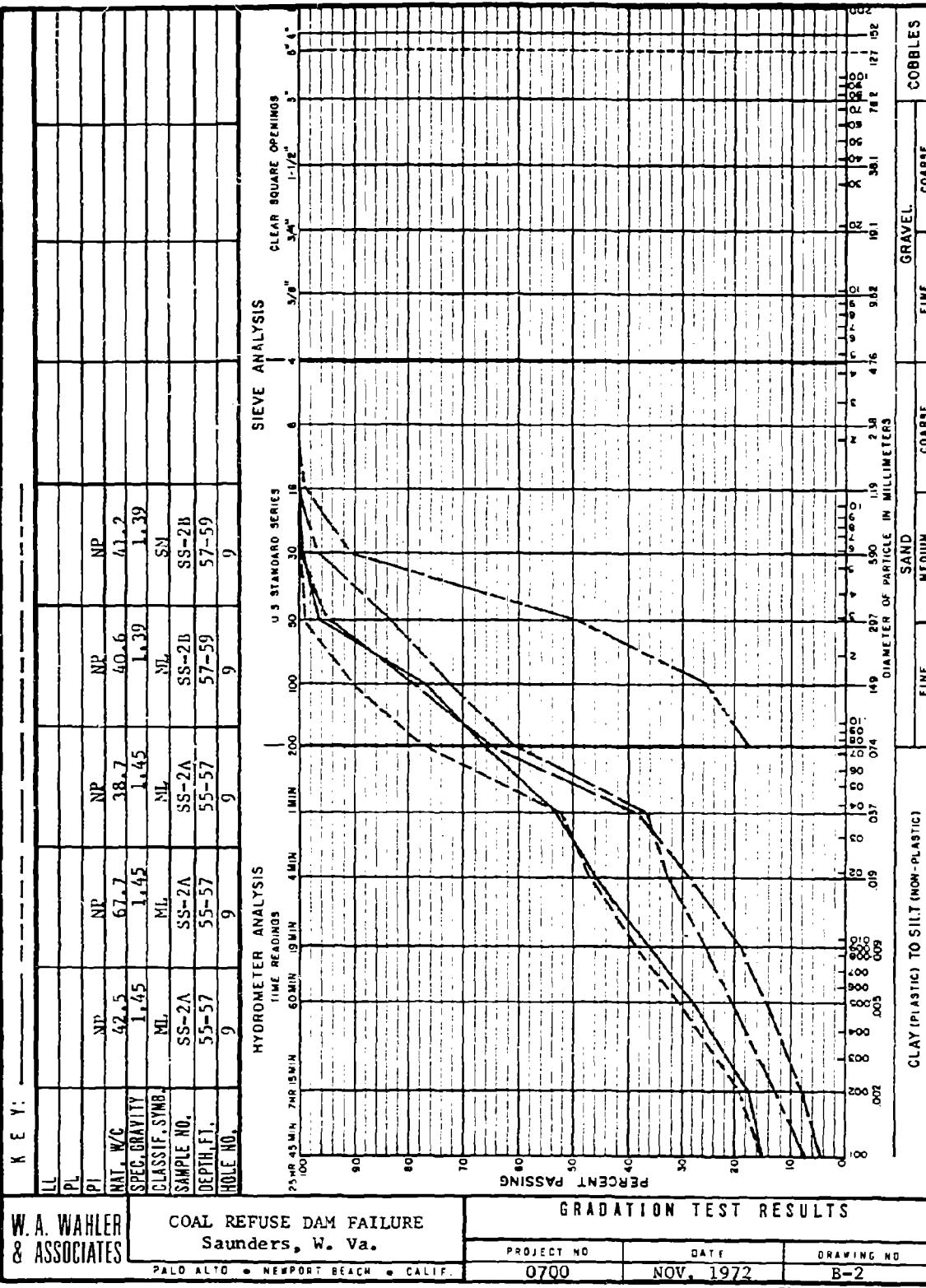
HOLE 8

KEY:		HYDROMETER ANALYSIS						SIEVE ANALYSIS										
LL	PL	NP	13.6	41.2	---	1.34	SM	S	USTI-2	20-22	55-57	8	8	3 1/2"	3"	5 1/4"	5 1/2"	6 1/4"
PI																		
NAT. W/C																		
SPEC. GRAVITY																		
CLASSIF. SYMB.																		
SAMPLE NO.																		
DEPTH, FT.																		
HOLE NO.																		
TIME READINGS	25 HR 45 MIN	7HR 15 MIN	60 MIN	15 MIN	4 MIN	1 MIN	100	100	100	100	100	100	100	100	100	100	100	100
PERCENT PASSING																		
CLAY (PLASTIC) TO SILT (NON-PLASTIC)																		
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11.1

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HOLE 9



HOLE 10

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**COAL REFUSE DAM FAILURE
Saunders - W. Va.**

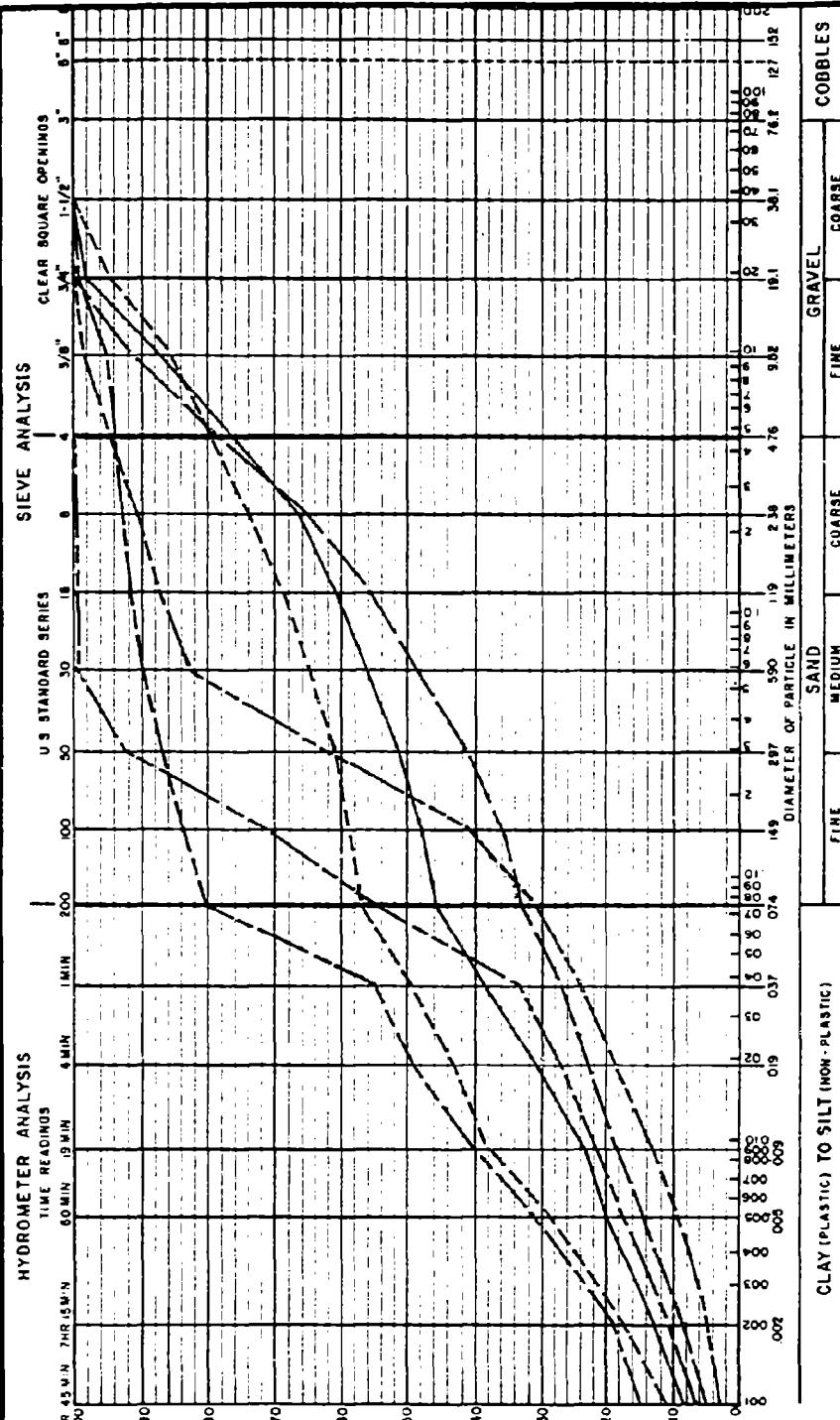
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GRADATION TEST RESULTS

PROJECT NO	DATE	DRAWING NO
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HOLE 1

K E Y:	L	L	NP	NP	NP	NP	NP
1	NP	NP	NP	NP	NP	NP	NP
AT. W/G	12.0	10.5	17.6	37.3	45.0	32.0	
PEC. GRAVITY	2.24	2.24	2.24	1.66	1.66	1.66	
CLASSIF. SYMBOL.	S/N	N/L	S/N	N/L	N/L	S/N	
AMPLE NO.	PST-1	PST-1	PST-1	SS-3A	SS-3A	SS-3A	
DEPTH FT.	35-37	35-37	35-37	85-87	85-87	85-87	
ROLE NO.	11	11	11	11	11	11	



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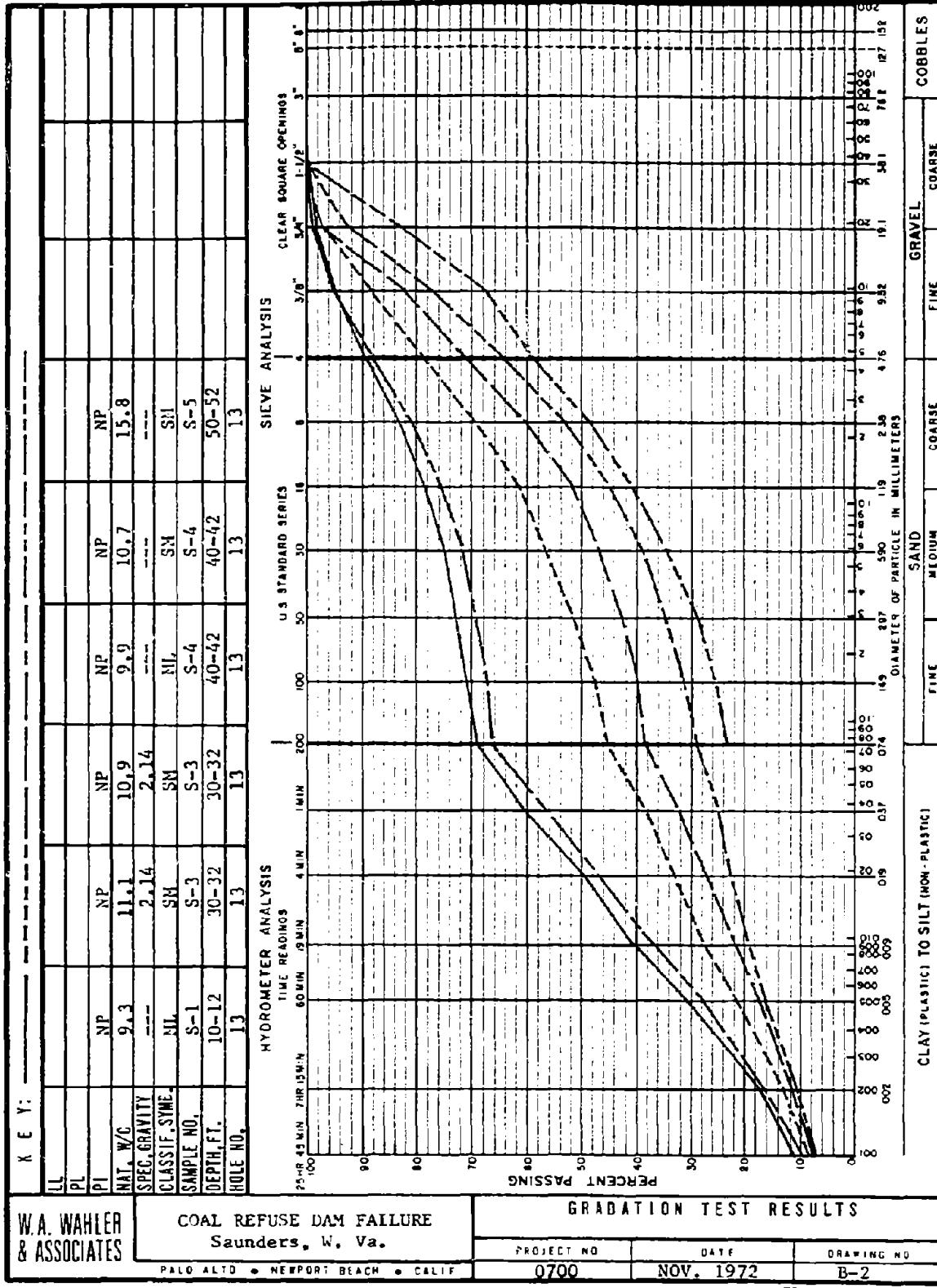
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GRADATION TEST RESULTS

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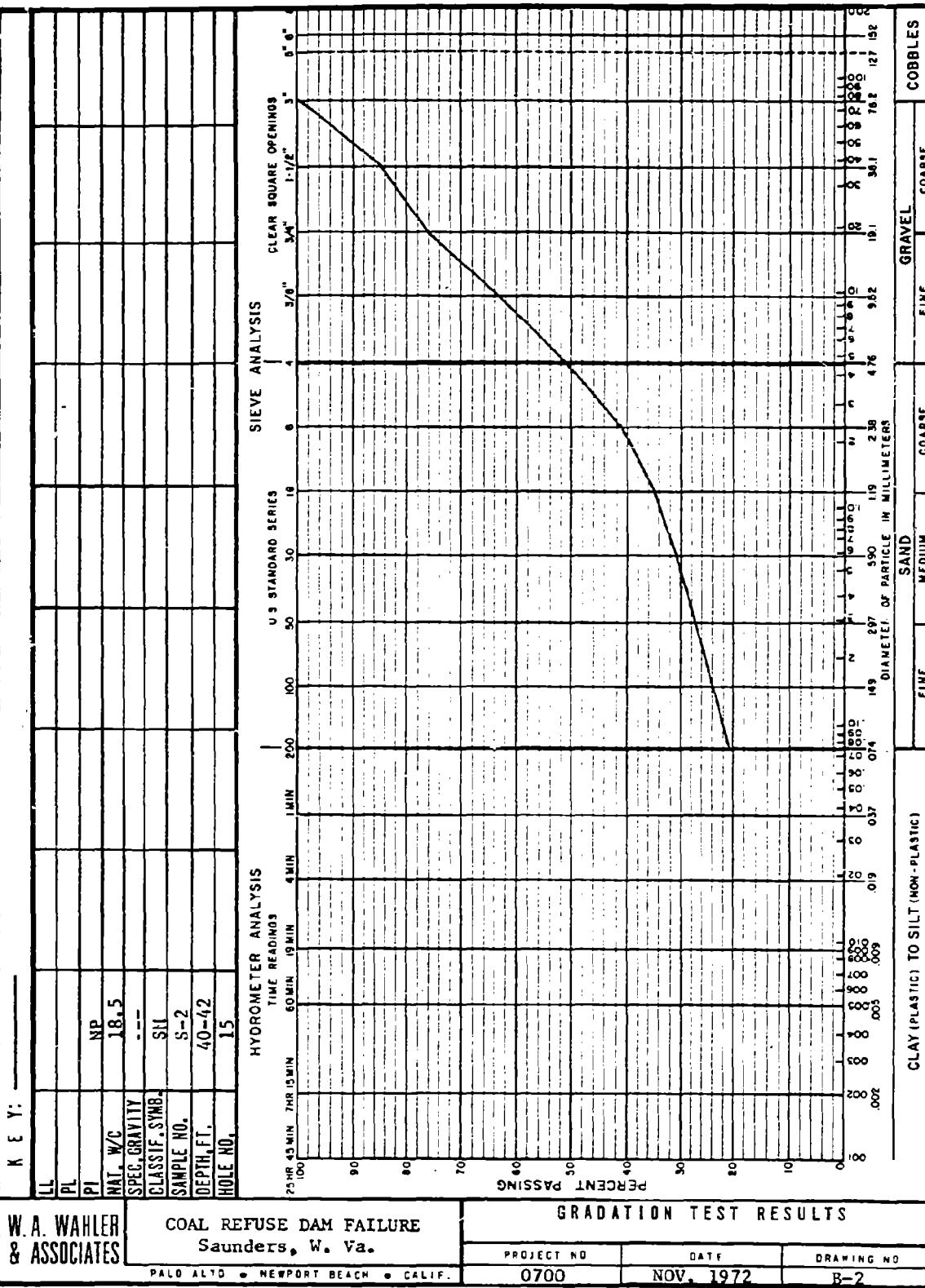
HOLE 13



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HOLE 15

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GRADATION TEST RESULTS

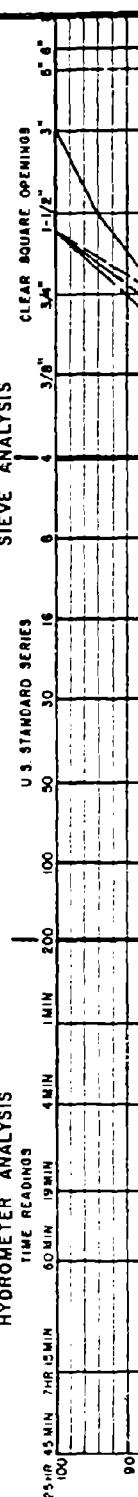
PROJECT NO	DATE	DRAWING NO
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SAMPLE A-1

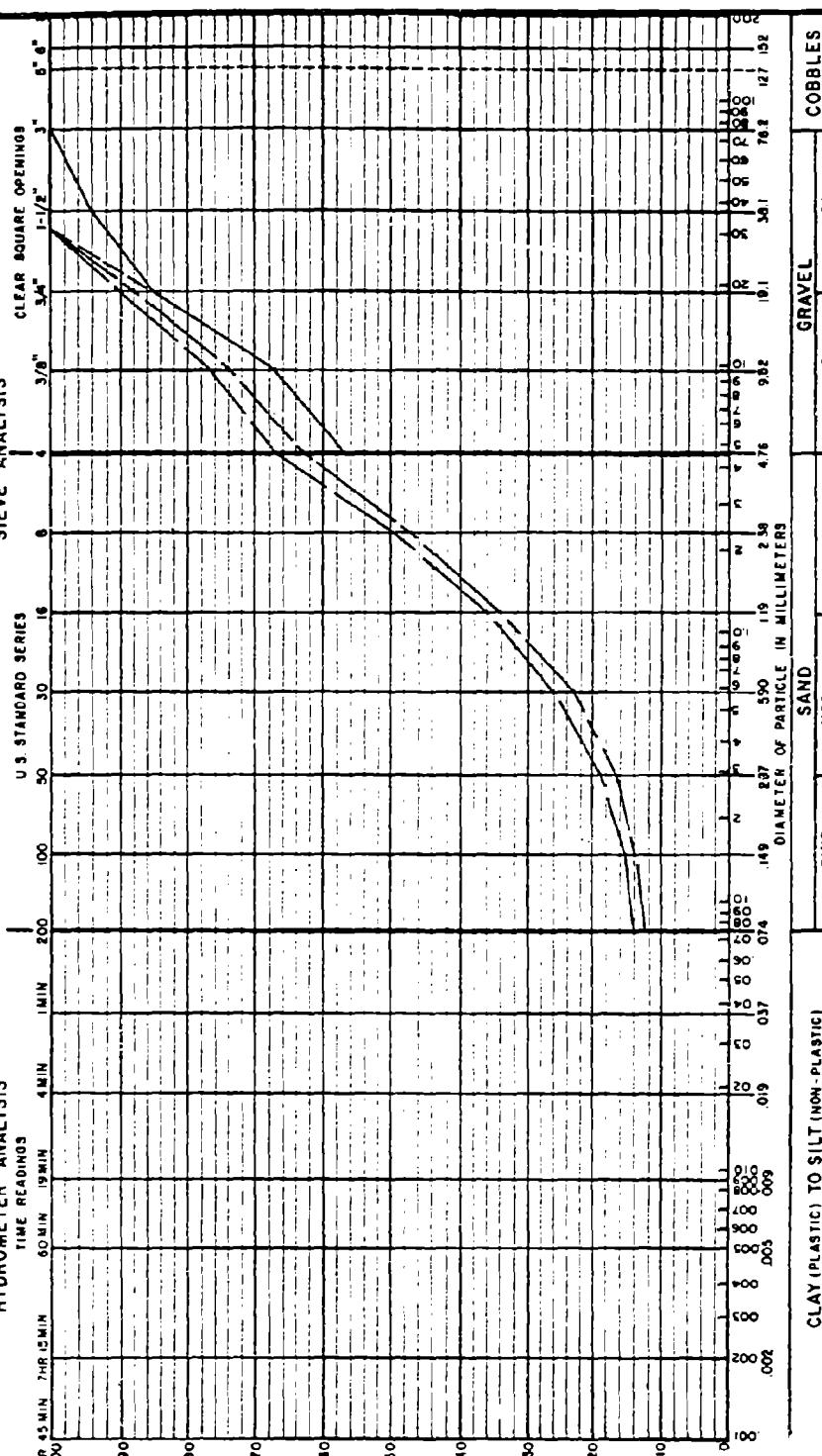
TOTAL
AVERAGE
GRADATION

K E Y:	TOTAL GRADATION			SET-UP GRADATION			ICU SAMPLE AFTER FAILURE			K_0 SAMPLE AFTER FAILURE		
	LL	PL	PI	NP	NP	NP	NP	NP	NP	NP	NP	NP
NAT. W/C	---	---	---	---	---	---	---	---	---	---	---	---
SPEC. GRAVITY	1.90	1.90	1.90	1.90	1.90	1.90	1.90	1.90	1.90	1.90	1.90	1.90
CLASSIF. SYMB.	SM	SM	SM	SM	SM	SM	SM	SM	SM	SM	SM	SM
SAMPLE NO.	A-1	A-1	A-1	A-1	A-1	A-1	A-1	A-1	A-1	A-1	A-1	A-1
DEPTH FT.	---	---	---	---	---	---	---	---	---	---	---	---
HOLE NO.	---	---	---	---	---	---	---	---	---	---	---	---

HYDROMETER ANALYSIS



SIEVE ANALYSIS



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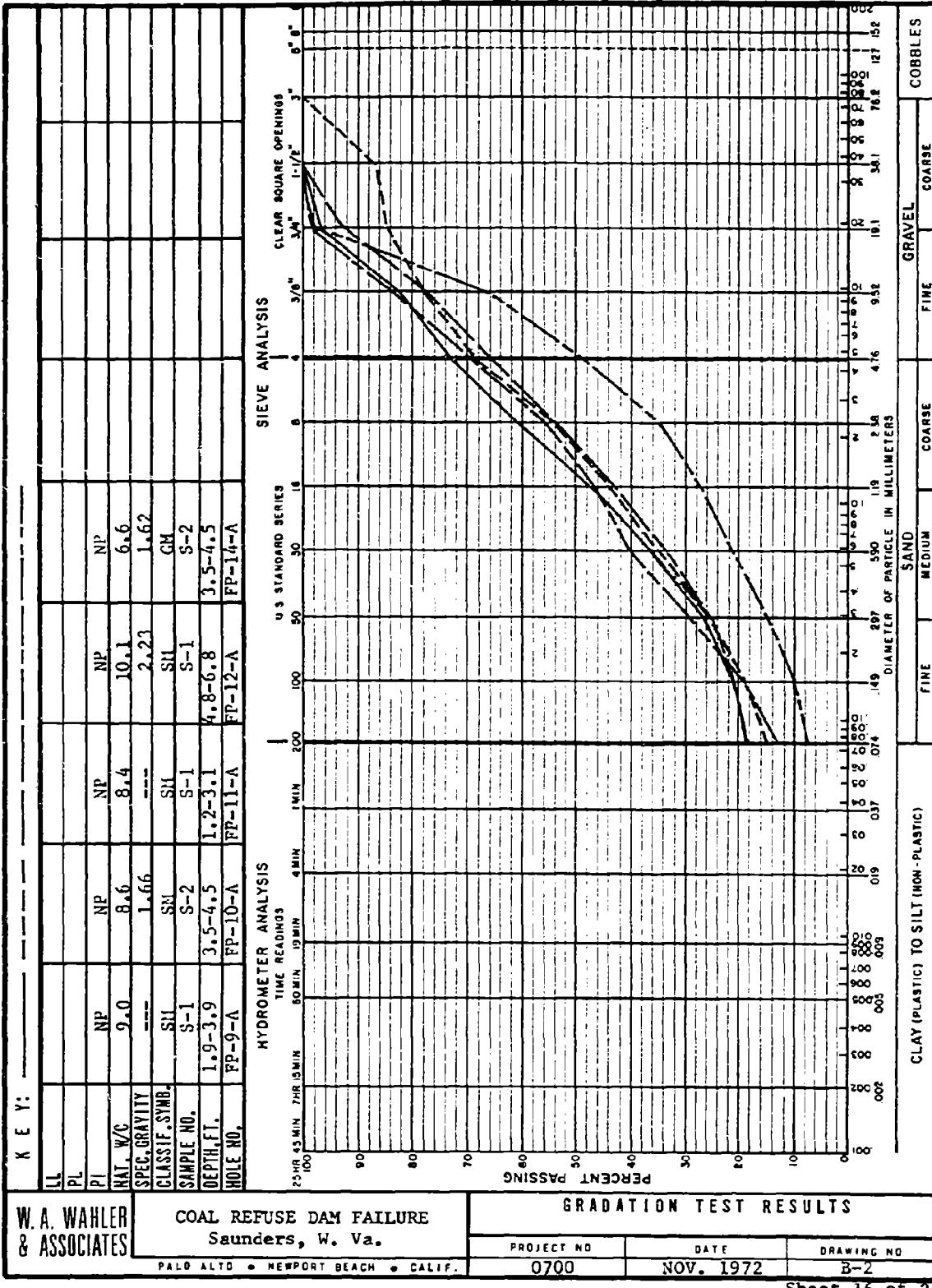
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GRADATION TEST RESULTS

PROJECT NO	DATE	DRAWING NO
0700	NOV. 1972	B-2

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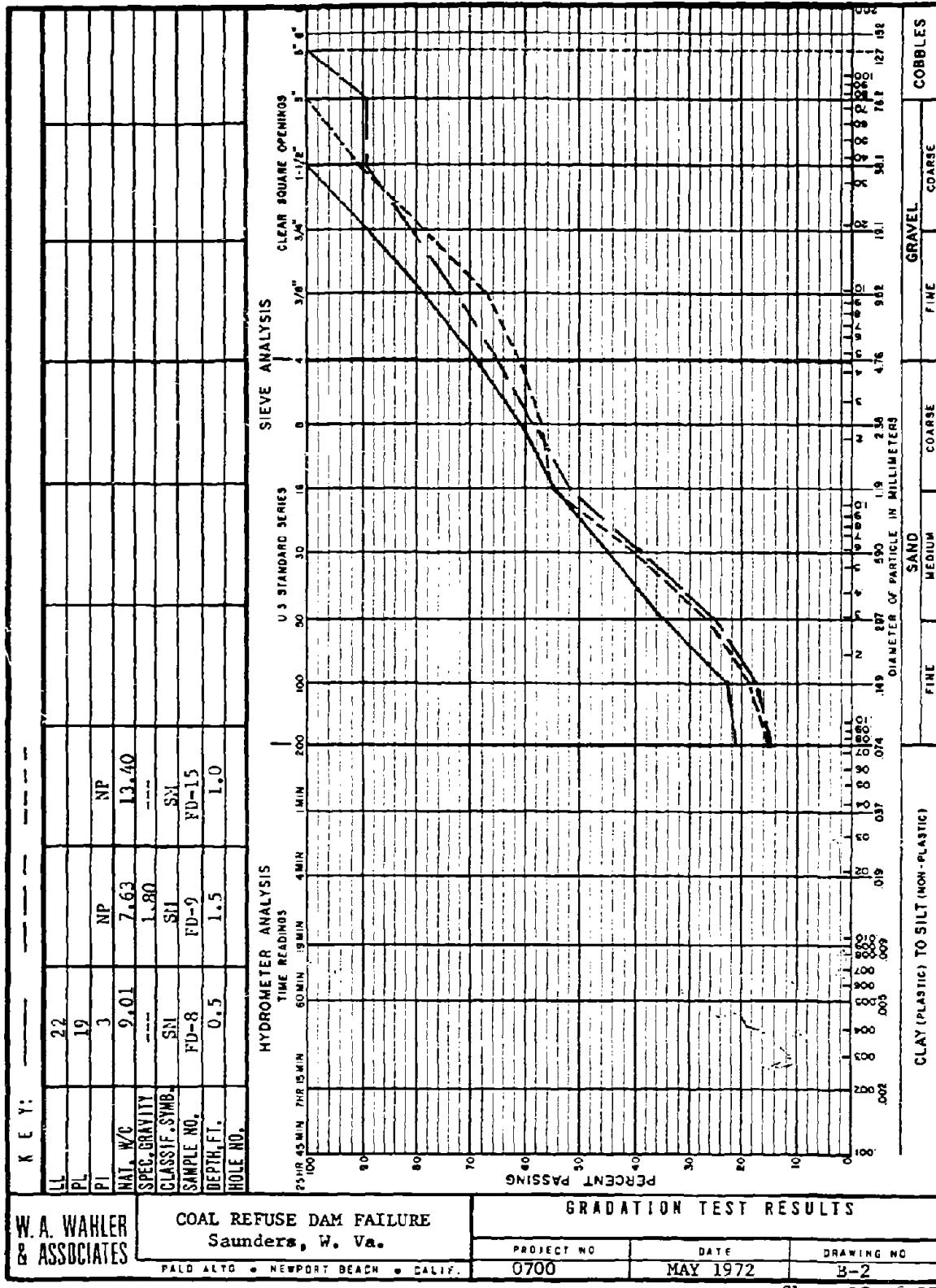
FIELD PERMEABILITY SAMPLES



FOUNDATION/CHANNEL AREA - DAM 3 AND DAM 1

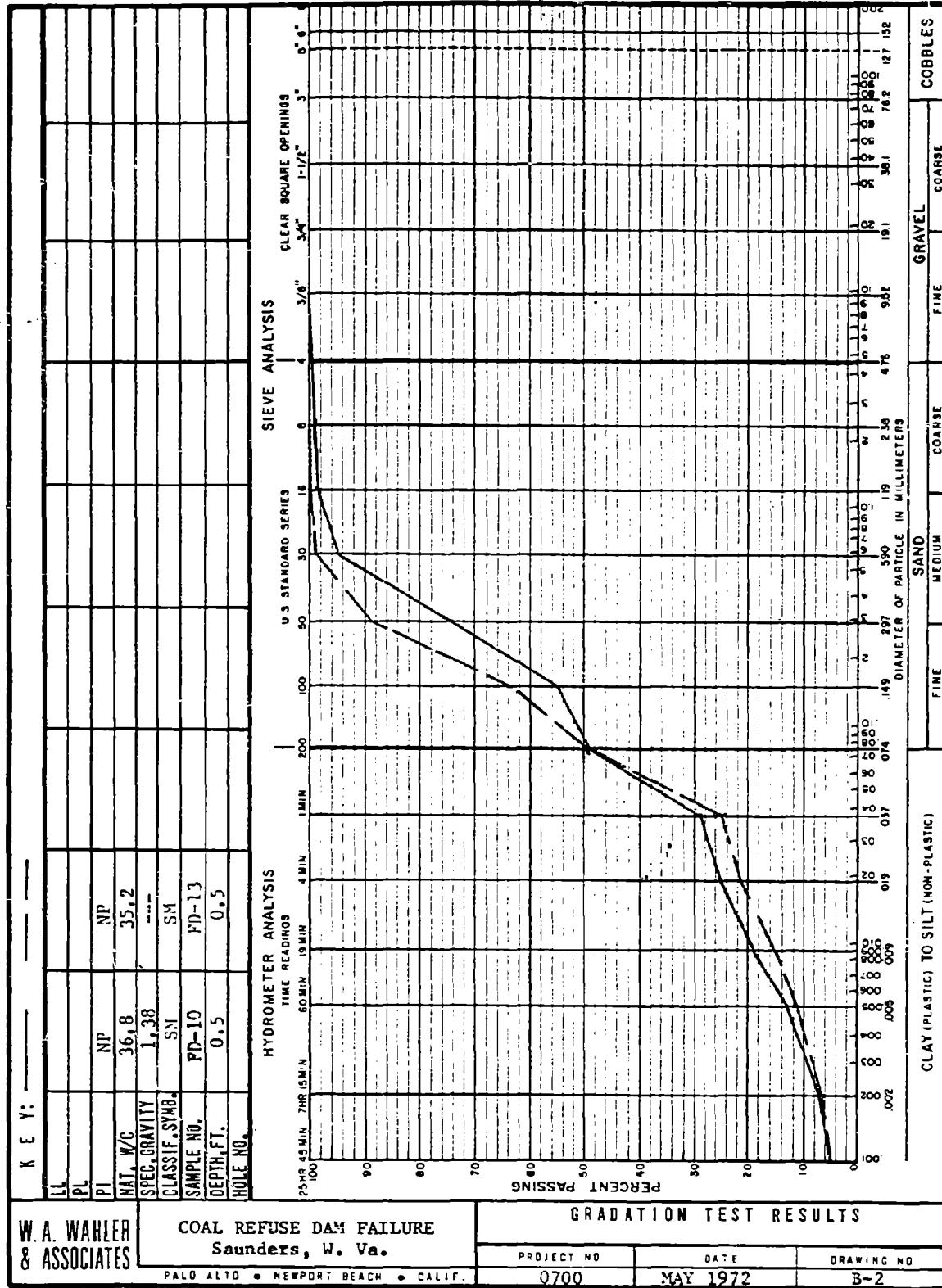
Sheet 17 of 25

GOB PILE AT BUFFALO CREEK



Sheet 18 of 25

TAILINGS NEAR LEFT ABUTMENT OF DAM 2



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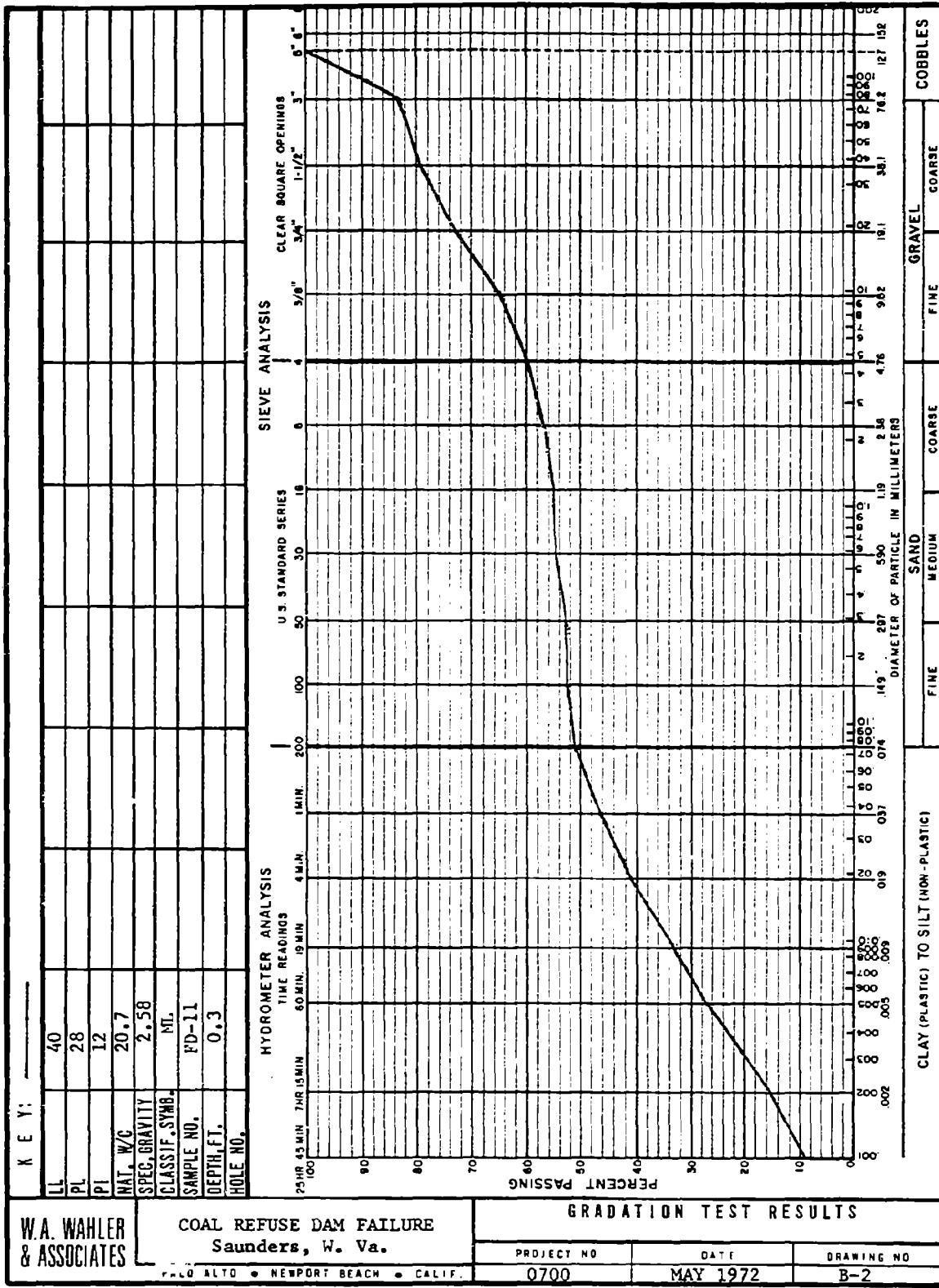
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GRADATION TEST RESULTS

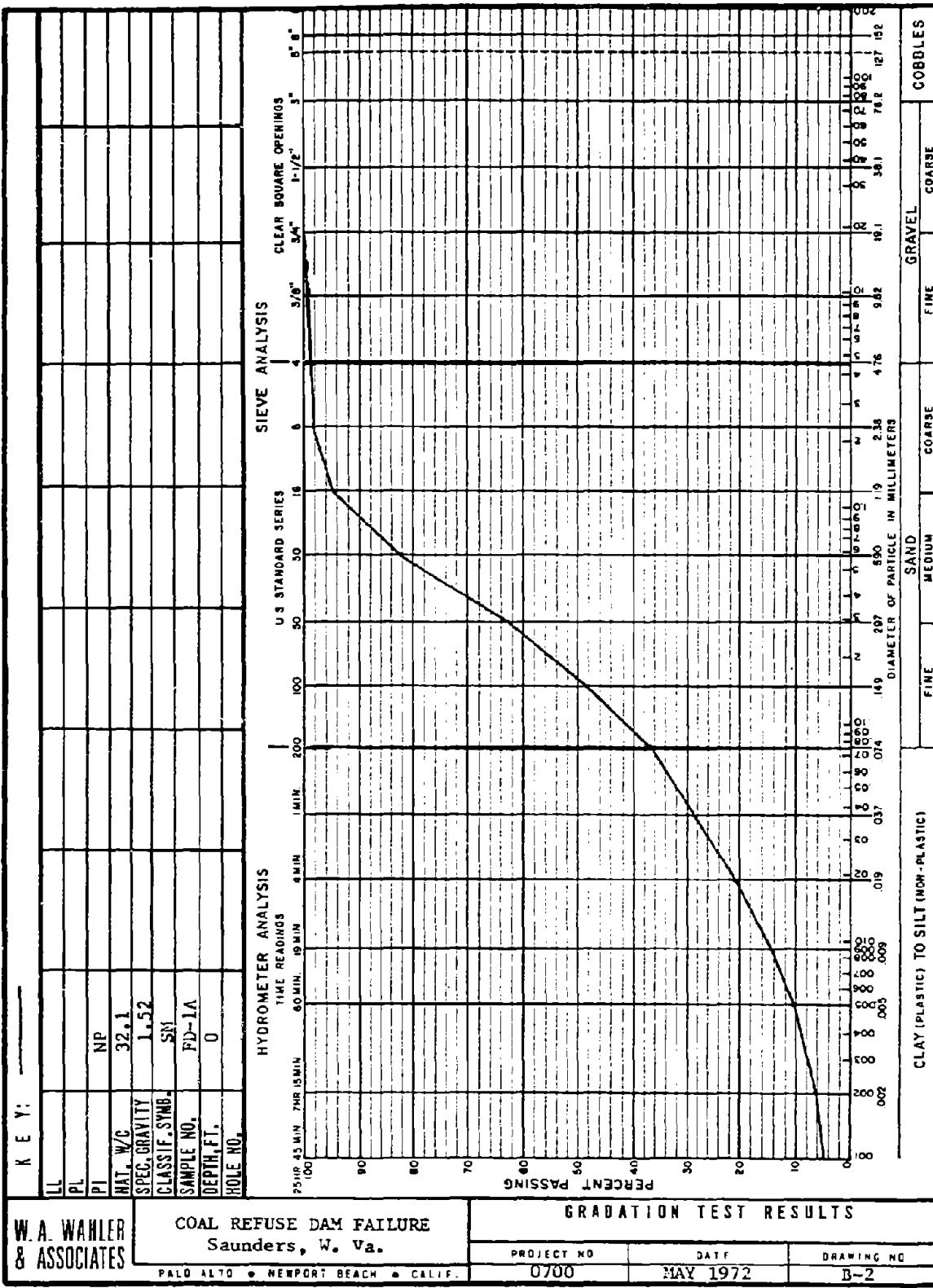
PROJECT NO	DATE	DRAWING NO
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NATURAL MATERIAL - LEFT ABUTMENT DAM 2

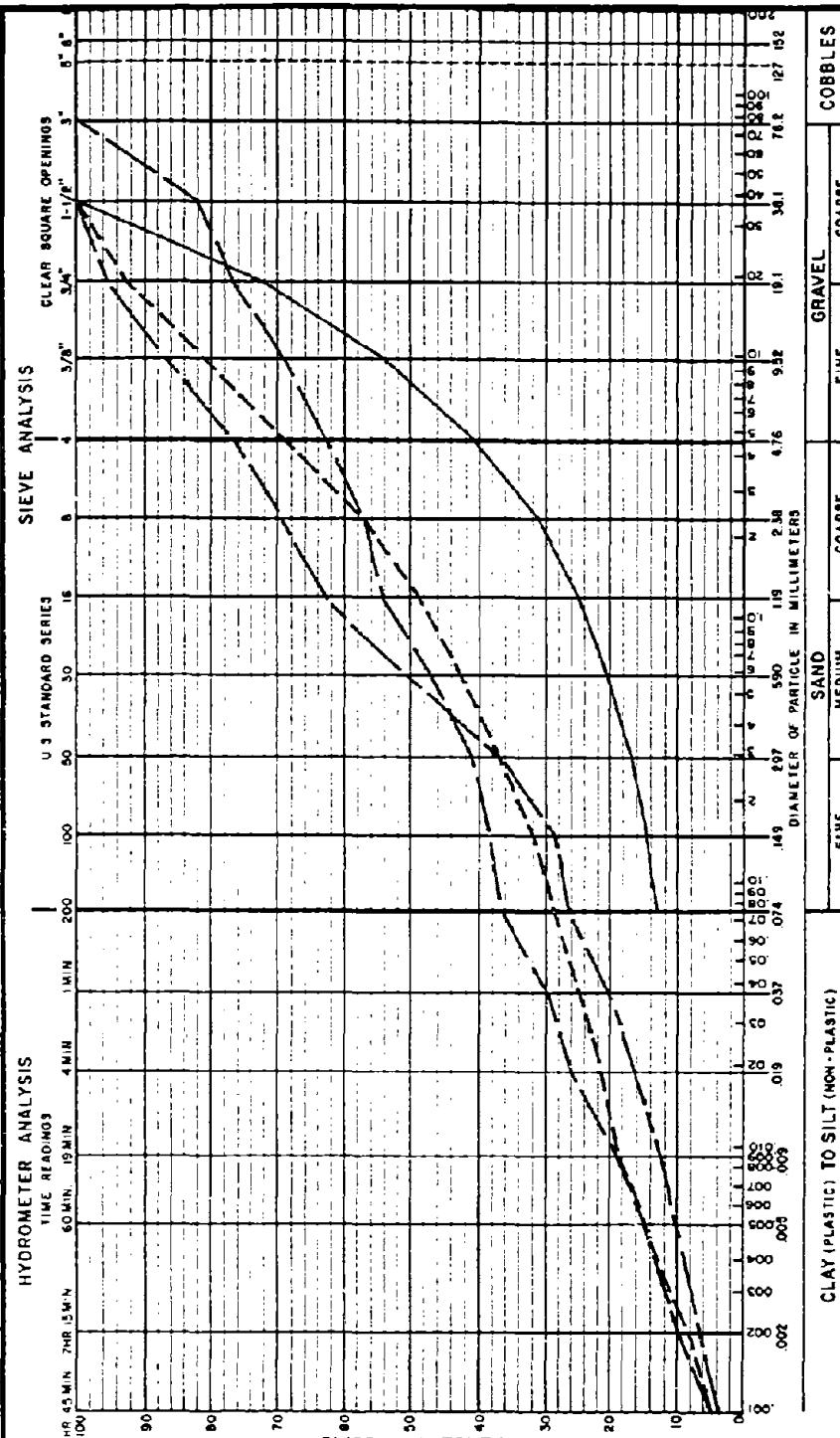


TAILINGS - DAM 4



RIGHT ABUTMENT
CREST DAM 4
DAM 3

K E Y:				
	29			
	23			
	NP	NP	NP	NP
I. I. W/C	7.54	10.40	5.49	6.85
SEC. GRAVITY	2.07	---	1.85	---
ASSIF. SYAB.	CN	SN	SM	SK
AMPLE NO.	FD-3A	FD-5A	FD-6A	FD-6A
PTH. FT.	1.0	1.0	1.0	1.0
LE NO.				



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COAL REFUSE DAM FAILURE
Saunders, W. Va.

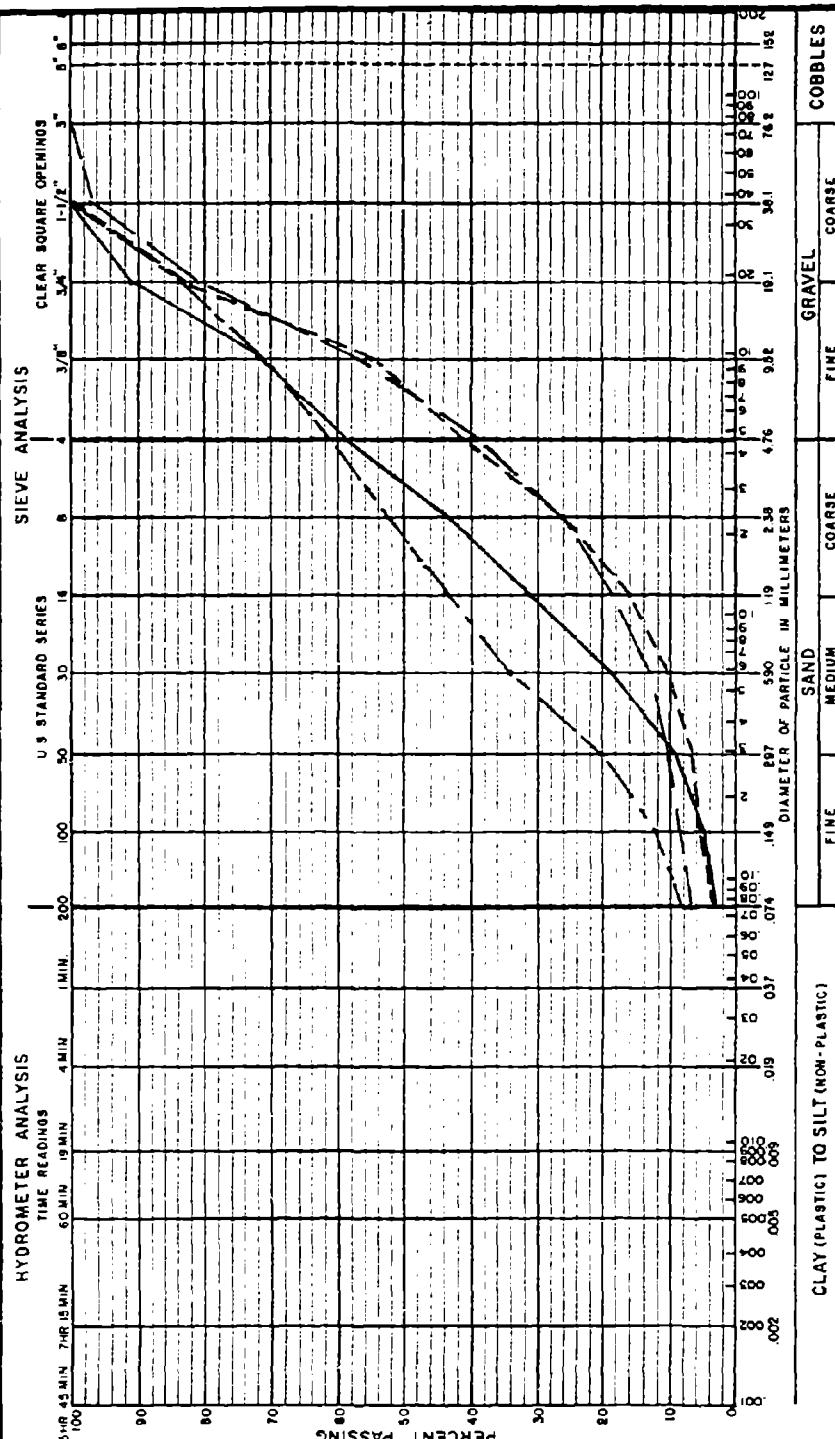
PALO ALTO • NEWPORT BEACH • CALIF

GRADATION TEST RESULTS

PROJECT NO	DATE	DRAWING NO
0700	MAY 1972	B-2

DOZER CUT THROUGH REMNANT OF DAM 3

K E V:	23	21	2	NP	NP	NP
AL. W/C	6.8		3.9	3.1	5.0	
PEC. GRAVITY	---		2.20	---	1.91	
CLASSIF. SYMBOL	SP		CH-CH	CH	SP-SN	
EXAMPLE NO.	FD-8A		FD-10A	FD-13A	FD-14A	
DEPTH, FT.	6.8		5.8	5.2	9.3	
OLE NO.						



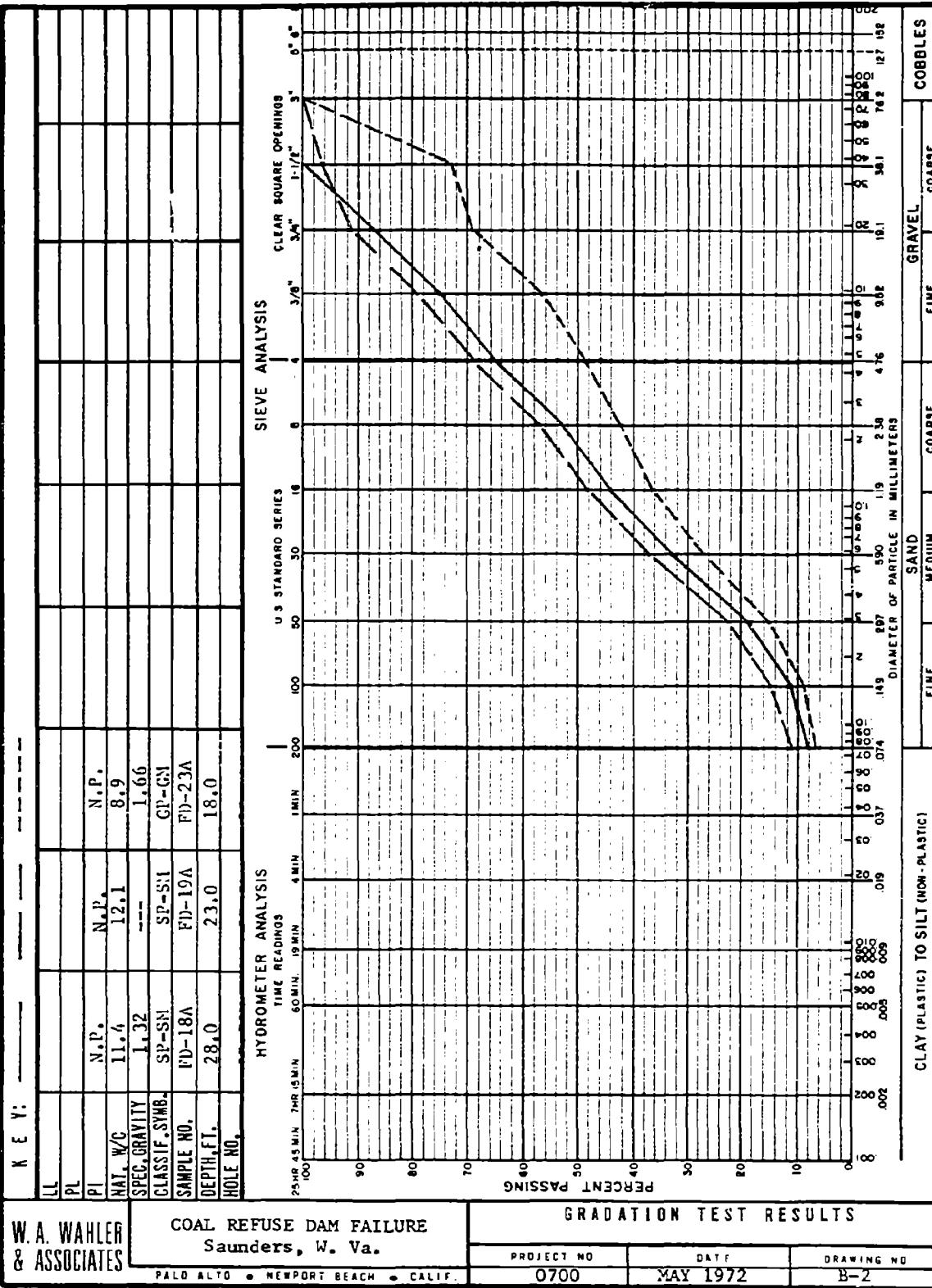
**W.A. WAHLER
& ASSOCIATES**

COAL REFUSE DAM FAILURE
Saunders, W. Va.

GRADATION TEST RESULTS

Saunders, W. Va.	PROJECT NO	DATE	DRAWING NO
PALO ALTO • NEWPORT BEACH • CALIF.	0700	MAY 1972	B-2

DOZER CUT THROUGH REMNANT OF DAM 3



**W. A. WAHLER
& ASSOCIATES**

**COAL REFUSE DAM FAILURE
Saunders, W. Va.**

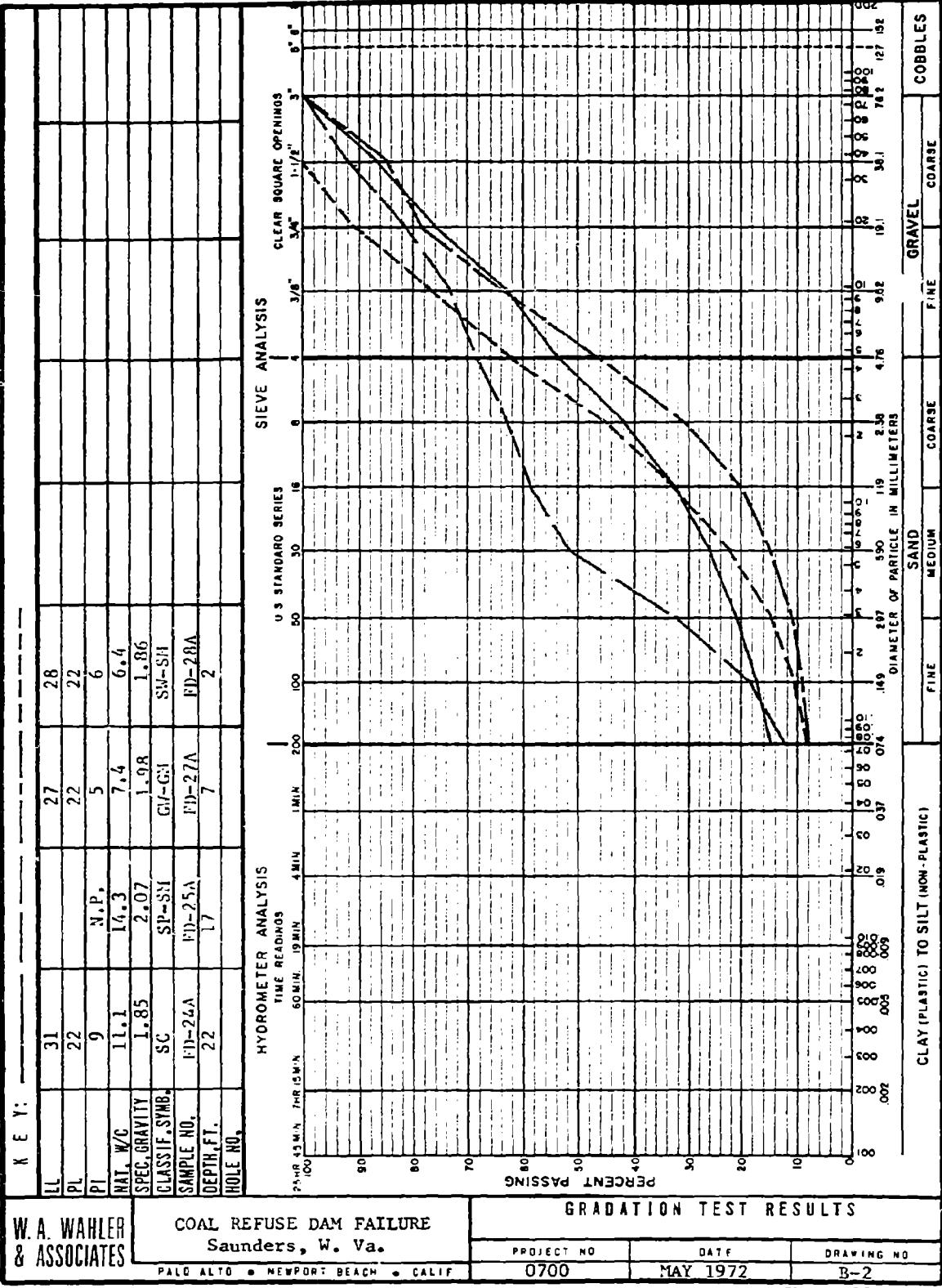
PALO ALTO • NEWPORT BEACH • CALIF.

GRADATION TEST RESULTS

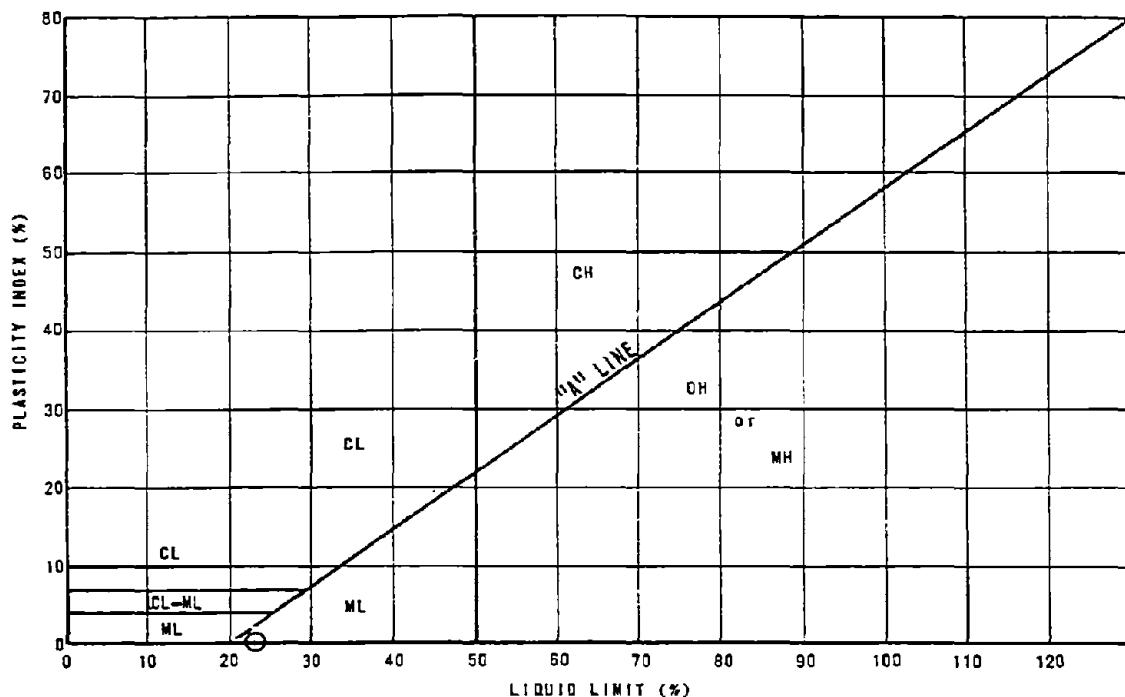
PROJECT NO.	DATE	DRAWING NO.
0700	MAY 1972	B-2

Sheet 24 of 25

DOZER CUT THROUGH REMNANT OF DAM 2

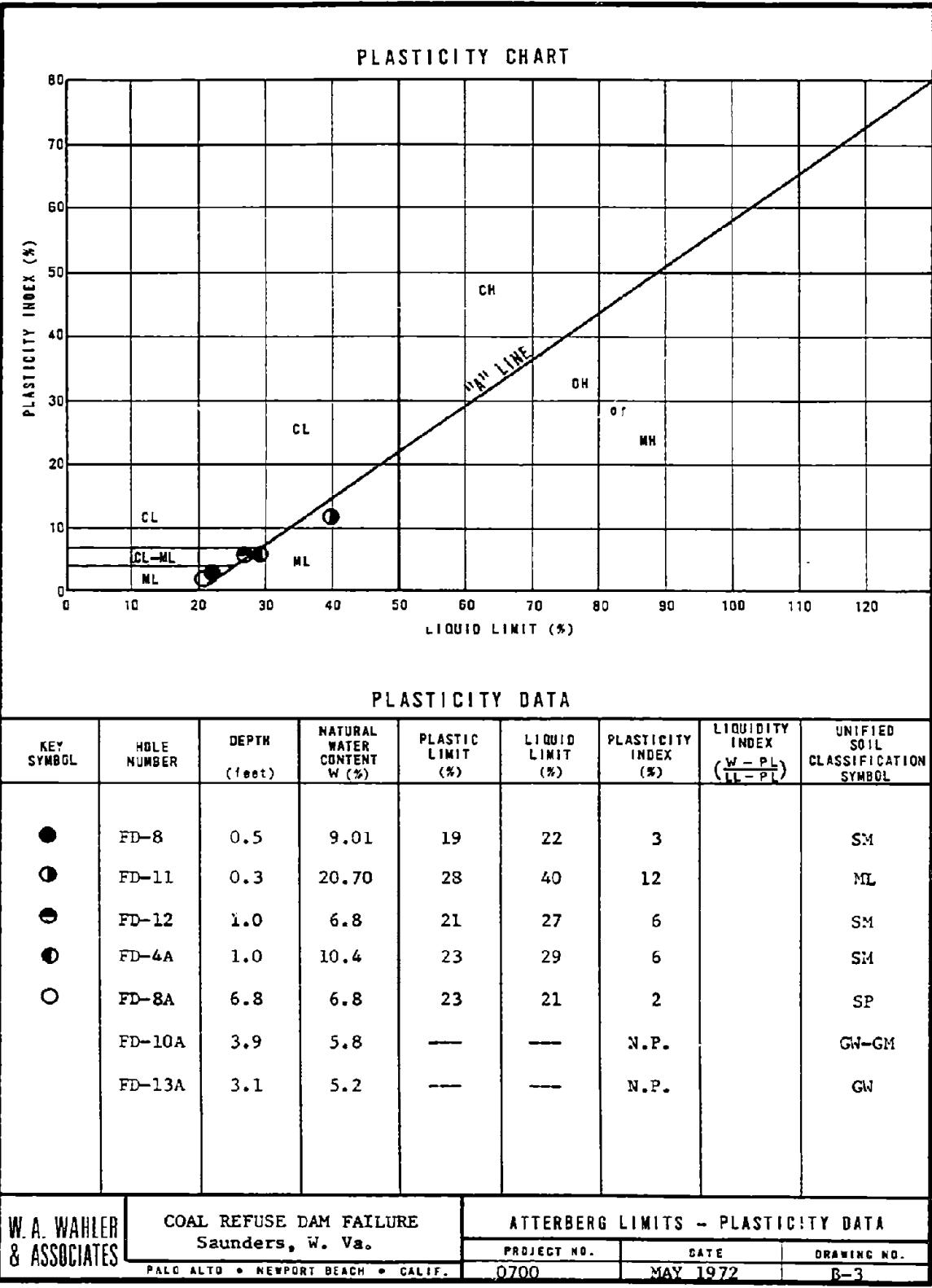


PLASTICITY CHART

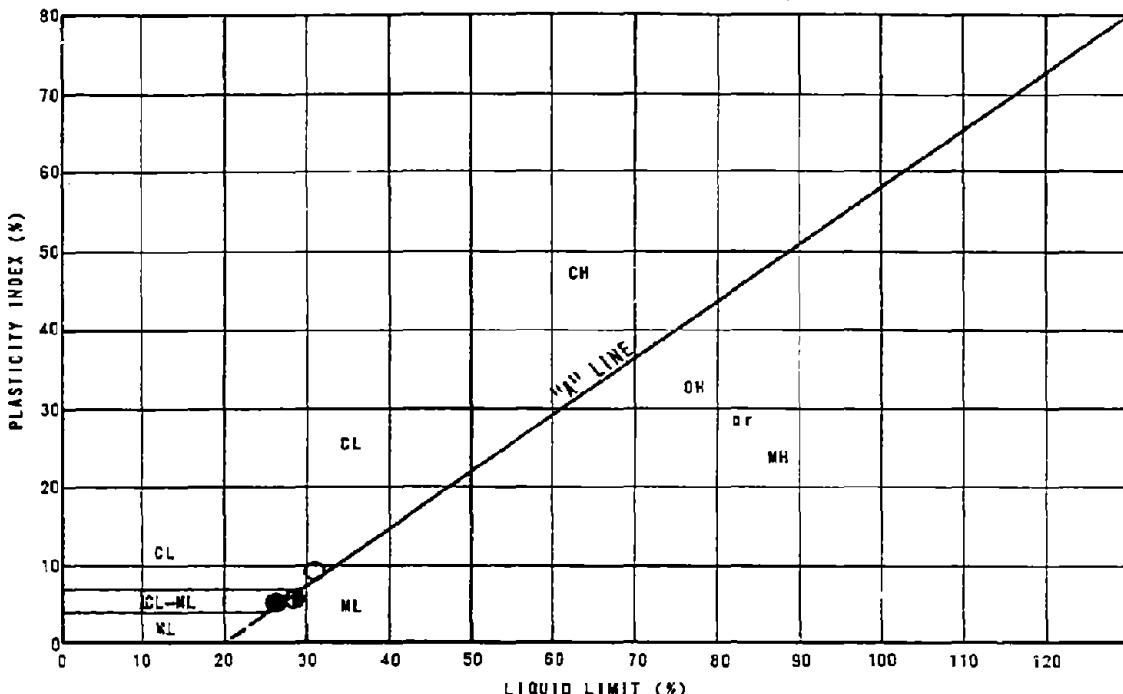


PLASTICITY DATA

KEY SYMBOL	HOLE NUMBER	DEPTH (feet)	NATURAL WATER CONTENT W (%)	PLASTIC LIMIT (%)	LIQUID LIMIT (%)	PLASTICITY INDEX (%)	LIQUIDITY INDEX ($\frac{W - PL}{LL - PL}$)	UNIFIED SOIL CLASSIFICATION SYMBOL
◎	10	60.2-62.5		23	23	0	---	SM
<hr/>								
W.A. WAHLER & ASSOCIATES		COAL REFUSE DAM FAILURE Saunders, W. Va.			ATTERBERG LIMITS - PLASTICITY DATA			
					PROJECT NO.	DATE	DRAWING NO.	
		PALO ALTO • NEWPORT BEACH • CALIF.			0700	OCTOBER 1972	B-3	



PLASTICITY CHART



PLASTICITY DATA

KEY SYMBOL	HOLE NUMBER	DEPTH (feet)	NATURAL WATER CONTENT W (%)	PLASTIC LIMIT (%)	Liquid Limit (%)	PLASTICITY INDEX (%)	LIQUIDITY INDEX (W - PL / IL - PL)	UNIFIED SOIL CLASSIFICATION SYMBOL
○	FD-14A	5.0	9.3	—	—	N.P.		SP-SM
	FD-18A	10.0	11.4	—	—	N.P.		SP-SM
	FD-23A	35.0	8.9	—	—	N.P.		GP-CM
	FD-24A	22.0	11.1	22	31	9		SC
	FD-25A	17.0	14.3	—	—	N.P.		SP-SM
	FD-27A	7.0	7.4	22	27	5		GW-GM
	FD-28A	2.0	6.4	22	28	6		SW-SM
W.A. WAHLER & ASSOCIATES		COAL REFUSE DAM FAILURE Saunders, W. Va. PALO ALTO • NEWPORT BEACH • CALIF.			ATTERBERG LIMITS - PLASTICITY DATA			
					PROJECT NO.	DATE	DRAWING NO.	
					0700	MAY 1972	B-3	

710-3

FIGURE B-4
SUMMARY
OF
SPECIFIC GRAVITY TEST RESULTS

HOLE NO.	SAMPLE NO.	DEPTH (ft)	MATERIAL TYPE	MINUS NO. 4 SPECIFIC GRAVITY	PLUS 3/4 ¹¹ SPECIFIC GRAVITY
2	S-4	23.0-25.0	EMBANKMENT, DAM NO. 3	1.70	---
4	S-6	30.0-32.0	EMBANKMENT, DAM NO. 2	2.32	---
4	S-7	35.0-37.0	EMBANKMENT, DAM NO. 2	1.87	---
4	S-12	68.0-70.0	FOUNDATION, POOL 1 SLUDGE	1.37	---
4	S-13	70.0-72.0	FOUNDATION, POOL 1 SLUDGE	1.40	---
4	PST-5	75.0-77.0	FOUNDATION, POOL 1 SLUDGE	1.46*	---
4	PST-5	75.0-77.0	FOUNDATION, POOL 1 SLUDGE	1.90*	---
5	S-5	65.0-67.0	FOUNDATION, POOL 1 SLUDGE	1.39	---
5	S-5	65.0-67.0	FOUNDATION, POOL 1 SLUDGE	1.37	---
7	S-2	20.0-22.0	EMBANKMENT, DAM NO. 3	1.70	---
7	S-5	50.0-52.0	FOUNDATION, POOL 2 SLUDGE	1.39	---
7	PST-1	55.0-56.3	FOUNDATION, POOL 2 SLUDGE	1.42	---
7	S-7	71.1-73.5	FOUNDATION, POOL 1 SLUDGE	1.42	---
8	PST-2	55.0-57.0	FOUNDATION, POOL 2 SLUDGE	1.34	---
9	SS-2A	55.0-57.0	FOUNDATION, POOL 2 SLUDGE	1.45	---
9	SS-2B	57.0-59.0	FOUNDATION, POOL 2 SLUDGE	1.39	---
10	S-9	60.7-62.7	MIXED EMBANKMENT AND SLUDGE	1.52	---
10	S-13	77.0-78.5	FOUNDATION, POOL 1 SLUDGE	1.81*	---
10	S-14	80.0-81.6	FOUNDATION, POOL 1 SLUDGE	1.77*	---
10	S-14	80.0-81.6	FOUNDATION, POOL 1 SLUDGE	1.83*	---
11	PST-1	35.0-37.0	EMBANKMENT, DAM NO. 3	2.24	---
11	SS-3A	85.0-87.0	FOUNDATION, POOL 1 SLUDGE	1.66	---
13	S-3	30.0-32.0	GOB PILE, COARSE COAL WASTE	2.14	---
FP-10A	S-2	3.5-4.5	EMBANKMENT, DAM NO. 3	1.66	---
FP-12A	S-1	4.8-6.8	EMBANKMENT, DAM NO. 3	2.23	---
FP-14A	S-2	3.5-4.5	EMBANKMENT, DAM NO. 3	1.62	---
	FD-1	0.5	EMBANKMENT, DAM NO. 3	---	2.34
	FD-3	0.5	EMBANKMENT, DAM NO. 3	---	1.75
	FD-4	0.5	EMBANKMENT, DAM NO. 3	1.75	1.68
	FD-9	1.5	GOB PILE, COARSE COAL WASTE	1.80	2.55
	FD-10	0.5	DISTURBED POOL 2 SLUDGE	1.38	----
	FD-11	0.3	NATURAL SOIL	2.58	2.66
	FD-12	1.0	EMBANKMENT, DAM NO. 1	2.43	----
	FD-1A	0	FOUNDATION, POOL 4 SLUDGE	1.52	----
	FD-3A	1.0	EMBANKMENT, DAM NO. 4	2.07	2.35
	FD-5A	1.0	EMBANKMENT, DAM NO. 3	1.85	2.12

* QUESTIONABLE DATA DUE TO HIGH OVEN TEMPERATURE. THESE DATA WERE NOT INCLUDED IN THE DETERMINATION OF AVERAGE SPECIFIC GRAVITY.

W.A. WAHLER
& ASSOCIATES

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FIGURE B-4
Sheet 1 of 2

FIGURE B-4 — CONTINUED
SUMMARY
OF
SPECIFIC GRAVITY TEST RESULTS

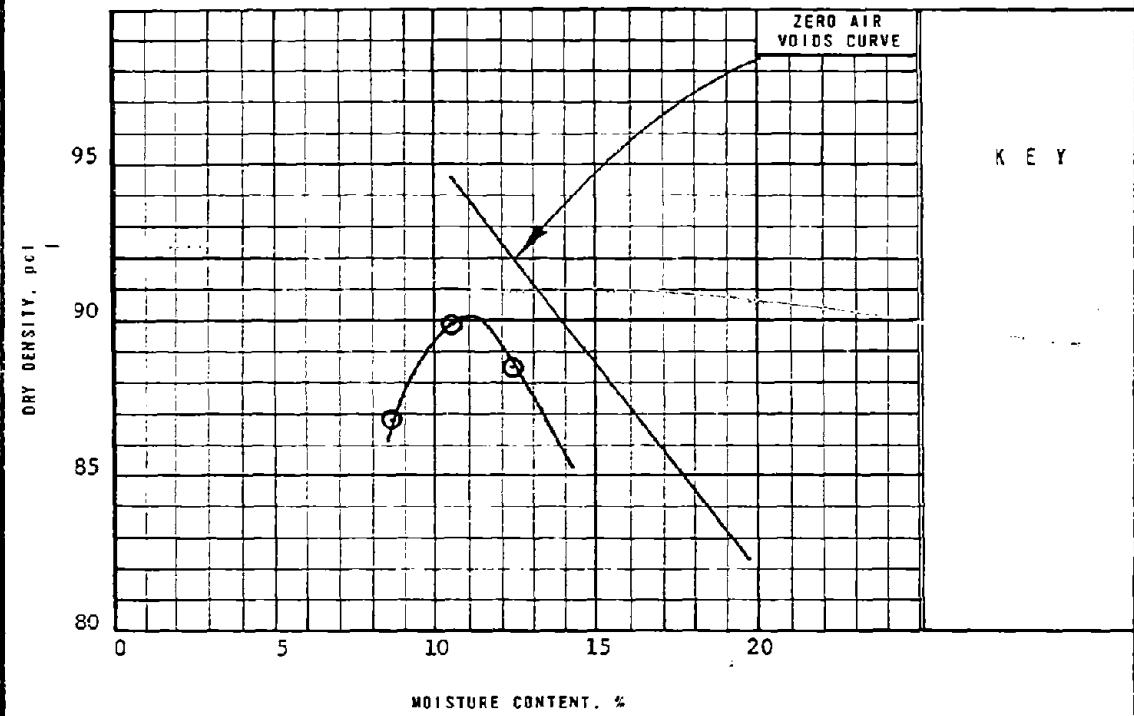
HOLE NO.	SAMPLE NO.	DEPTH (ft)	MATERIAL TYPE	MINUS NO. 4 SPECIFIC GRAVITY	PLUS 3/4" SPECIFIC GRAVITY
	FD-10A	3.9	EMBANKMENT, DAM NO. 3	2.20	2.06
	FD-14A	5.0	EMBANKMENT, DAM NO. 3	1.91	2.24
	FD-18A	35.0	EMBANKMENT, DAM NO. 3	1.32	2.02
	FD-23A	10.0	EMBANKMENT, DAM NO. 3	1.66	1.98
	FD-24A	22.0	EMBANKMENT, DAM NO. 3	1.85	----
	FD-25A	17.0	EMBANKMENT, DAM NO. 3	2.07	----
	FD-27A	7.0	EMBANKMENT, DAM NO. 3	1.98	2.51
	FD-28A	2.0	EMBANKMENT, DAM NO. 3	1.86	2.28
	A-1	COMBINED SAMPLE	EMBANKMENT, DAM NO. 3	1.90	1.84

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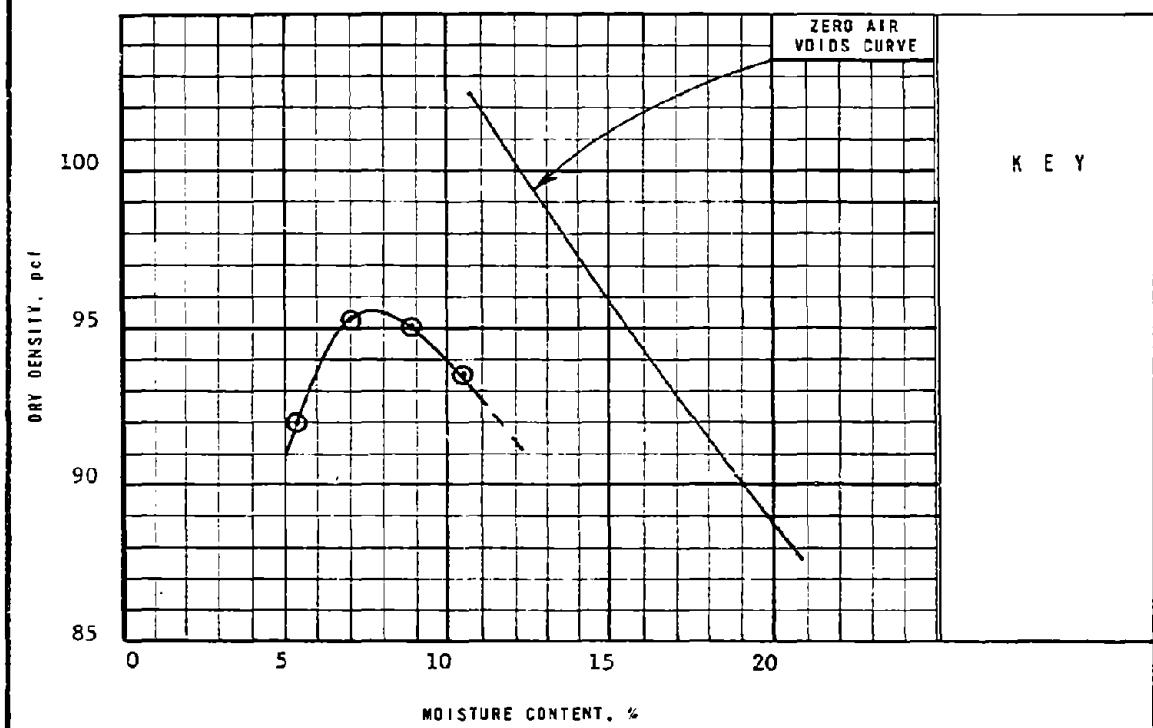
FIGURE B-4
Sheet 2 of 2

SAMPLE NO.	HOLE NO.	DEPTH (ft)	SAMPLE DESCRIPTION	SPECIFIC GRAVITY	LIQUID LIMIT (%)	PLASTIC LIMIT (%)	PERCENT PASSING	
							3/4"	No. 4
FD-4		0.5	Dark gray, silty SAND (SM)	1.75		NP	80	65



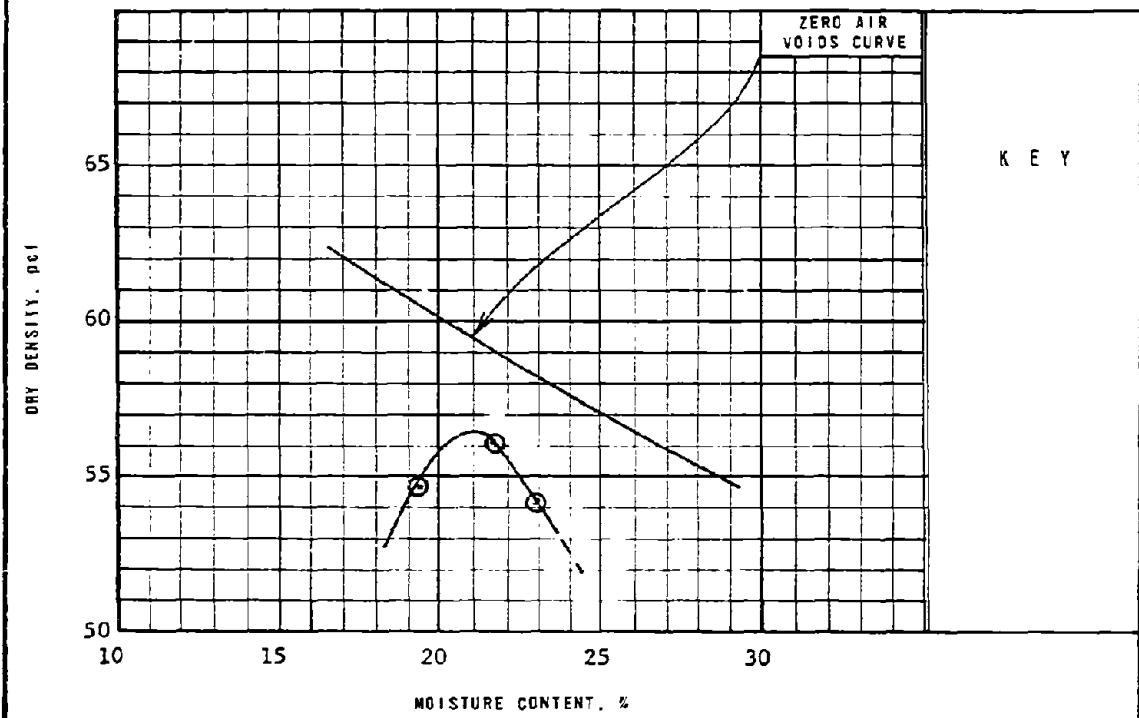
SAMPLE NO		FD-4		
NATURAL WATER CONTENT, %		7.6		
OPTIMUM WATER CONTENT, %		11.0		
MAXIMUM DRY DENSITY, pcf		90.3		
ASTM TEST DESIGNATION COMPACTIVE ENERGY ft.lb/ft ³		D-1557-70 20,000		
W.A. WAHLER & ASSOCIATES		COAL REFUSE DAM FAILURE Saunders, W. Va. PALO ALTO - NEWPORT BEACH - CALIF.	COMPACTION TEST RESULTS	
			PROJECT NO.	DATE
			0700	MAY 1972
				DRAWING NO.
				B-5

SAMPLE NO.	HOLE NO	DEPTH (ft)	SAMPLE DESCRIPTION	SPECIFIC GRAVITY	LIQUID LIMIT (%)	PLASTIC LIMIT (%)	PERCENT PASSING	
							3/4"	No. 4
FD-9		1.5	Dark gray, silty SAND (SM)	1.80		NP	81	65



SAMPLE NO	FD-9		
NATURAL WATER CONTENT, %	7.6		
OPTIMUM WATER CONTENT, %	7.5		
MAXIMUM DRY DENSITY, pcf	95.5		
ASTM TEST DESIGNATION COMPACTIVE ENERGY ft.lb/ft ³	D-1557-70 20,000		
W.A. WAHLER & ASSOCIATES 805-2	COAL REFUSE DAM FAILURE Saunders, W. Va. PALO ALTO - NEWPORT BEACH - CALIF.	COMPACTION TEST RESULTS	
		PROJECT NO.	DATE
		0700	MAY 1972
			B-5

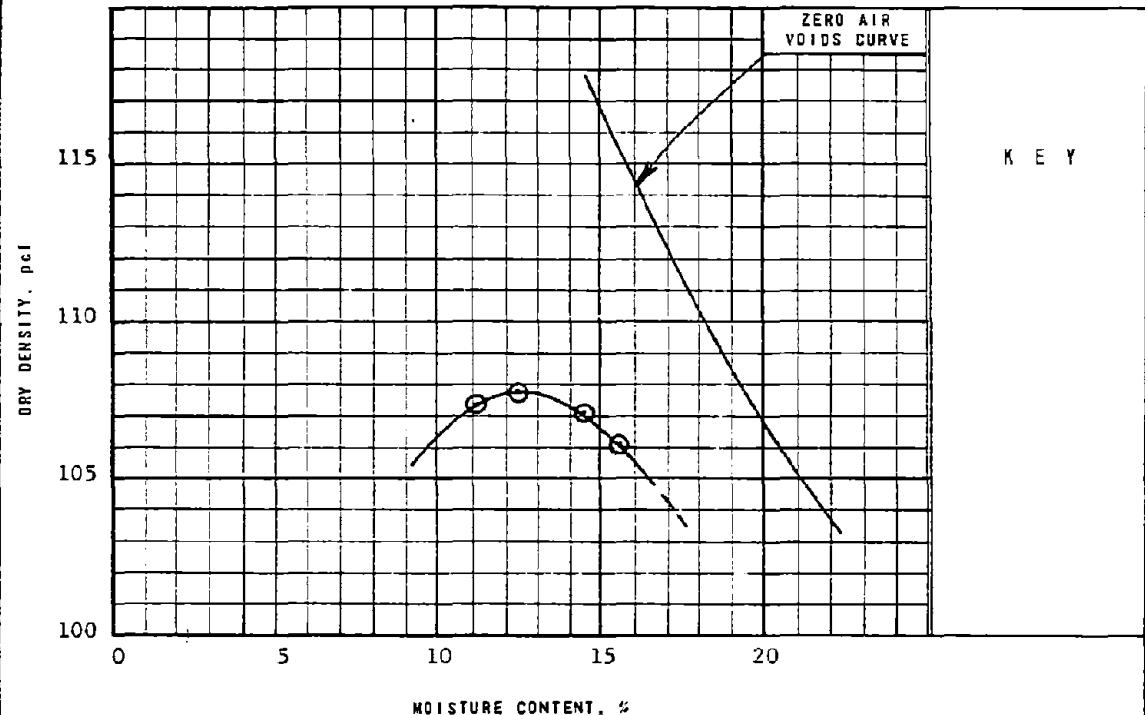
SAMPLE NO.	HOLE NO	DEPTH (ft)	SAMPLE DESCRIPTION	SPECIFIC GRAVITY	LIQUID LIMIT (%)	PLASTIC LIMIT (%)	PERCENT PASSING	
							3/4"	NO. 4
FD-10		0.5	Black, sandy SILT (SM/ML)	1.38		NP	100	99



SAMPLE NO	FD-10		
NATURAL WATER CONTENT, %	36.8		
OPTIMUM WATER CONTENT, %	21.0		
MAXIMUM DRY DENSITY, pcf	56.4		
ASTM TEST DESIGNATION COMPACTIVE ENERGY ft. lb/ft ³	D-1557-70 20,000		
W.A. WAHLER & ASSOCIATES	COAL REFUSE DAM FAILURE Saunders, W. Va. PALO ALTO • NEWPORT BEACH • CALIF.	COMPACTION TEST RESULTS	
		PROJECT NO.	DATE
		0700	MAY 1972
			D-5

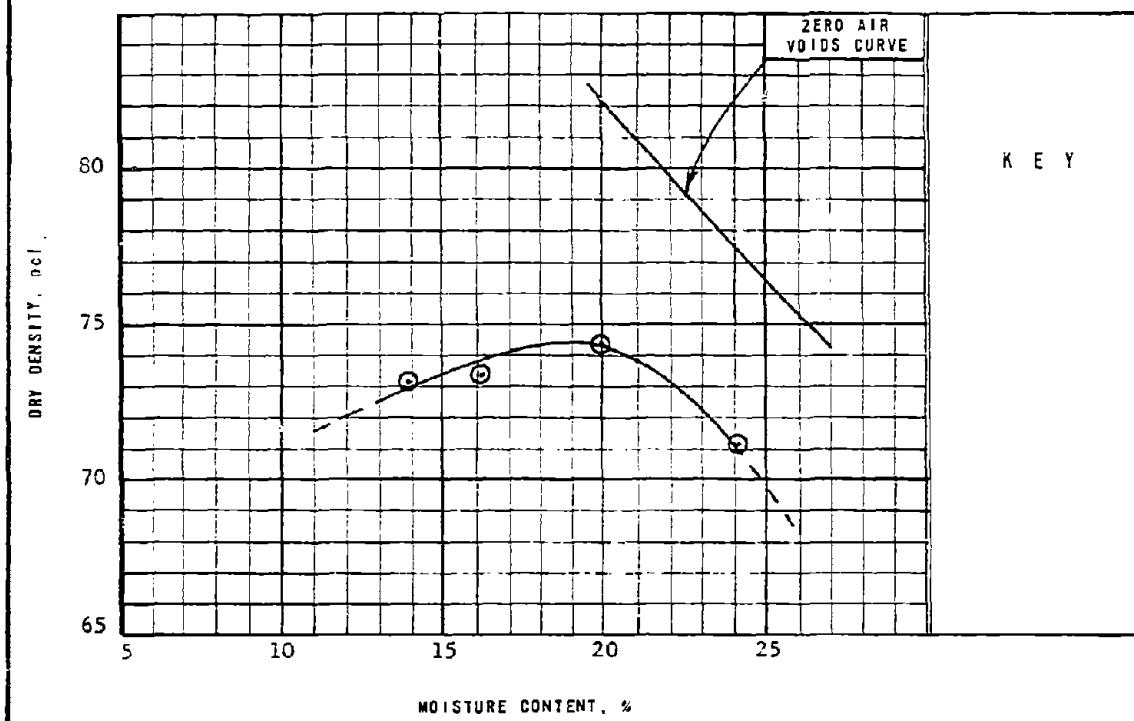
805-2

SAMPLE NO.	HOLE NO	DEPTH (ft)	SAMPLE DESCRIPTION	SPECIFIC GRAVITY	LIQUID LIMIT (%)	PLASTIC LIMIT (%)	PERCENT PASSING	
							3/4"	No. 4
FD-11		0.3	Light brown, gravelly, sandy SILT (ML/GM)	2.58	40	28	73	60



SAMPLE NO	FD-11		
NATURAL WATER CONTENT. %	20.7		
OPTIMUM WATER CONTENT. %	12.5		
MAXIMUM DRY DENSITY. pcf	107.8		
ASTM TEST DESIGNATION COMPACTIVE ENERGY ft. lb/ft ³	D-1557-70 20,000		
W. A. WAHLER & ASSOCIATES	COAL REFUSE DAM FAILURE Saunders, W. Va. PALO ALTO - NEWPORT BEACH - CALIF.	COMPACTION TEST RESULTS	
		PROJECT NO.	DATE
		0700	MAY 1972
			DRAWING NO.
			B-5

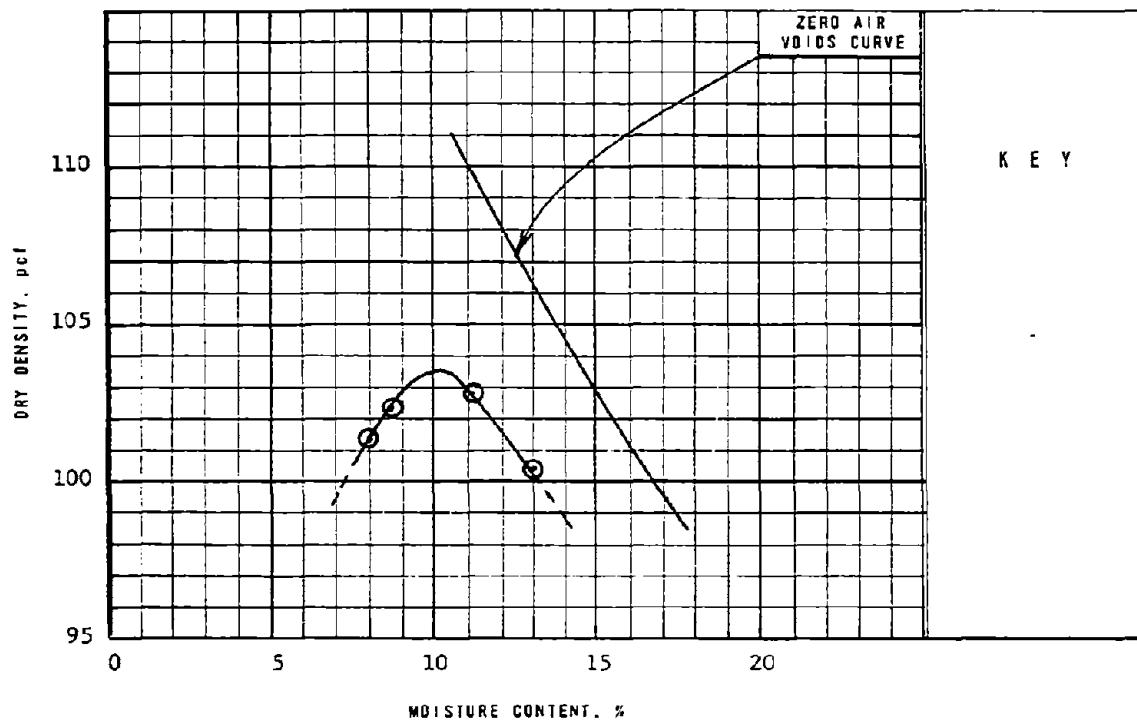
SAMPLE NO.	HOLE NO.	DEPTH (ft.)	SAMPLE DESCRIPTION	SPECIFIC GRAVITY	LIQUID LIMIT (%)	PLASTIC LIMIT (%)	PERCENT PASSING	
							3/4"	NO. 4
FD-1A		0	Black, silty SAND (SM)	1.52		NP	100	99



SAMPLE NO	FD-1A		
NATURAL WATER CONTENT, %	32.1		
OPTIMUM WATER CONTENT, %	19.0		
MAXIMUM DRY DENSITY, pcf	74.4		
ASTM TEST DESIGNATION COMPACTIVE ENERGY ft.lb/ft ³	D-1557-70 20,000		
W. A. WAHLER & ASSOCIATES	COAL REFUSE DAM FAILURE Saunders, W. Va. PALO ALTO • NEWPORT BEACH • CALIF.	COMPACTION TEST RESULTS	
		PROJECT NO.	DATE
	0700	MAY 1972	B-3

SAMPLE NO.	HOLE NO.	DEPTH (ft)	SAMPLE DESCRIPTION	SPECIFIC GRAVITY	LIQUID LIMIT (%)	PLASTIC LIMIT (%)	PERCENT PASSING	
							3/4"	No. 4
FD-3A		1.0	Light gray, silty GRAVEL (GP-GM)	2.07		NP	72	41

Combined sample of FD-3A and FD-4A.

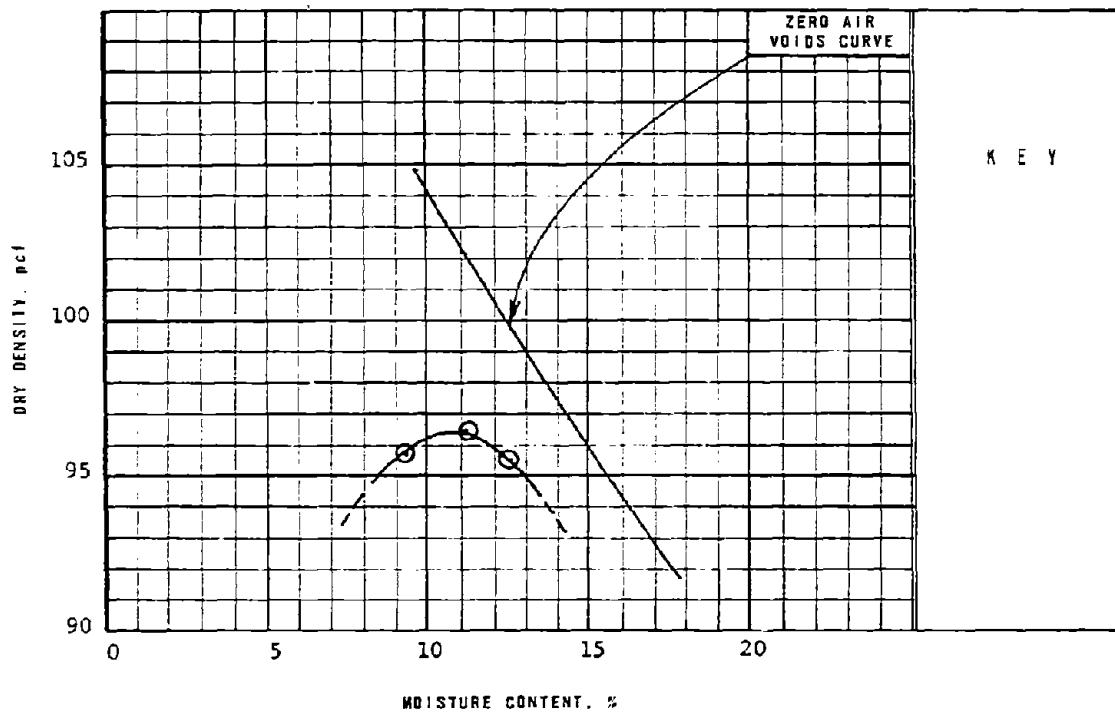


SAMPLE NO	FD-3A		
NATURAL WATER CONTENT. %	7.5		
OPTIMUM WATER CONTENT. %	10.0		
MAXIMUM DRY DENSITY. pcf	103.4		
ASTM TEST DESIGNATION COMPACTIVE ENERGY ft.lb/ft ³	D-1557-70 20,000		

805-2 W.A. WAHLER & ASSOCIATES	COAL REFUSE DAM FAILURE Saunders, W. Va. PALO ALTO • NEWPORT BEACH • CALIF.	COMPACTION TEST RESULTS		
		PROJECT NO.	DATE	DRAWING NO.
		0700	MAY 1972	D-5

SAMPLE NO.	HOLE NO.	DEPTH (ft)	SAMPLE DESCRIPTION	SPECIFIC GRAVITY	LIQUID LIMIT (%)	PLASTIC LIMIT (%)	PERCENT PASSING	
							3/8"	No. 4
FD-5A		1.0	Light gray, silty SAND (SM)	1.85		NP	96	77

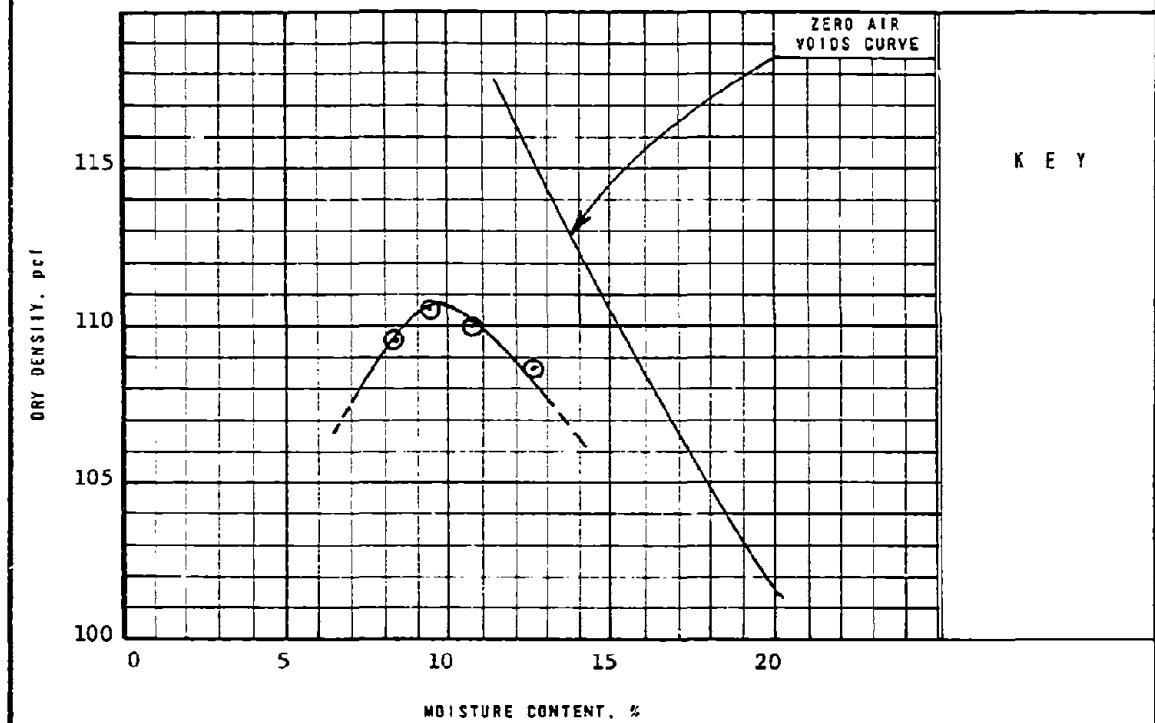
Combined sample from FD-5A and FD-6A.



SAMPLE NO	FD-5A		
NATURAL WATER CONTENT, %	5.5		
OPTIMUM WATER CONTENT, %	10.8		
MAXIMUM DRY DENSITY, pcf	96.5		
ASTM TEST DESIGNATION COMPACTIVE ENERGY ft-lb/ft ³	D-1557-70 20,000		
W.A. WAHLER & ASSOCIATES	COAL REFUSE DAM FAILURE Saunders, W. Va. PALO ALTO - NEWPORT BEACH - CALIF.	COMPACTIATION TEST RESULTS	
		PROJECT NO.	DATE
		0700	MAY 1972
			DRAWING NO. B-5

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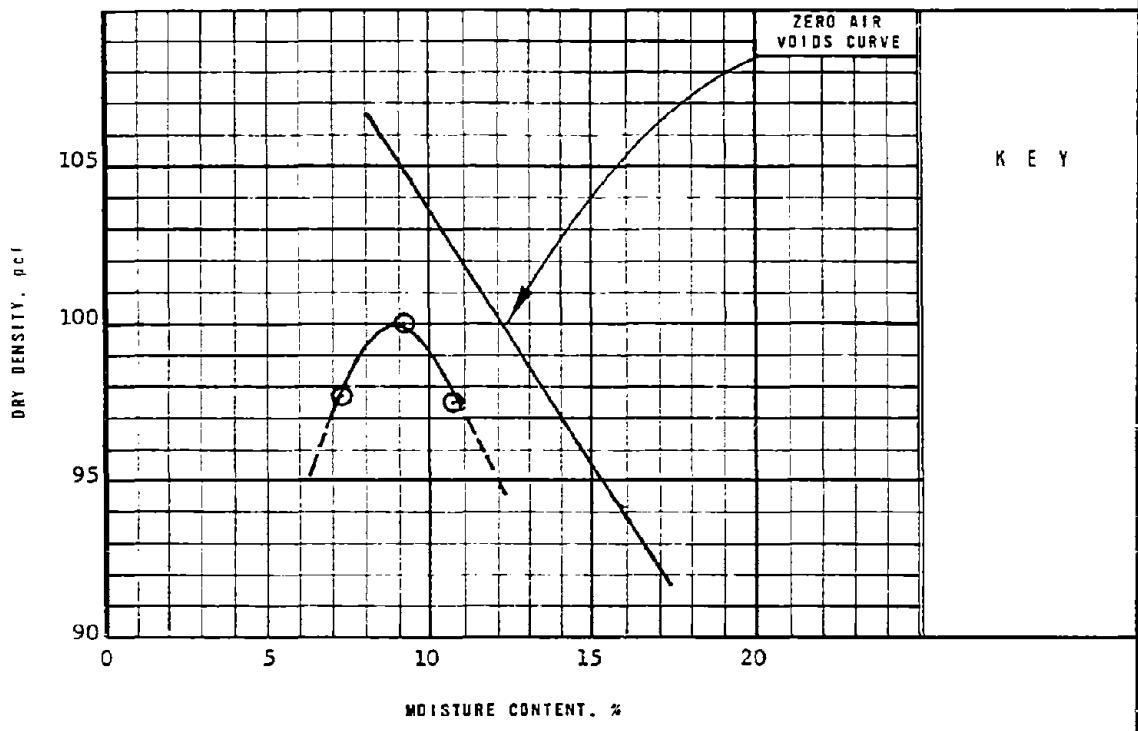
SAMPLE NO.	HOLE NO	DEPTH (ft)	SAMPLE DESCRIPTION	SPECIFIC GRAVITY	LIQUID LIMIT (%)	PLASTIC LIMIT (%)	PERCENT PASSING	
							3/4"	No. 4
FD-10A		5.8	Light gray, silty, sandy GRAVEL (GW-GM)	2.20		NP	81	40



SAMPLE NO		FD-10A		
NATURAL WATER CONTENT, %		3.9		
OPTIMUM WATER CONTENT, %		9.5		
MAXIMUM DRY DENSITY, pcf		110.7		
ASTM TEST DESIGNATION COMPACTIVE ENERGY ft.lb/fi ³		D-1557-70 20,000		
W. A. WAHLER & ASSOCIATES 605-2	COAL REFUSE DAM FAILURE Saunders, W. Va. PALO ALTO - NEWPORT BEACH - CALIF.		COMPACTION TEST RESULTS	
	PROJECT NO.	DATE	DRAWING NO.	
	0700	MAY 1972	B-5	

SAMPLE NO.	HOLE NO	DEPTH (ft)	SAMPLE DESCRIPTION	SPECIFIC GRAVITY	LIQUID LIMIT (%)	PLASTIC LIMIT (%)	PERCENT PASSING	
							3/4"	No. 4
FD-14A		9.3	Light gray, silty, gravelly SAND (SP-SM)	1.91		NP	84	62

Combined sample from FD-14A, FD-16A, and FD-17A.

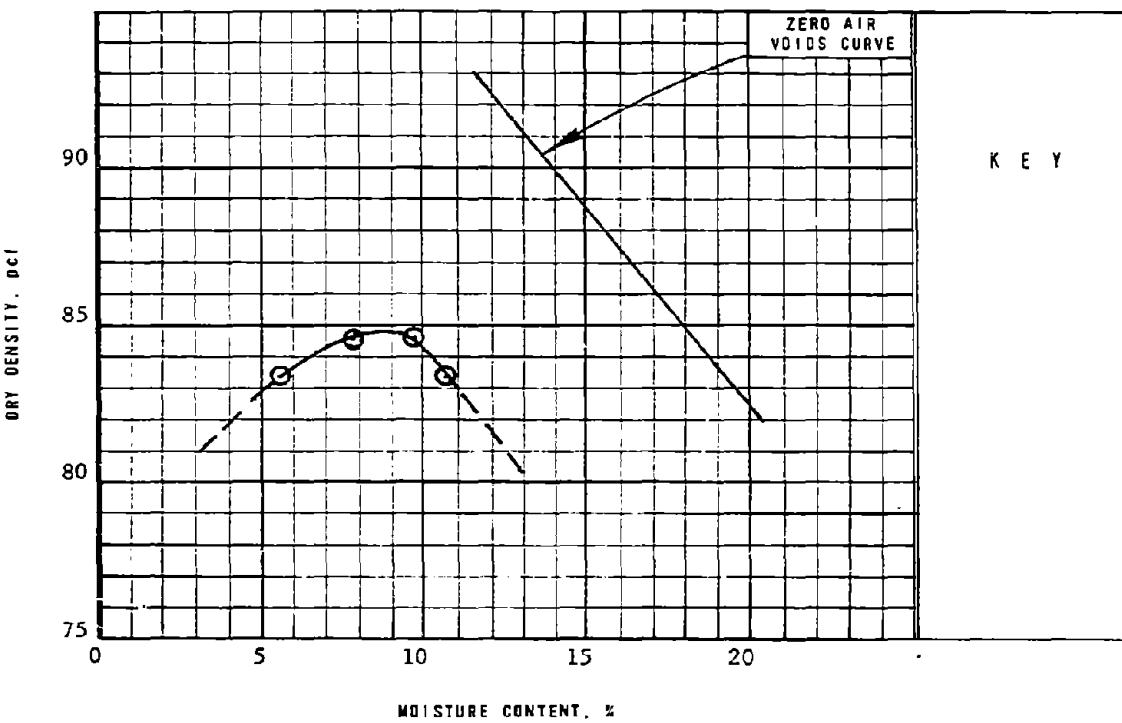


SAMPLE NO		FD-14A				
NATURAL WATER CONTENT, %		5.0				
OPTIMUM WATER CONTENT, %		9.0				
MAXIMUM DRY DENSITY, pcf		100.1				
ASTM TEST DESIGNATION COMPACTIVE ENERGY ft.lb/ft ³		D-1557-70 20,000				
W.A. WAHLER & ASSOCIATES		COAL REFUSE DAM FAILURE Saunders, W. Va. PALO ALTO - NEWPORT BEACH - CALIF.		COMPACTION TEST RESULTS		
				PROJECT NO.	DATE	DRAWING NO.
				0700	MAY 1972	B-5

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SAMPLE NO.	HOLE NO	DEPTH (ft)	SAMPLE DESCRIPTION	SPECIFIC GRAVITY	LIQUID LIMIT (%)	PLASTIC LIMIT (%)	PERCENT PASSING	
							3/4"	NO. 4
FD-18A		28.0	Light gray, silty, gravelly SAND (SP-SM)	1.32		NP	87	65

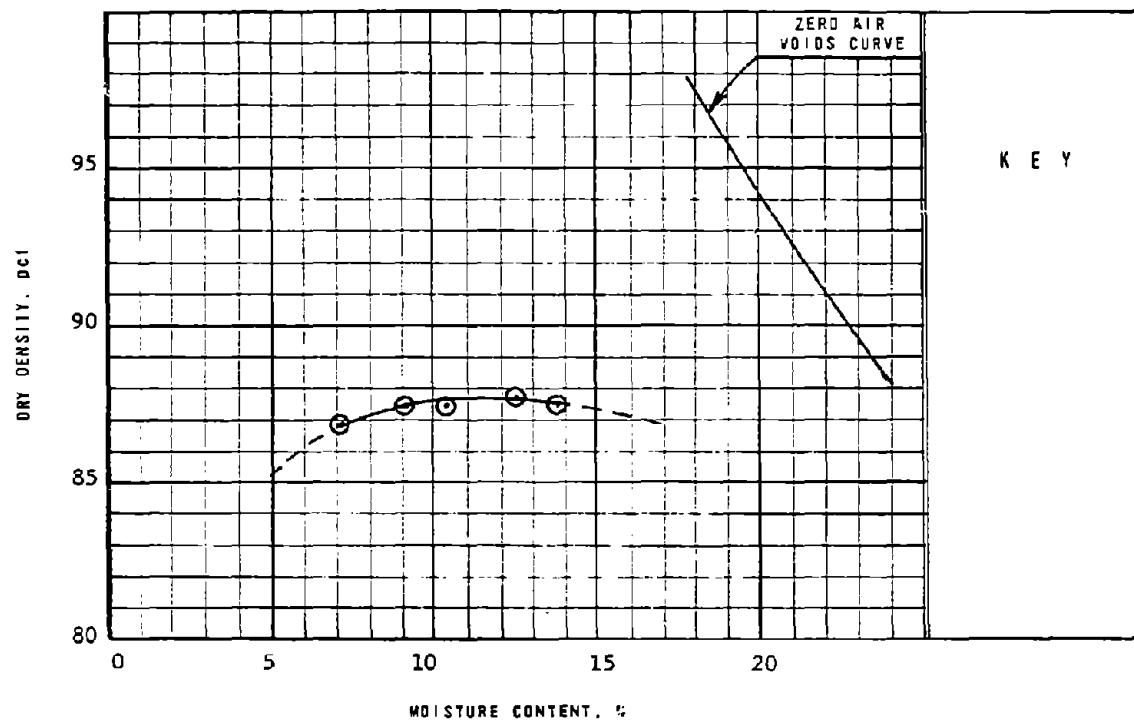
Combined sample of FD-18A, FD-20A, and FD-22A.



SAMPLE NO		FD-18A		
NATURAL WATER CONTENT, %		11.4		
OPTIMUM WATER CONTENT, %		9.0		
MAXIMUM DRY DENSITY, pcf		84.8		
ASTM TEST DESIGNATION COMPACTIVE ENERGY 11.1b/ft ³		D-1557-70 20,000		
W.A. WAHLER & ASSOCIATES 605-2	COAL REFUSE DAM FAILURE Saunders, W. Va. PALO ALTO - NEWPORT BEACH - CALIF.		COMPACTION TEST RESULTS	
	PROJECT NO.	0700	DATE	MAY 1972
			DRAWING NO.	B-3

SAMPLE NO.	HOLE NO	DEPTH (ft)	SAMPLE DESCRIPTION	SPECIFIC GRAVITY	LIQUID LIMIT (%)	PLASTIC LIMIT (%)	PERCENT PASSING	
							3/4"	NO. 4
FD-23A		18.0	Black, slightly silty, sandy GRAVEL (GP-GM)	1.66		NP	69	49

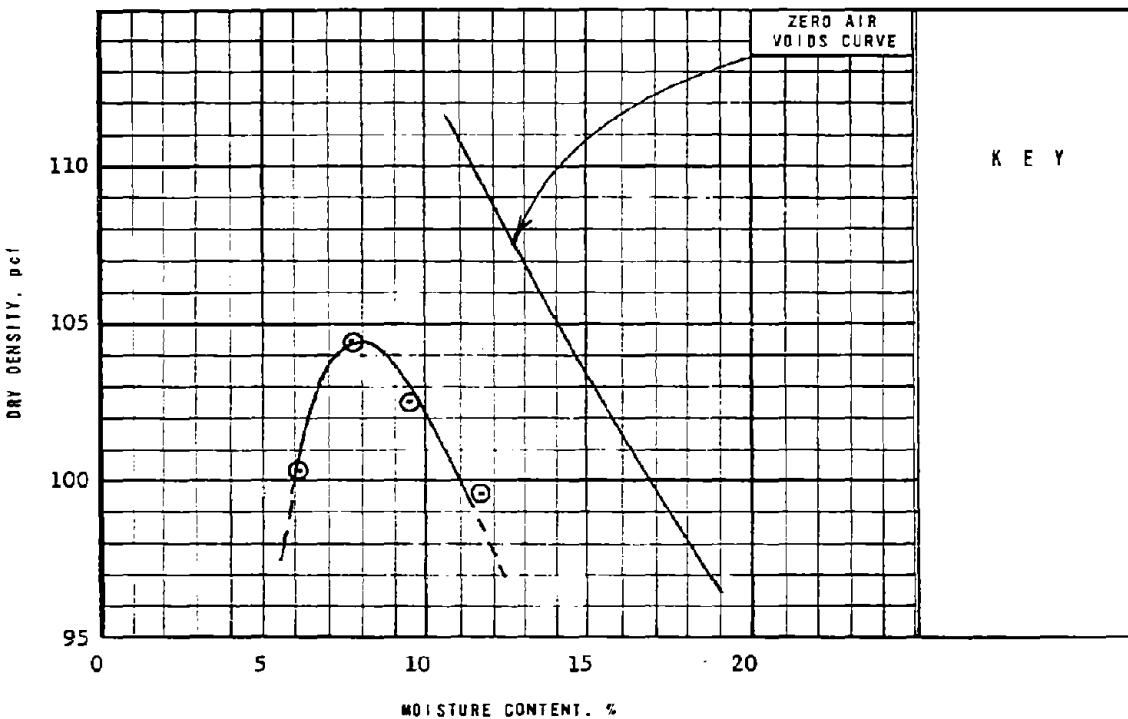
NOTE: Combined sample from FD-19A, FD-21A, and FD-23A.



SAMPLE NO	FD-23A		
NATURAL WATER CONTENT, %	8.9		
OPTIMUM WATER CONTENT, %	12.5		
MAXIMUM DRY DENSITY, pcf	87.8		
ASTM TEST DESIGNATION COMPACTIVE ENERGY ft. lb/ft ³	D-1557-70 20,000		
W.A. WALTER & ASSOCIATES	COAL REFUSE DAY FAILURE Saunders, W. Va. PALO ALTO - NEWPORT BEACH - CALIF.	COMPACTION TEST RESULTS	
		PROJECT NO.	DATE
		0700	May 1972
			DRAWING NO.
			B-5

SAMPLE NO.	HOLE NO	DEPTH (ft)	SAMPLE DESCRIPTION	SPECIFIC GRAVITY	LIQUID LIMIT (%)	PLASTIC LIMIT (%)	PERCENT PASSING	
							3/4"	NO. 4
FD-27A		7.0	Light gray, well graded, silty GRAVEL (GW-GM)	1.98	27	22	92	62

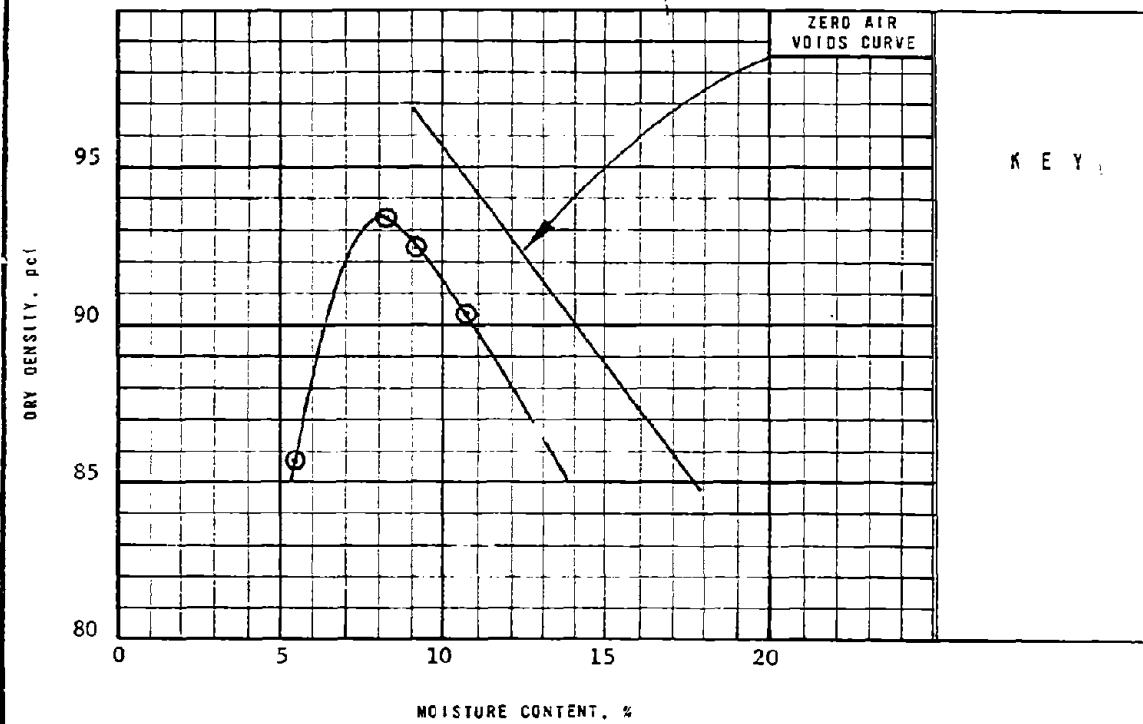
NOTE: Combined sample from FD-26A and FD-27A.



SAMPLE NO		FD-27A				
NATURAL WATER CONTENT, %		7.4				
OPTIMUM WATER CONTENT, %		8.0				
MAXIMUM DRY DENSITY, pcf		104.4				
ASTM TEST DESIGNATION COMPACTIVE ENERGY ft.lb/ft ³		D1557-70 20,000				
W.A. WAHLER & ASSOCIATES		COAL REFUSE DAM FAILURE Saunders, W. Va. PALO ALTO - NEWPORT BEACH - CALIF.		COMPACTION TEST RESULTS		
				PROJECT NO.	DATE	DRAWING NO.
				0700	MAY 1972	B-5

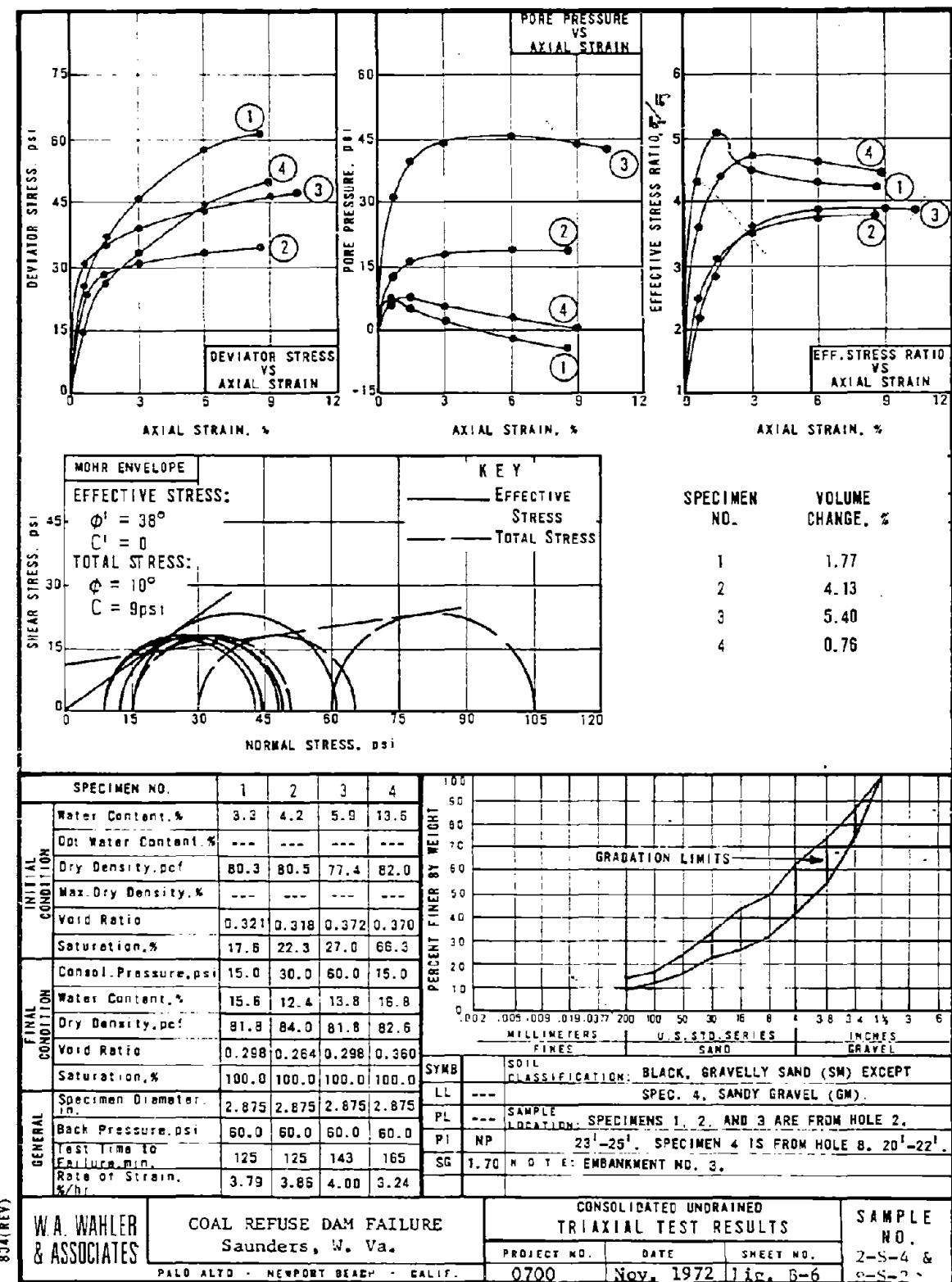
Sheet 12 of 13

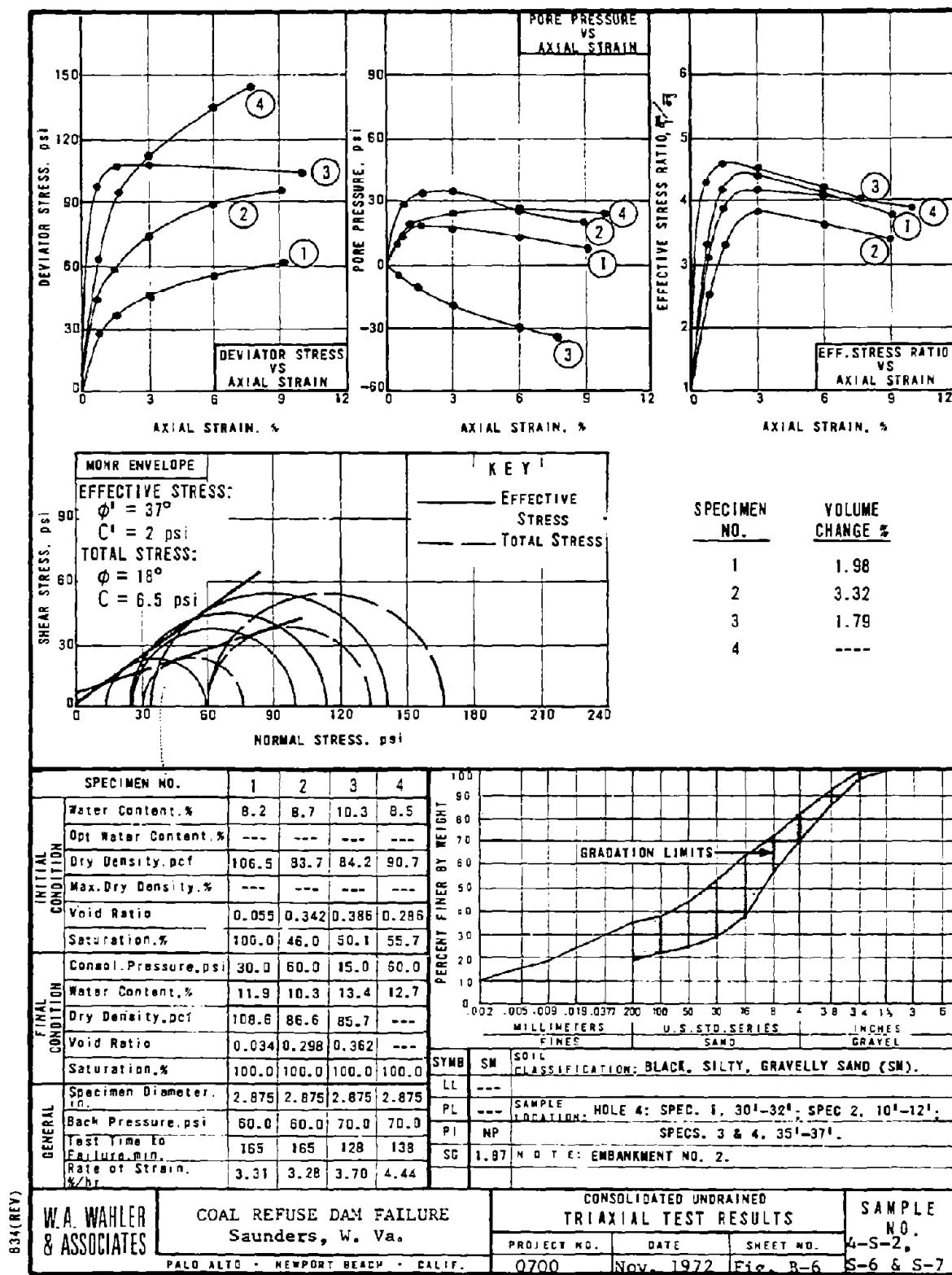
SAMPLE NO.	HOLE NO	DEPTH (ft)	SAMPLE DESCRIPTION	SPECIFIC GRAVITY	LIQUID LIMIT (%)	PLASTIC LIMIT (%)	PERCENT PASSING	
							3/4"	No. 4
FD-28A		2.0	Light gray, well graded, silty, gravelly SAND (SW-SM)	1.86	28	22	78	47



SAMPLE NO	FD-28A		
NATURAL WATER CONTENT, %	6.4		
OPTIMUM WATER CONTENT, %	8.2		
MAXIMUM DRY DENSITY, pcf	98.4		
ASTM TEST DESIGNATION COMPACTIVE ENERGY ft. lb/ft ³	D-1557-70 20,000		
W.A. WAHLER & ASSOCIATES	COAL REFUSE DAM FAILURE Saunders, W. Va. PALO ALTO - NEWPORT BEACH - CALIF.	COMPACTION TEST RESULTS	
		PROJECT NO.	DATE
		0700	MAY 1972
			DRAWING NO B-5

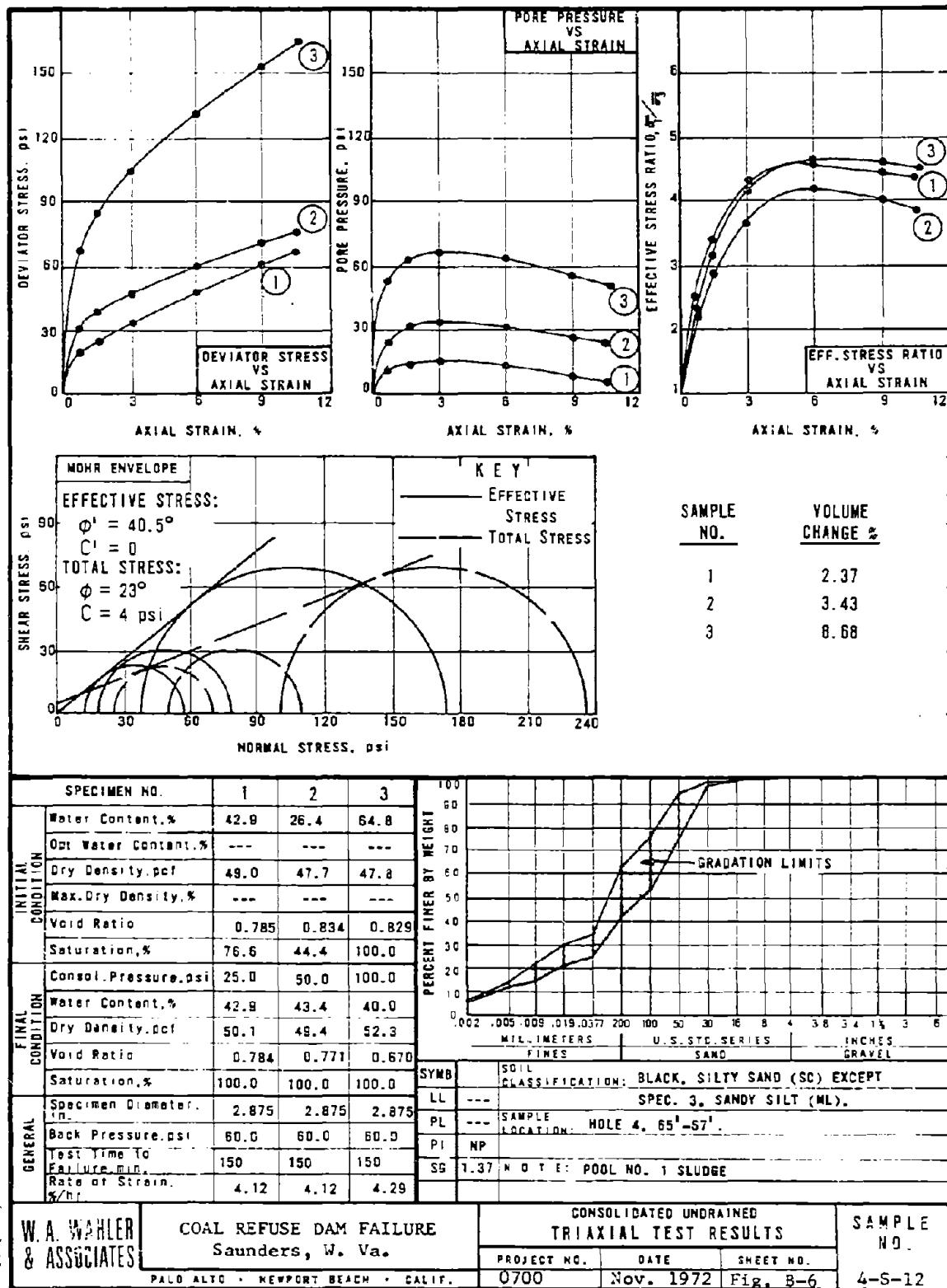
805-2

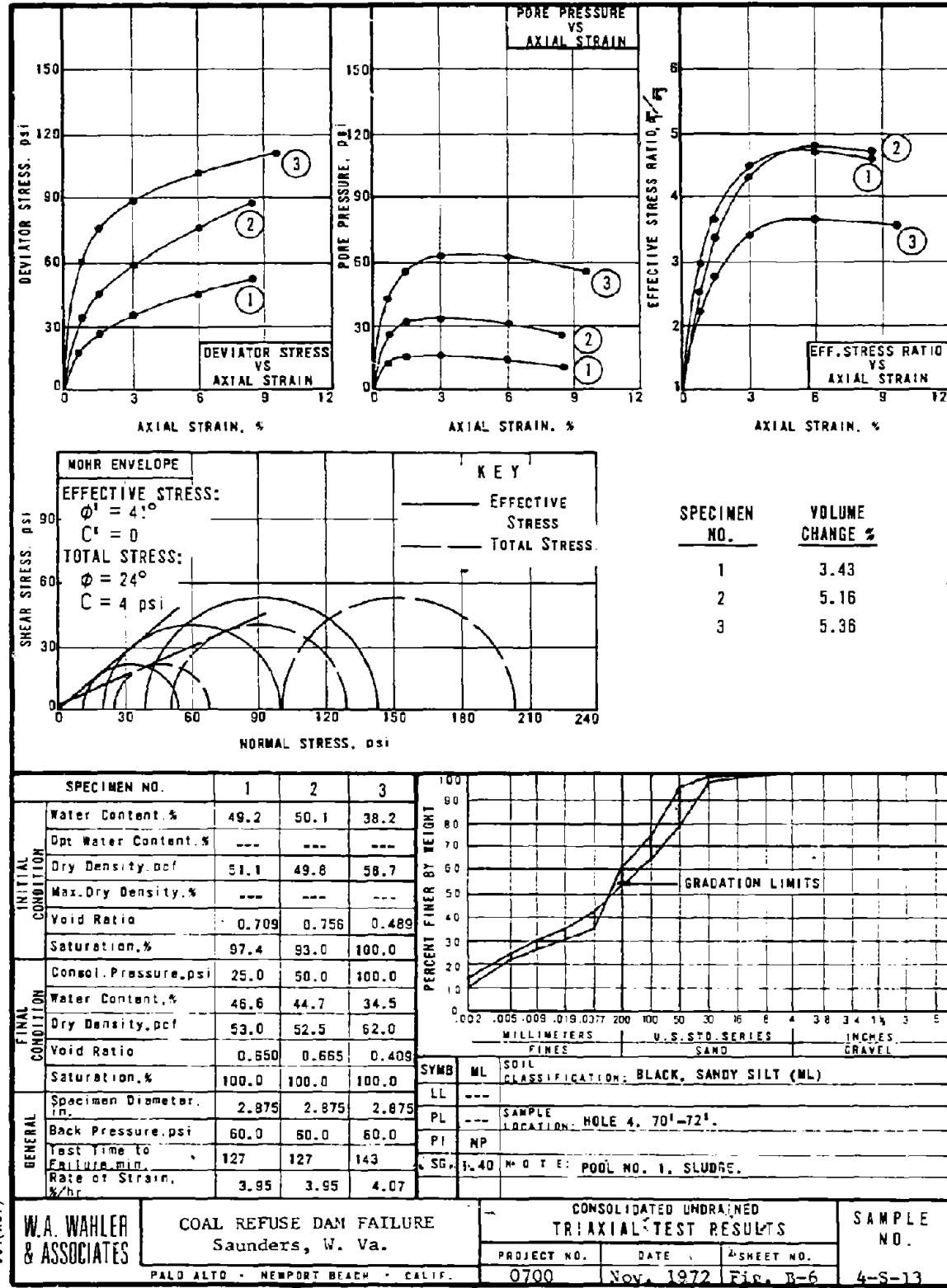


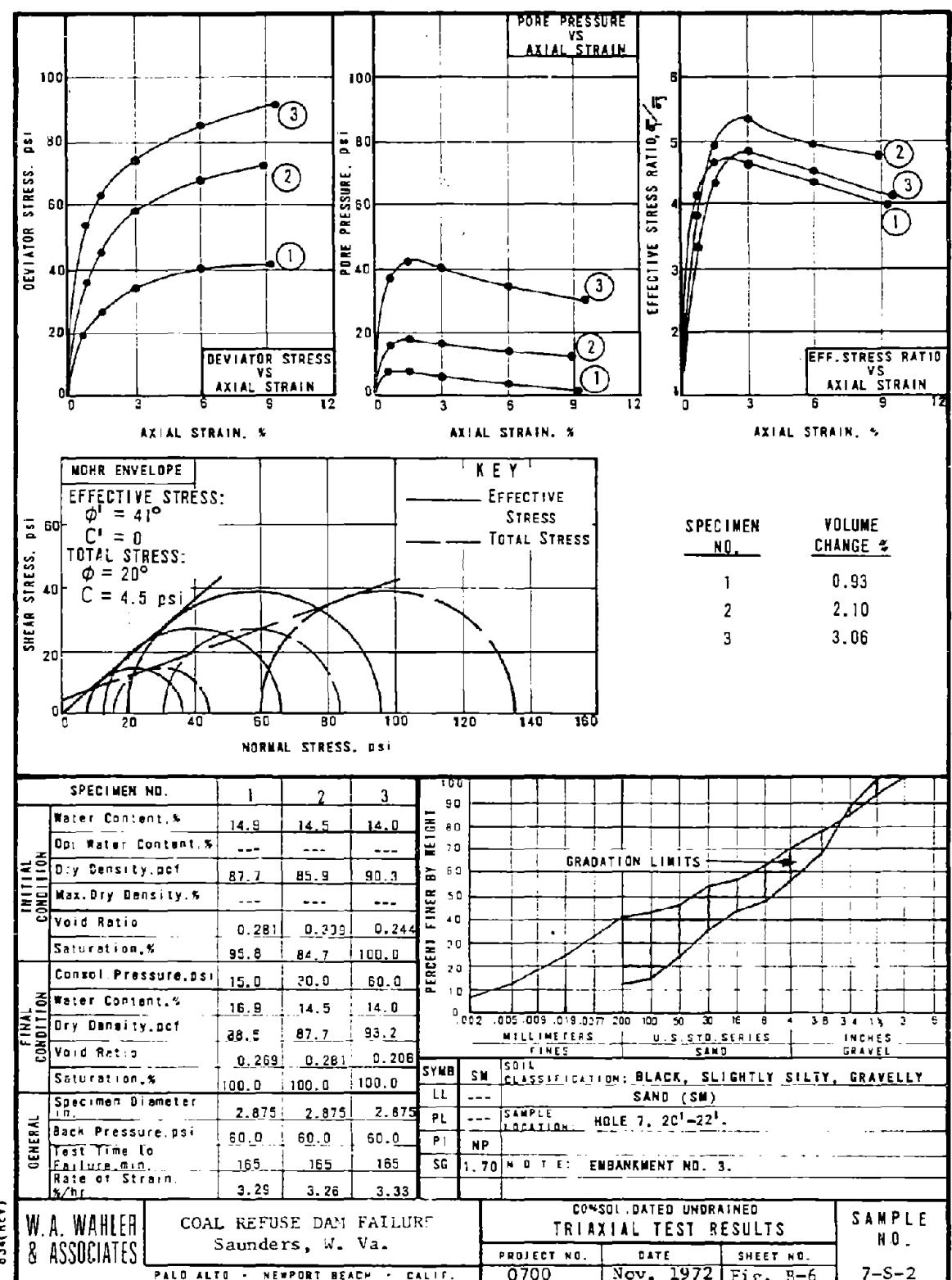


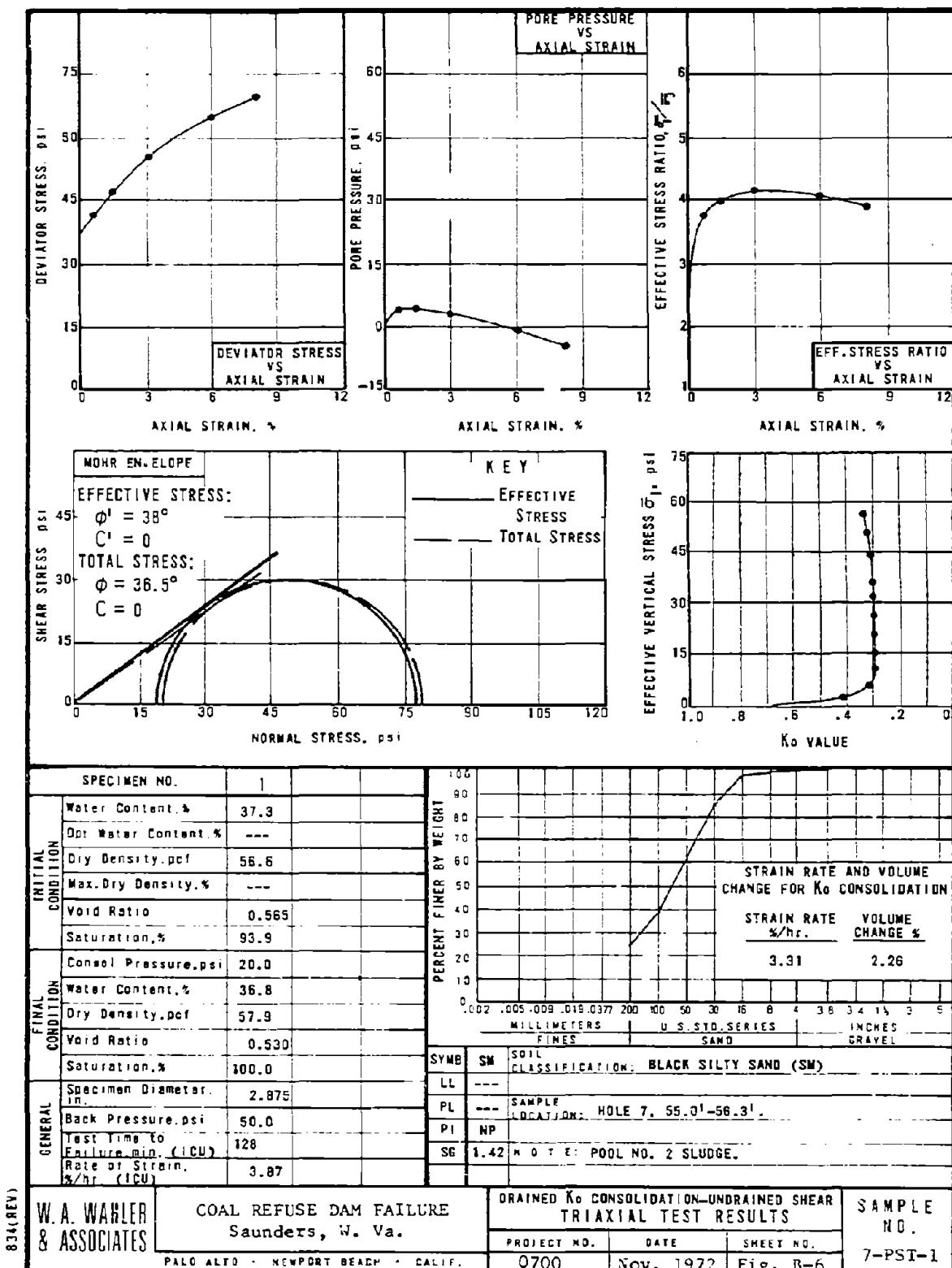
B34 (REV.)

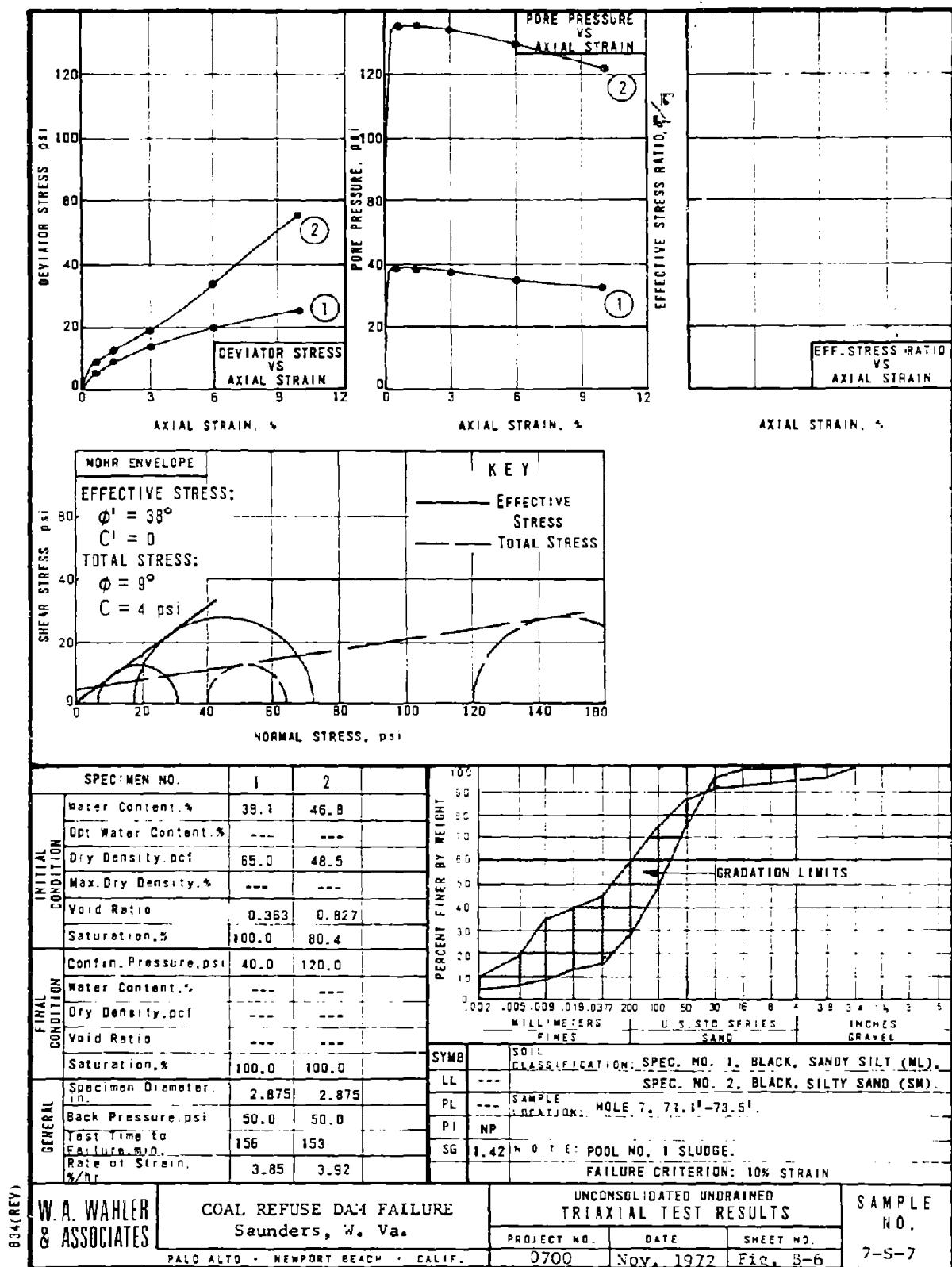
Sheet 2 of 15

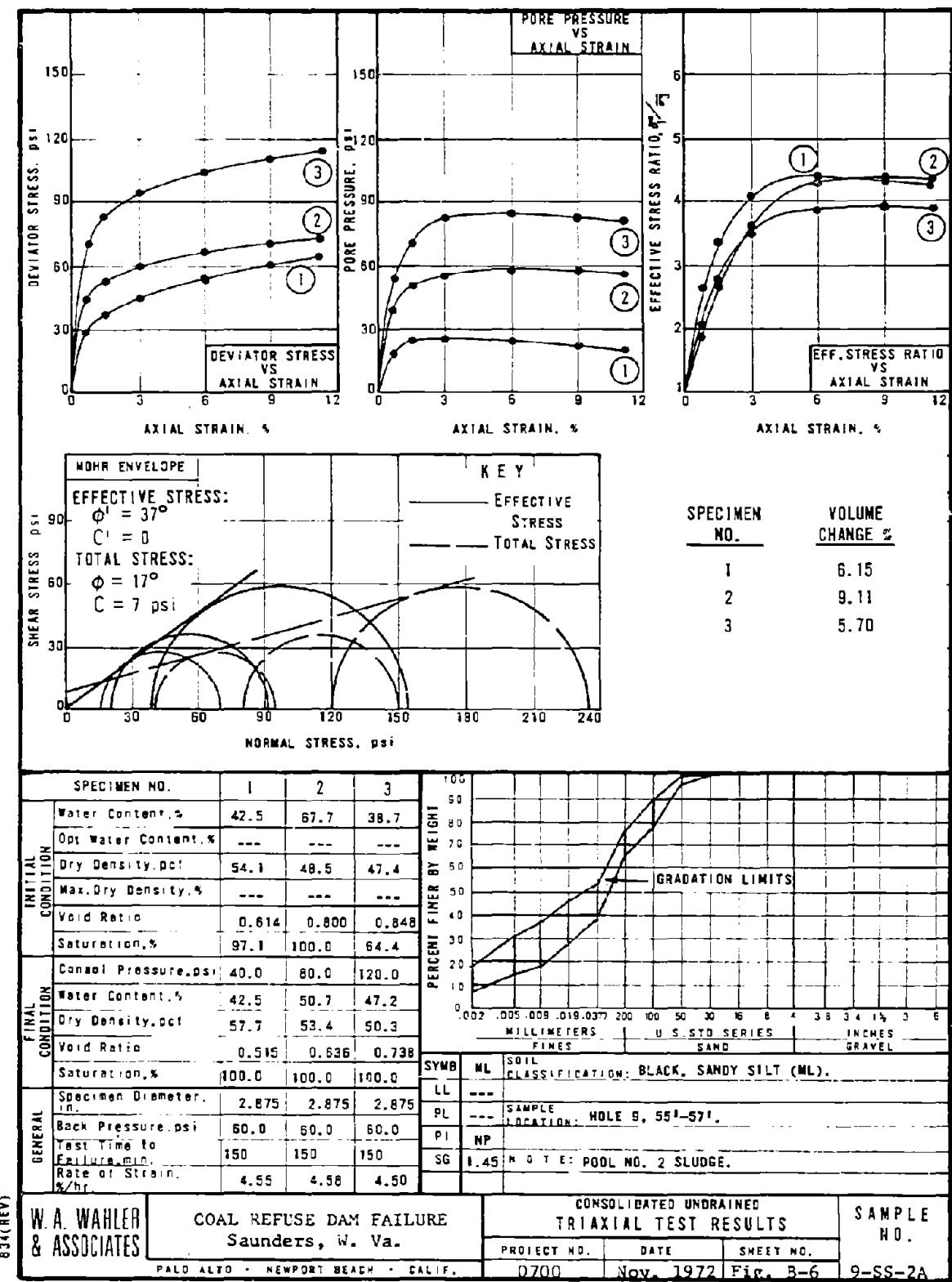


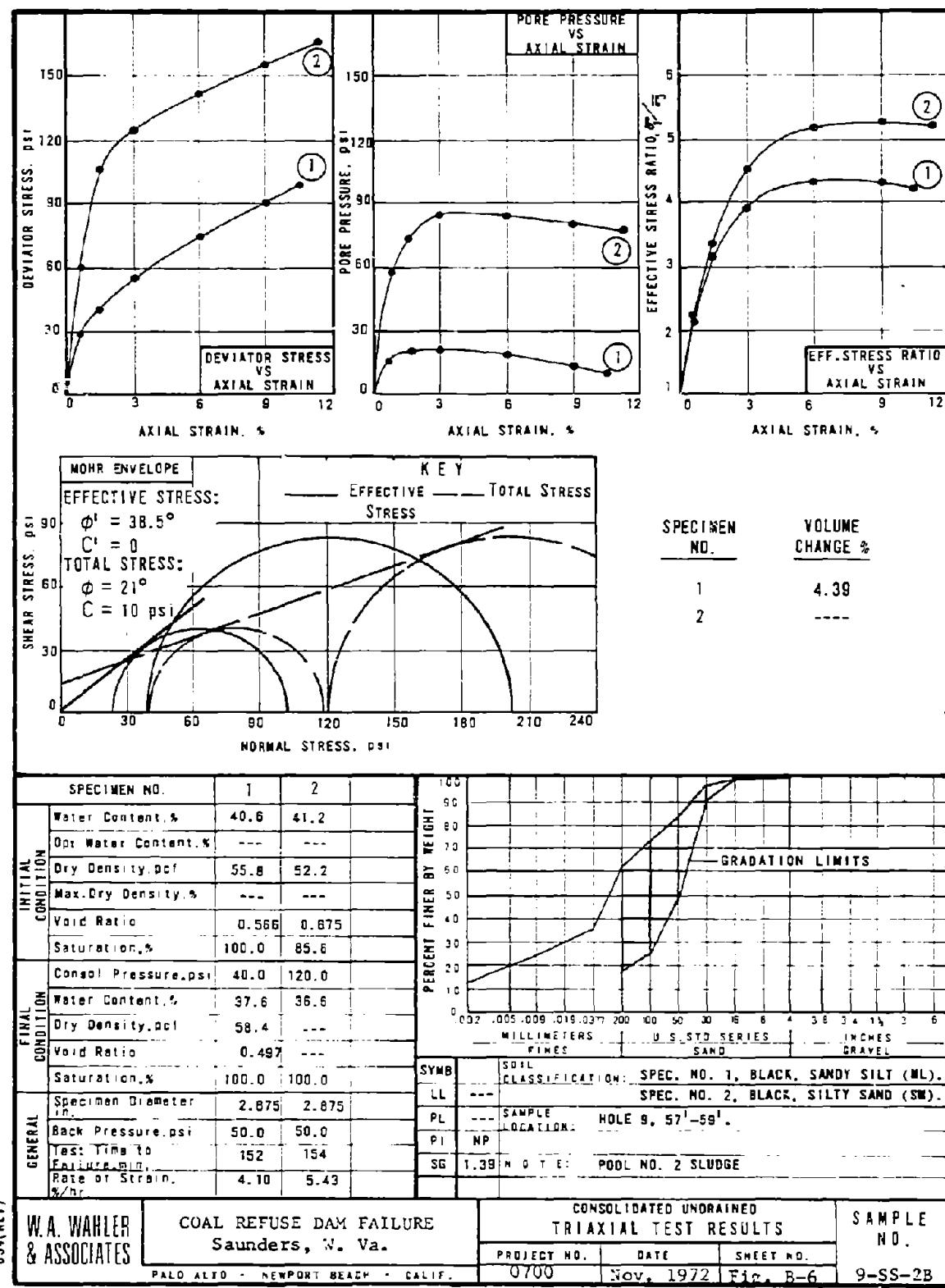


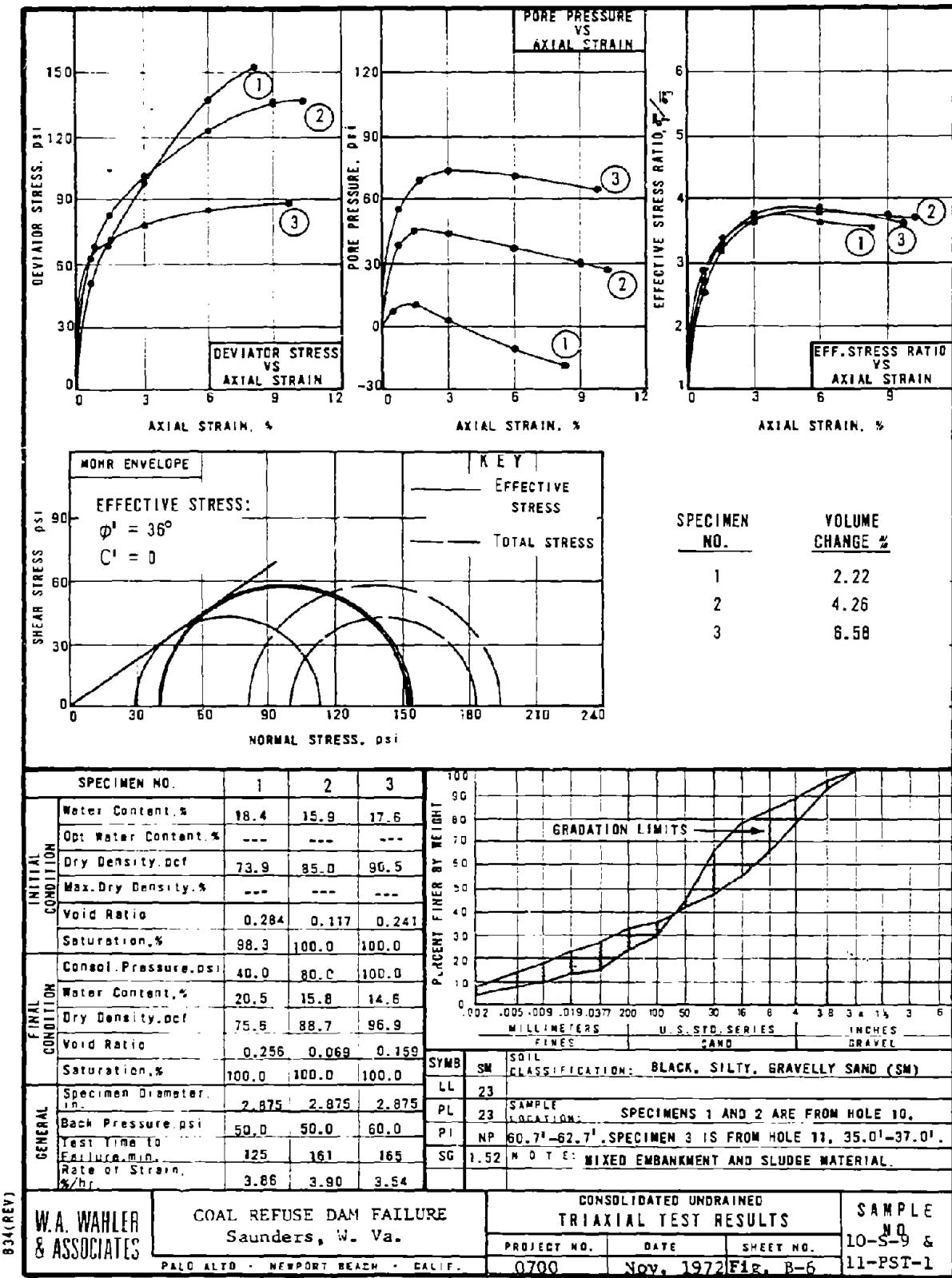


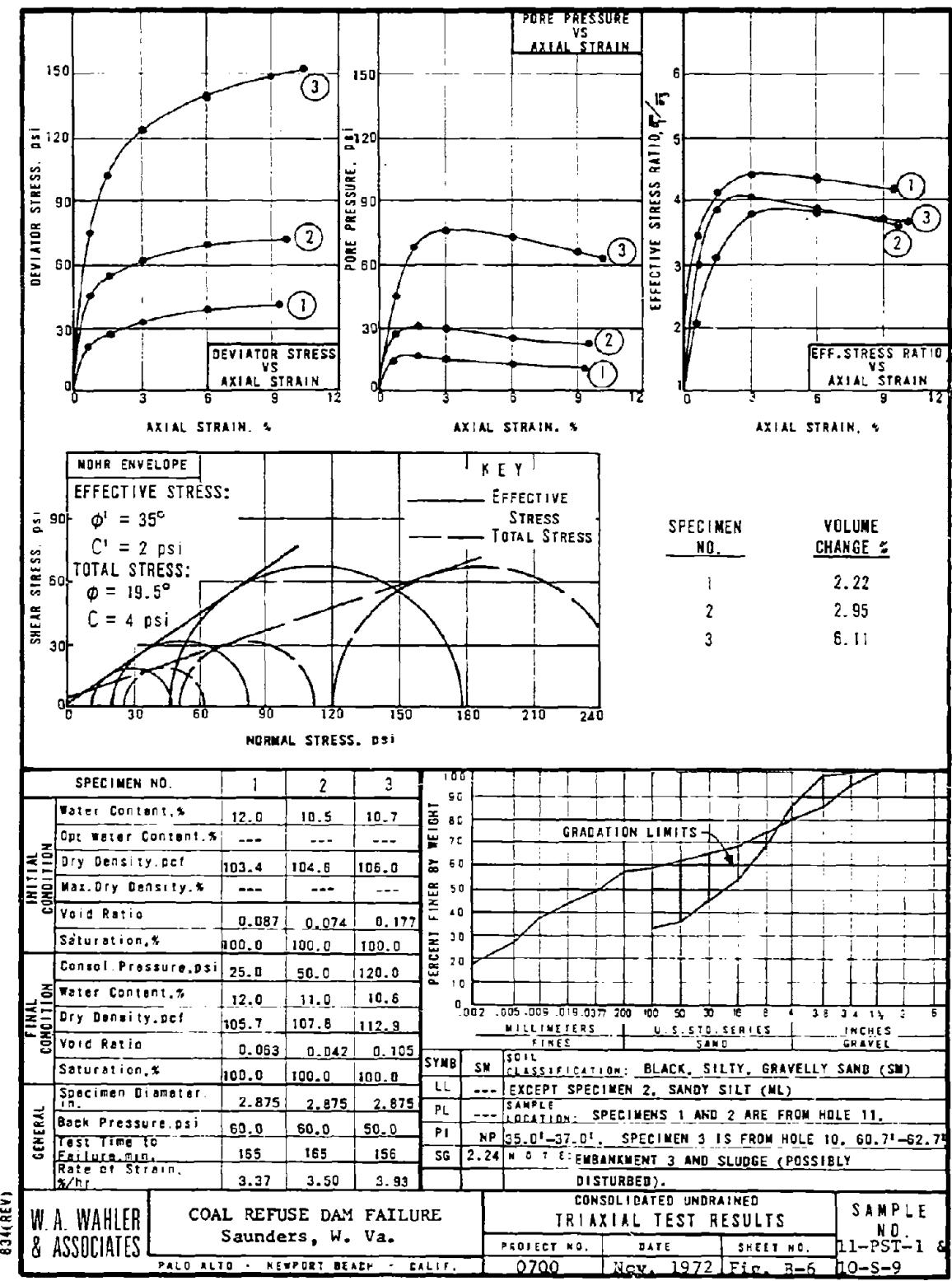


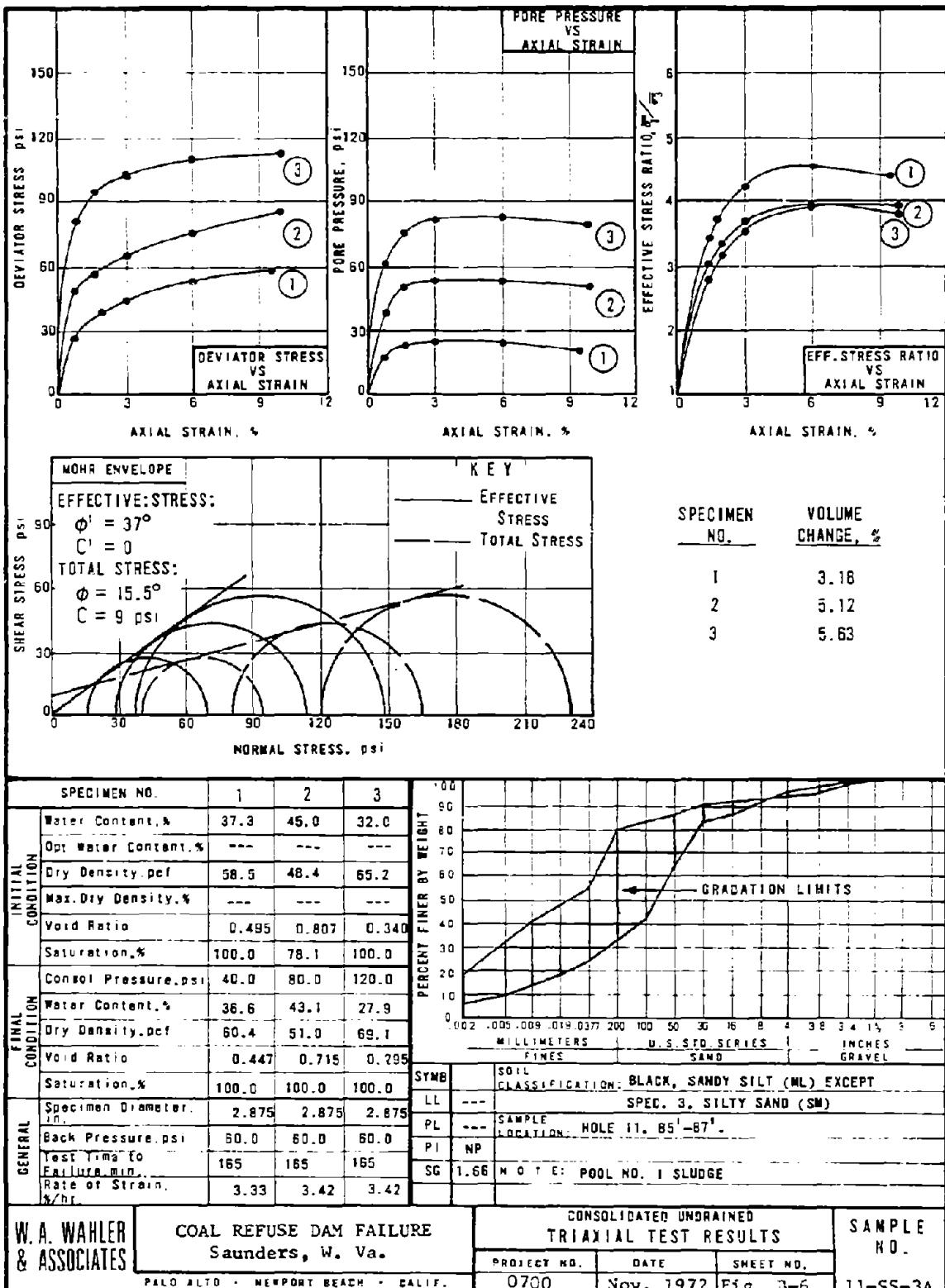




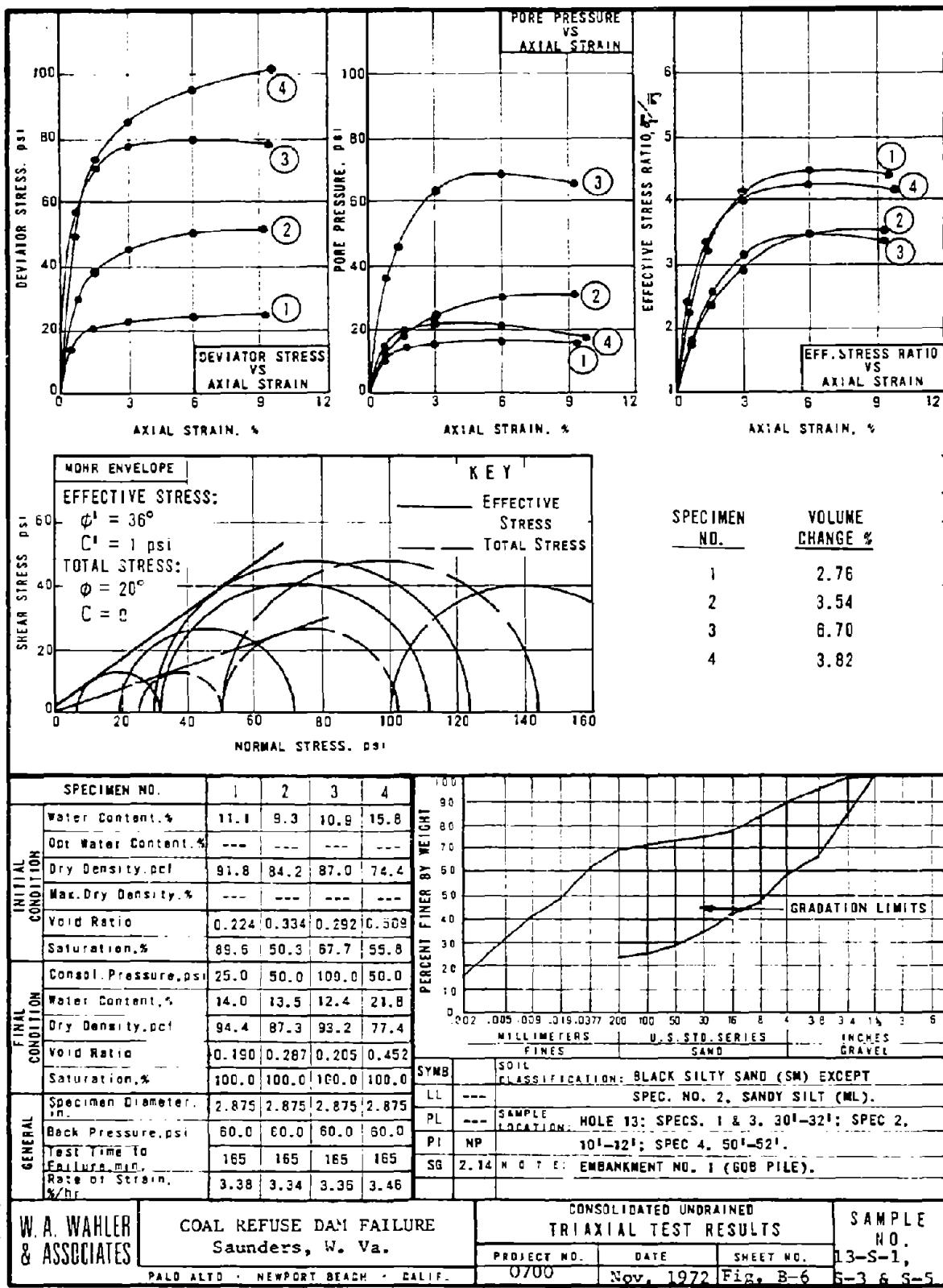


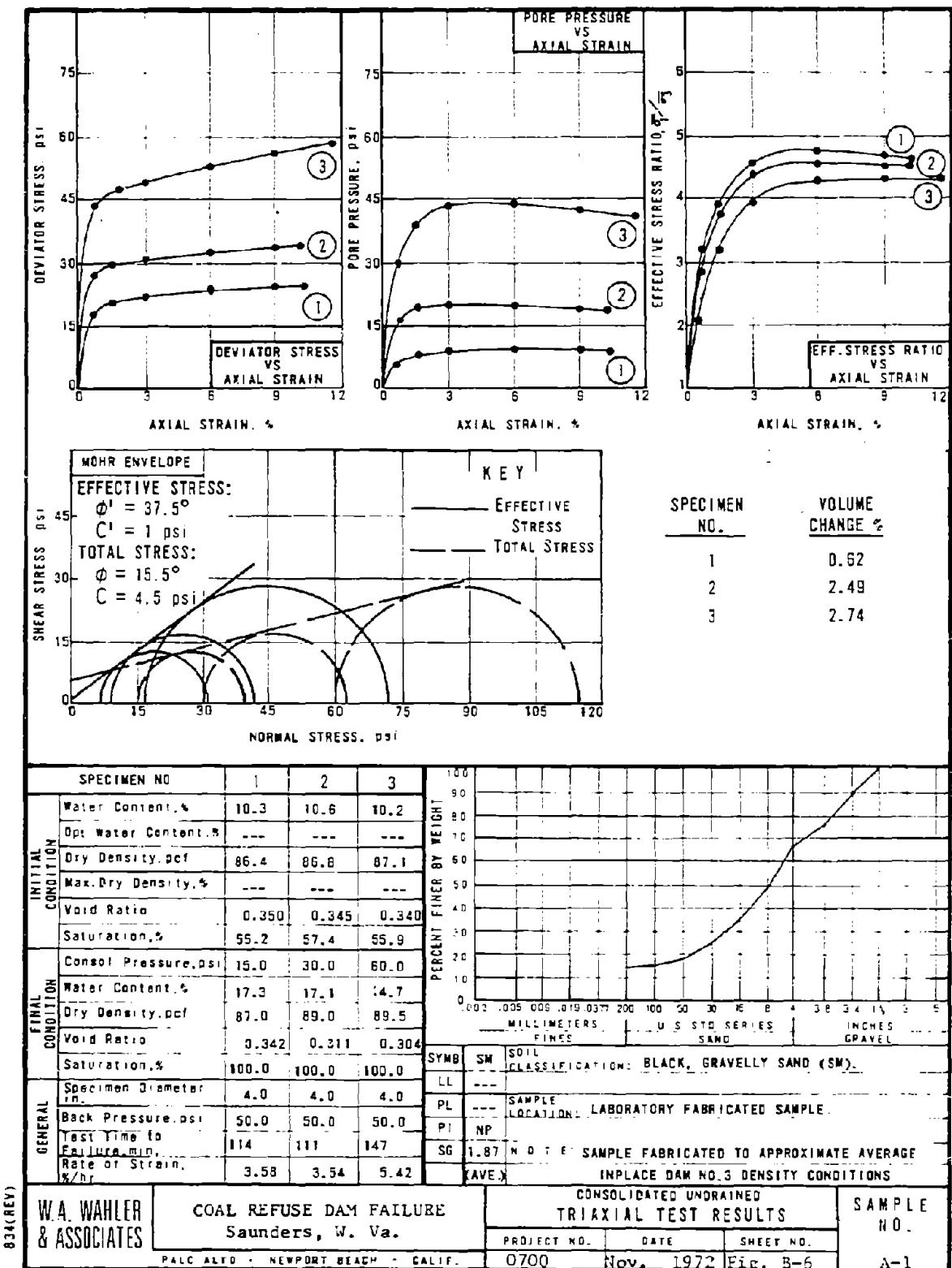




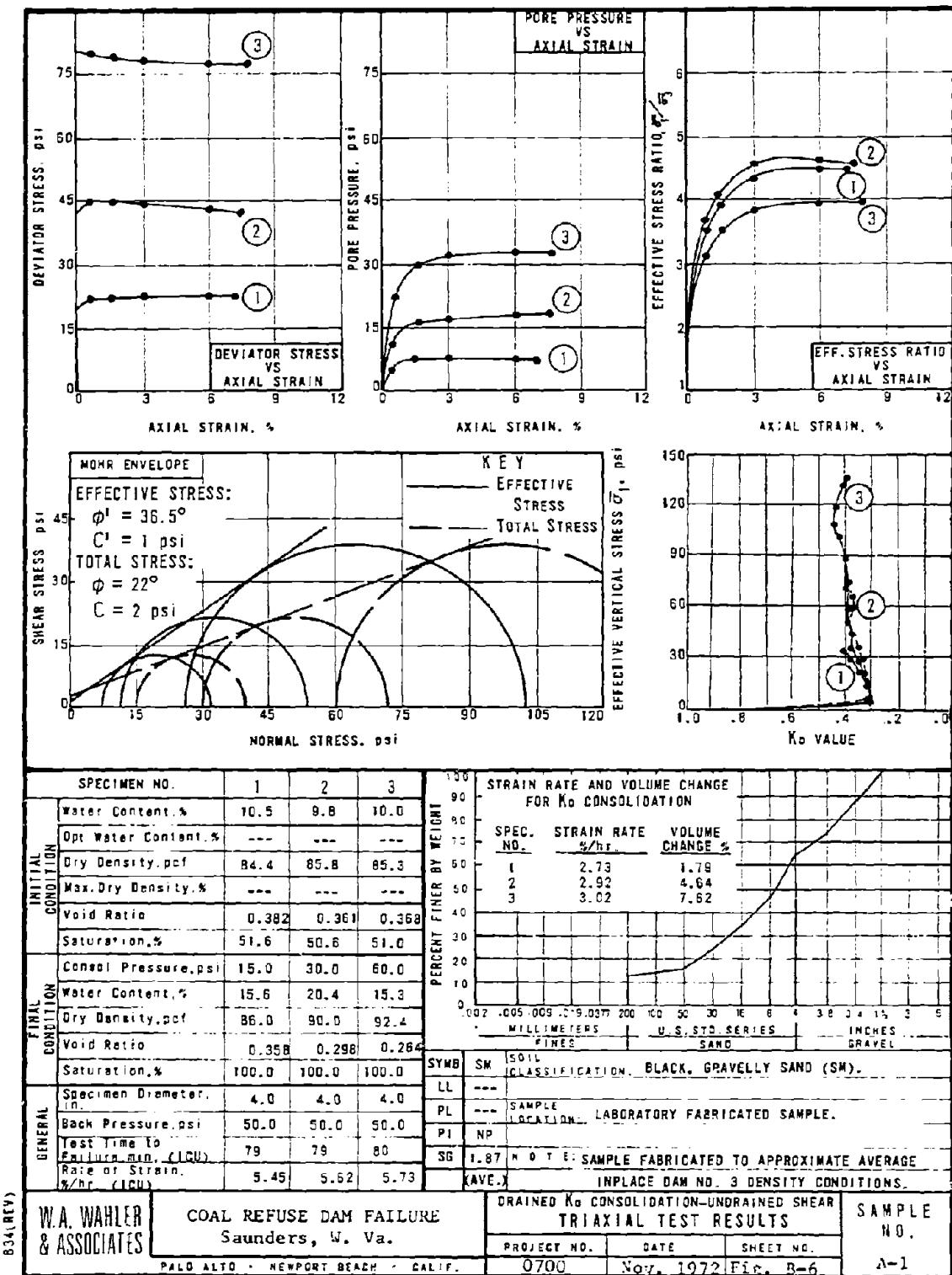


834(PEV)





834 (REV)



Sheet 15 of 15

FIGURE B-7
SUMMARY
OF
PERMEABILITY TEST DATA

SLE #	DEPTH (ft)	SOIL* TYPE	DRY DENSITY pcf	VOID RATIO (%)	WATER CONTENT (%)	DEGREE OF SATURATION (%)		COEFFICIENT OF PERMEABILITY cm/sec
						INITIAL	DURING TEST	
4	70.0-72.0	ML	52.5	0.665	44.7	93.0	100.0	4.5×10^{-7}
4	75.0-77.0	ML	56.3	0.618	37.9	87.6	100.0	1.3×10^{-5}
4	75.0-77.0	ML	63.6	0.864	40.3	94.8	100.0	3.0×10^{-7}
7	10.0-12.0	SM	66.7	0.223	11.6	86.4	100.0	1.1×10^{-4}
7	20.0-22.0	SM	87.7	0.281	14.9	95.8	100.0	1.1×10^{-4}
-	55.0-56.3	SM	53.7	0.650	41.9	87.5	100.0	1.9×10^{-4}
7	55.0-56.3	SM	54.8	0.617	40.3	100.0	100.0	1.5×10^{-4}
8	20.0-22.0	SM	82.0	0.370	13.6	66.3	100.0	3.7×10^{-5}
8	55.0-57.0	SM	50.1	0.669	40.9	81.0	100.0	1.7×10^{-4}
9	55.0-57.0	ML	54.1	0.614	42.5	97.1	100.0	5.1×10^{-6}
10	77.0-79.5	ML	67.5	0.654	30.9	94.9	100.0	1.0×10^{-6}
10	80.0-81.6	SM	54.5	1.000	37.3	59.6	100.0	3.4×10^{-4}
10	80.0-81.6	ML	59.6	0.872	40.9	85.7	100.0	6.0×10^{-6}
11	35.0-37.0	SM	103.4	0.087	12.0	100.0	100.0	3.0×10^{-5}
11	55.0-57.0	ML	58.5	0.495	37.3	100.0	100.0	1.4×10^{-6}
13	30.0-32.0	SM	91.8	0.224	11.1	89.6	100.0	4.6×10^{-5}
12	50.0-52.0	SM	74.4	0.509	15.8	55.8	100.0	3.0×10^{-8}
FP-9A	1.9-3.8	SM	99.4	0.406	11.9	49.3	100.0	5.5×10^{-6}
FP-10A	3.5-4.5	SM	94.6	0.471	14.8	48.2	100.0	2.7×10^{-5}
FP-10A	3.5-4.5	SM	95.5	0.457	14.2	100.0	100.0	1.6×10^{-5}
FP-10A	3.5-4.5	SM	97.4	0.429	12.9	100.0	100.0	1.9×10^{-5}
FP-11A	1.2-3.1	SM	101.9	0.365	10.4	50.4	100.0	9.4×10^{-6}
FP-12A	4.8-6.8	SM	88.4	0.574	19.2	38.3	100.0	1.2×10^{-4}
FP-12A	4.8-6.8	SM	89.2	0.560	18.5	100.0	100.0	1.0×10^{-4}
FP-12A	4.8-6.8	SM	91.1	0.527	17.1	100.0	100.0	6.4×10^{-5}
FP-12A	3.5-4.5	SM	106.3	0.309	11.7	45.5	100.0	6.6×10^{-6}
FP-14A	3.5-4.5	SM	107.7	0.292	11.0	100.0	100.0	4.4×10^{-5}
FP-14A	3.5-4.5	SM	111.0	0.254	9.2	100.0	100.0	1.7×10^{-5}
A-1	COMBINED	SM	86.4	0.350	10.3	55.2	100.0	8.4×10^{-4}

*UNIFIED SOIL CLASSIFICATION SYMBOL

NOTE DRY DENSITIES AND WATER CONTENTS SHOWN REPRESENT CONDITIONS AFTER SET-UP AND APPLICATION OF A SMALL CONFINING PRESSURE IN THE LABORATORY TRIAXIAL SHEAR APPARATUS, AND DO NOT NECESSARILY COINCIDE WITH IN-SITU CONDITIONS

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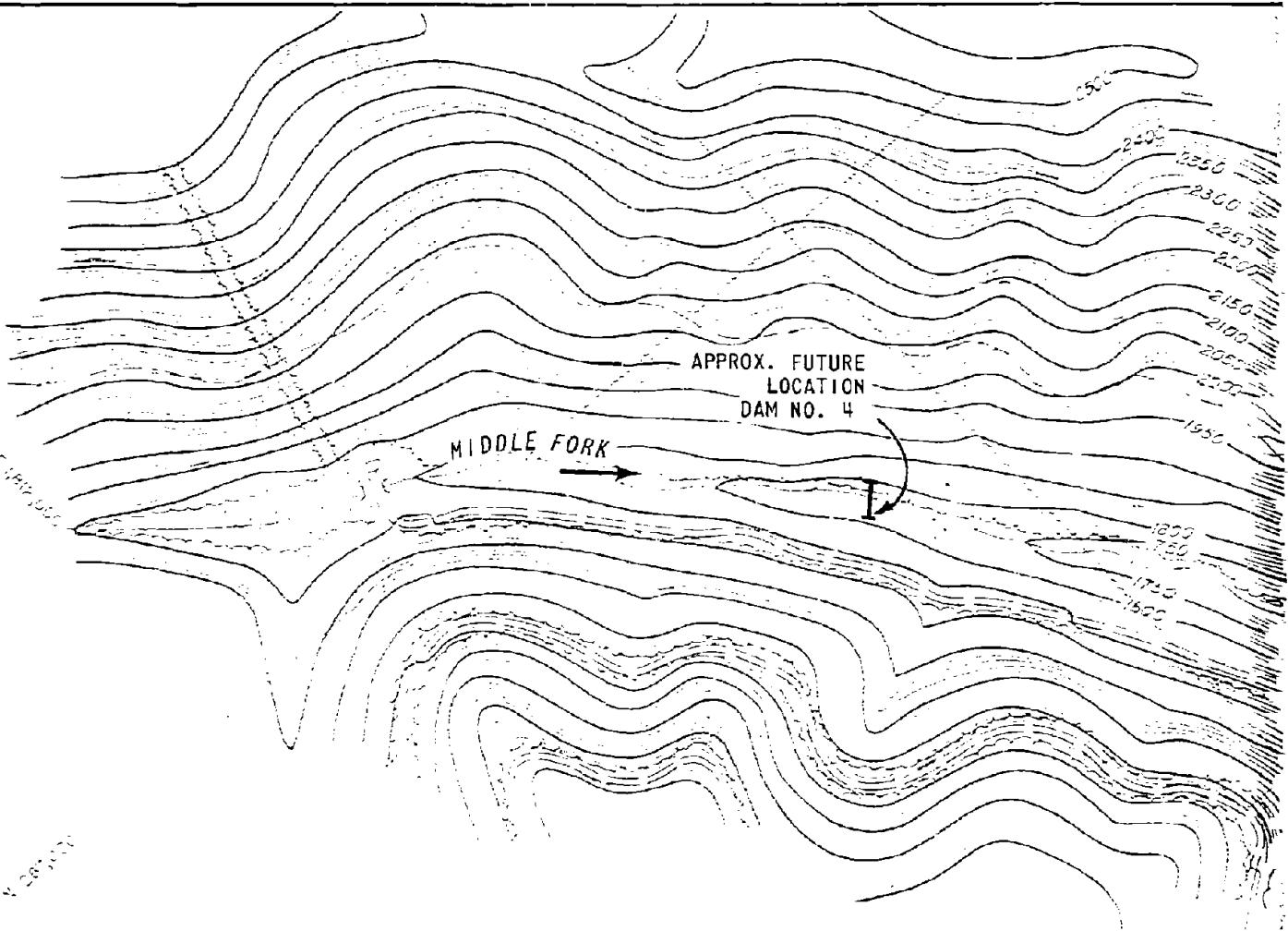
16-1

FIGURE B-7
Sheet 1 of 1

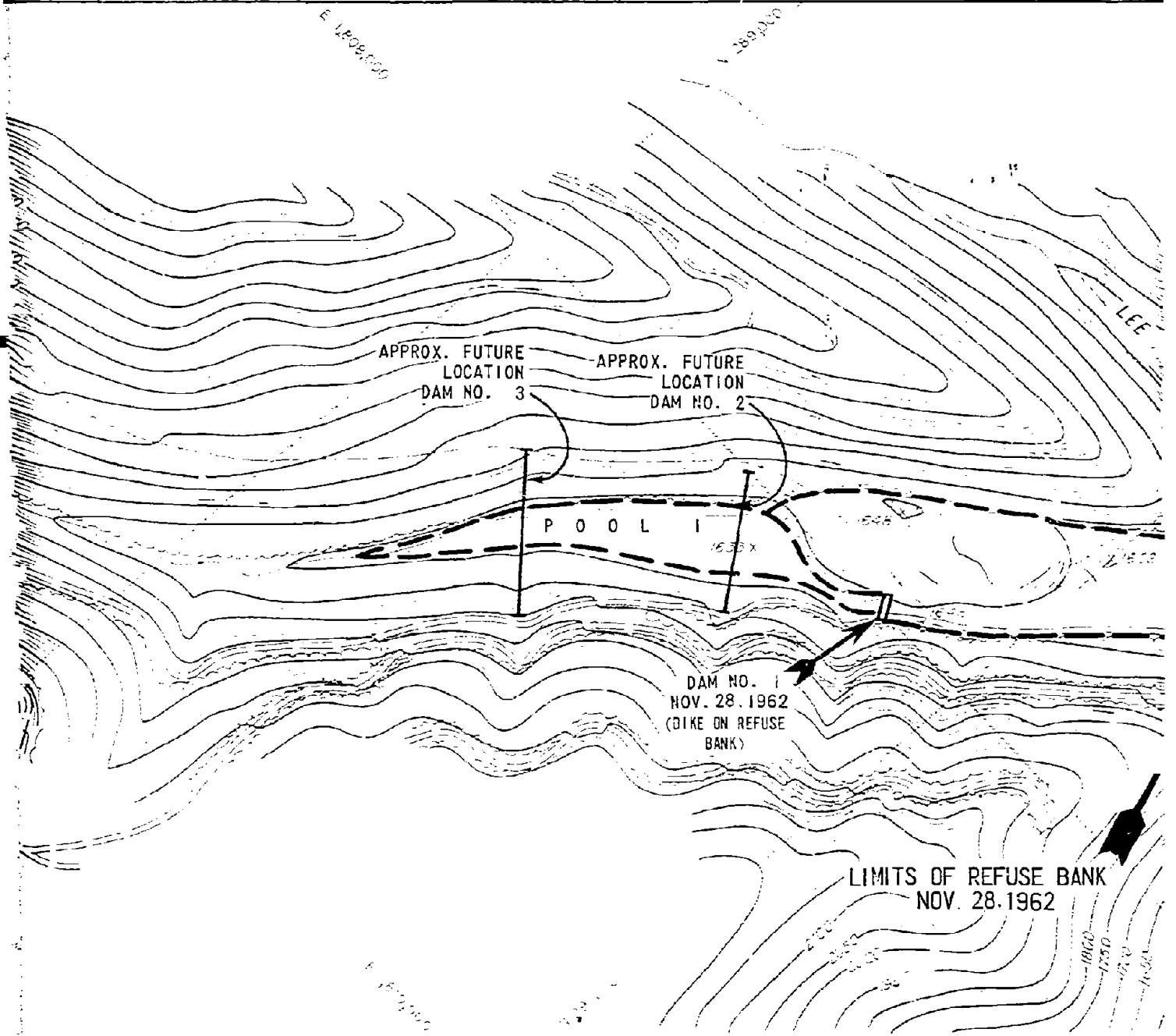
APPENDIX C

SUPPORTING DATA

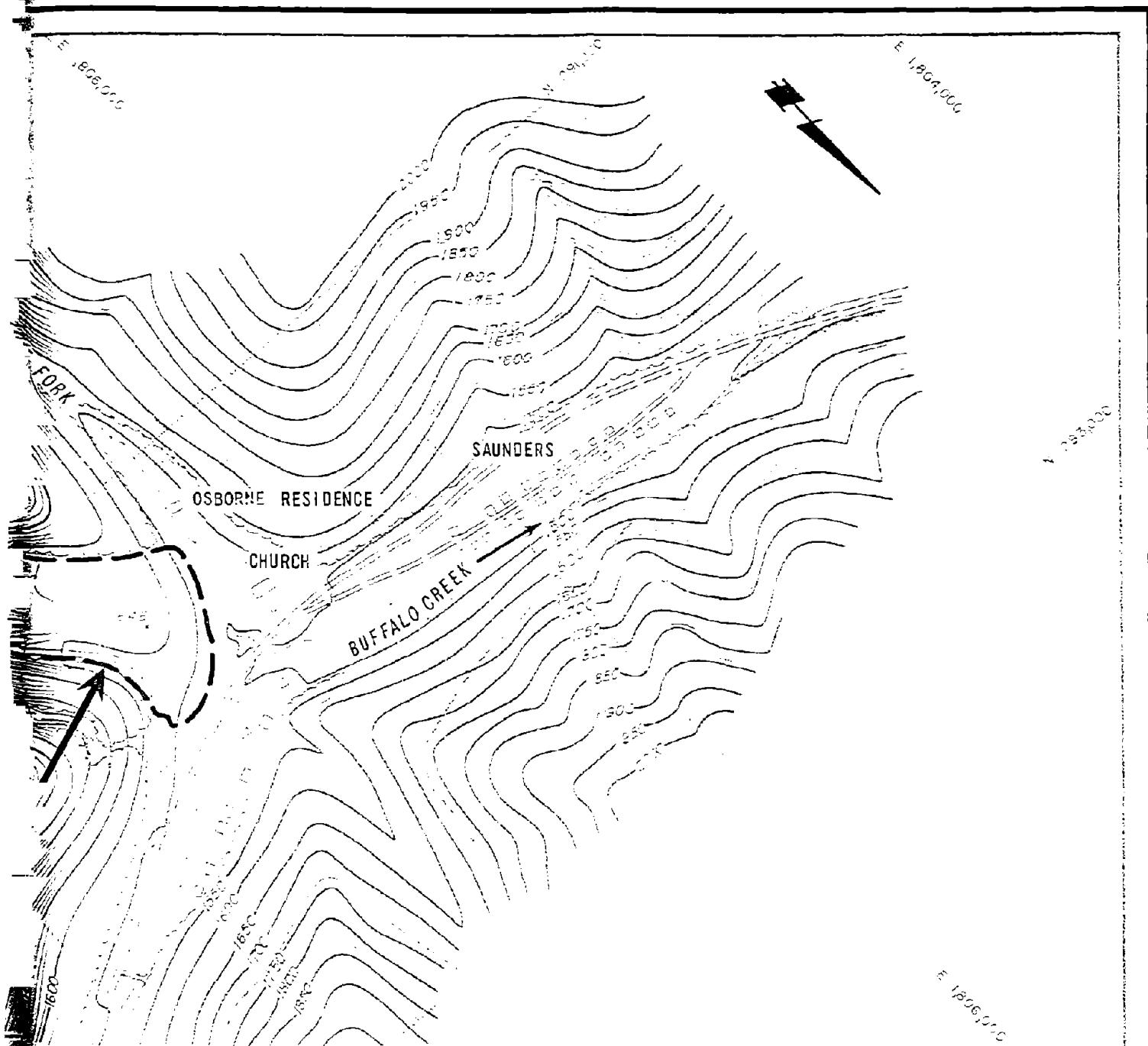
This Appendix contains a number of tables and figures that present significant data used or compiled during our investigation, but which were intentionally removed from Volume 1 of the report in order to avoid unnecessary text interruption by basic data inclusions.



NOTES (1) TOPOGRAPHY BY MICHAEL BAKER JR., INC., BASED
ON AERIAL PHOTOGRAPHS TAKEN NOVEMBER 26, 1952
(2) ELEVATIONS ARE APPROXIMATE, NO FIELD CONTROL



SCALE
400 0 400 FEET
CONTOUR INTERVAL 10 FEET



166

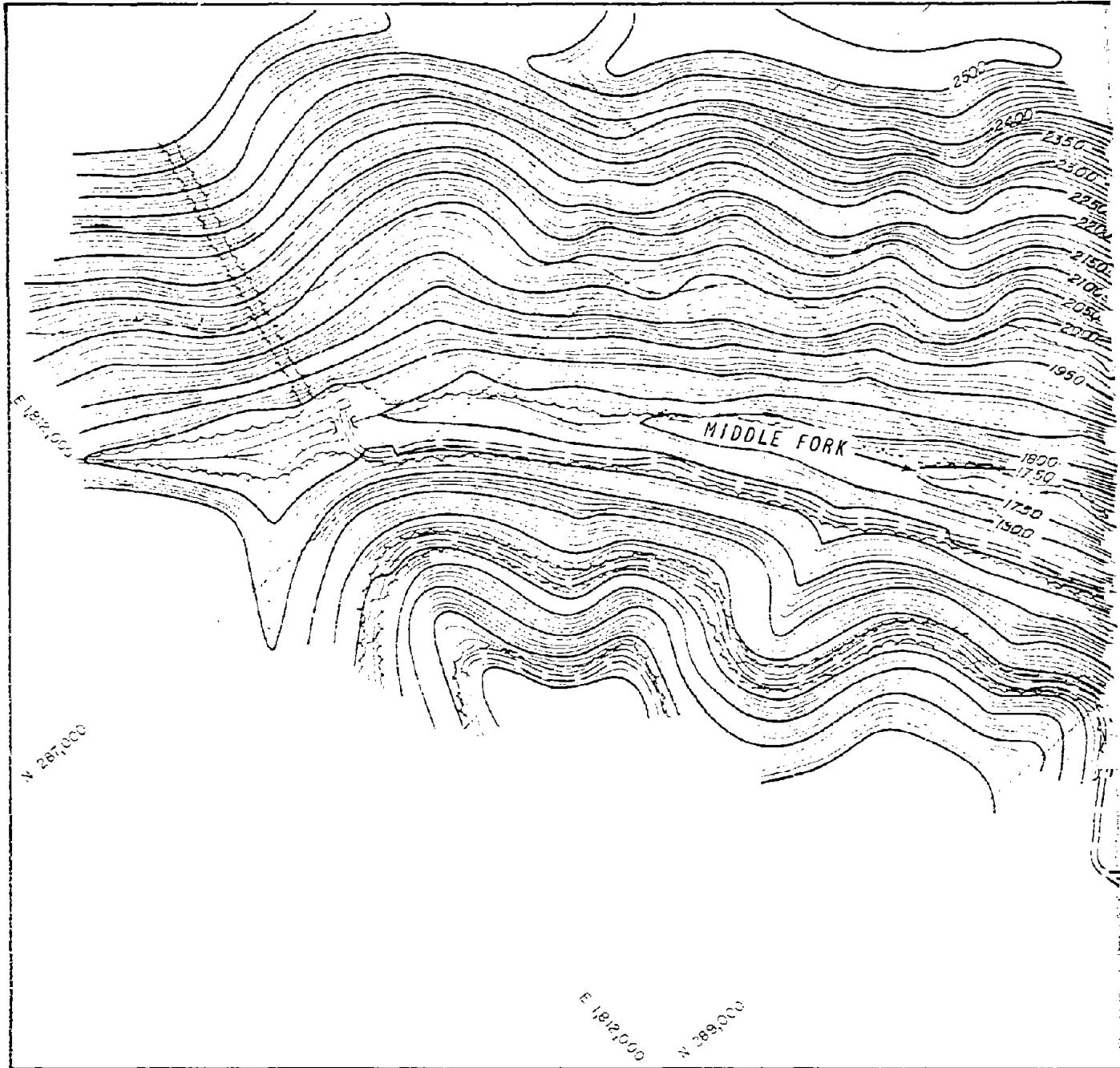
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COAL REFUSE DAM FAILURE
SAUNDERS, WEST VIRGINIA

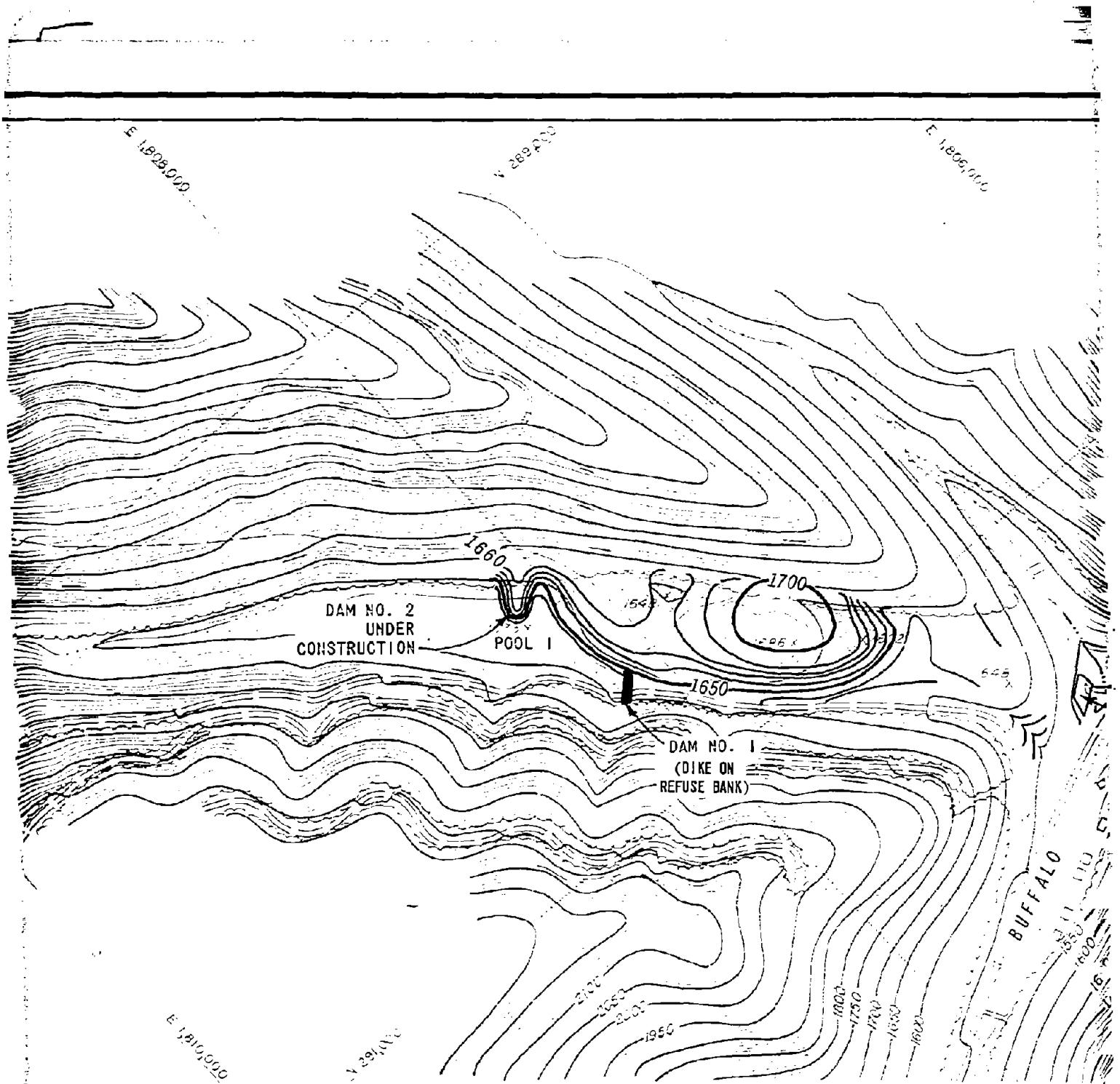
PALO ALTO • NEWPORT BEACH • CALIF.

TOPOGRAPHIC MAP OF MIDDLE FORK VALLEY
NOVEMBER 28, 1962

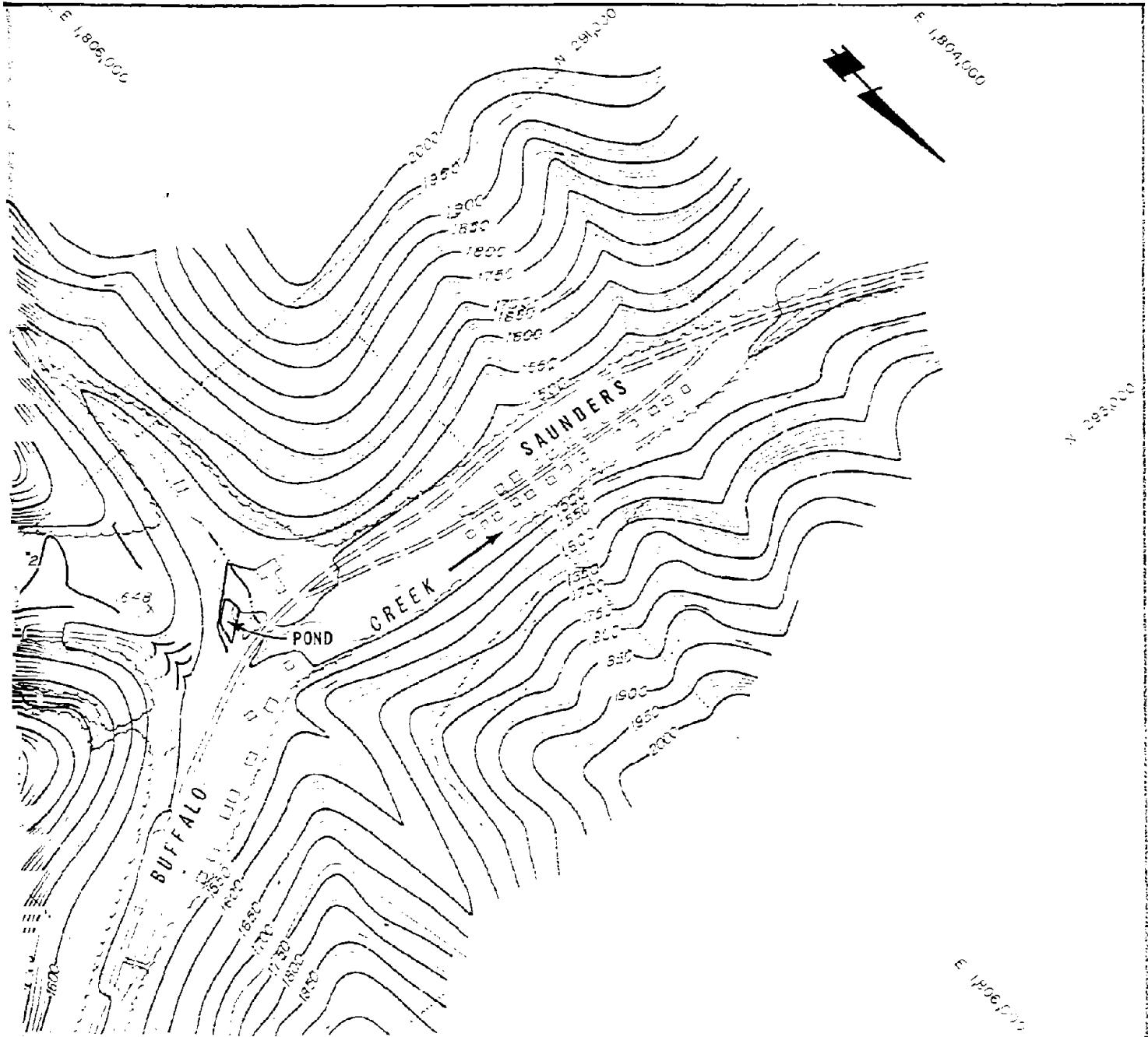
PROJECT NO.	DATE	DRAWING NO.
0700	NOVEMBER 1972	1-1



NOTES (1) TOPOGRAPHY MODIFIED FROM FIGURE C-1 OF THIS REPORT. 1966 CONTOURS SHOWN IN BOLD LINES.
(2) CONTOURS IN DAM NO. 2 - REFUSE BANK AREA ARE GENERALIZED. BASED ON SKETCH BY W E DAVIES 12/9/66



SCALE
400 0 400 FEET
CONTOUR INTERVAL 10 FEET



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**COAL REFUSE DAM FAILURE
SAUNDERS, WEST VIRGINIA**

PALO ALTO • NEWPORT BEACH • CALIF

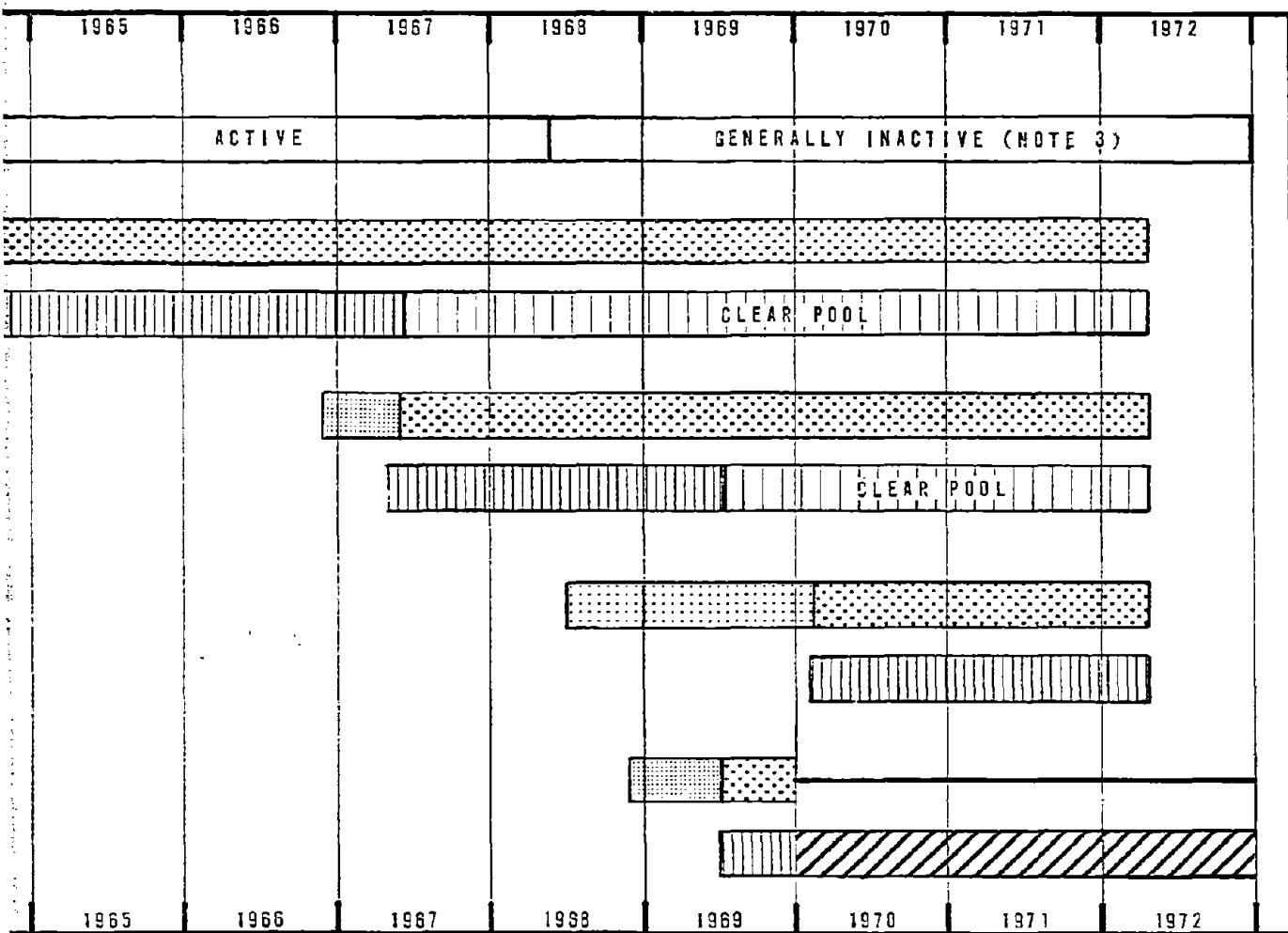
**DECEMBER 1966 TOPOGRAPHY
MIDDLE FORK VALLEY**

PROJECT NO.	DATE	FIGURE NO.
0700	NOVEMBER 1972	C-2

FEATURE	YEAR	1960	1961	1962	1963	1964	1965
REFUSE BANK						INACTIVE (NOTE 2)	
DAM NO. 1							
POOL 1							
DAM NO. 2							
POOL 2							
DAM NO. 3							
POOL 3							
DAM NO. 4							
POOL 4							
		1960	1961	1962	1963	1964	1965

CALENDAR OF DAM AND POOL
MIDDLE FORK
1960-1972

- NOTES: (1) REFUSE BANK ACTIVE = RECEIVING COAL REFUSE. REFUSE BANK WAS ACTIVE SINCE 1947.
 (2) REFUSE BANK INACTIVE = MINES CLOSED.
 (3) REFUSE BANK GENERALLY INACTIVE = MOST OR ALL OF THE COAL REFUSE OUTPUT BEING USED TO BUILD OR ENLARGE DAMS, OR PLACED ELSEWHERE.
 (4) THE PATTERN OF REFUSE PLACEMENT CAUSED THE REFUSE BANK TO COALESCE WITH DAM NO. 1 SOMETIME BETWEEN 1960 AND 1962. IT THUS BECAME FUNCTIONALLY A PART OF DAM NO. 1 AT THAT TIME. DURING THE PERIOD 1967-1969, THE PATTERN OF REFUSE PLACEMENT CAUSED THE REFUSE BANK TO COALESCE WITH THE LEFT PORTION OF THE DOWNSTREAM FACE OF DAM NO. 2 ALSO. SEE THE ARTIST'S SKETCHES IN THIS CHAPTER FOR A VISUAL REPRESENTATION OF THIS SEQUENCE.
- HORIZONTAL
1/12"
- (5) THE TIMING SHOWN HEREON REPRESENTS AN INTERPRETATION OF THE AVAILABLE DATA AND TESTIMONY. SOME CONFLICTS EXIST IN THE SOURCE DATA.

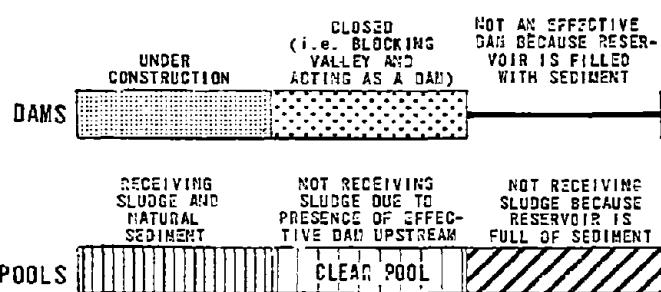


F DAM AND POOL ACTIVITY

MIDDLE FORK

1960-1972

K E Y



ONLY.

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& ASSOCIATES

COAL REFUSE DAM FAILURE
SAUNDERS, WEST VIRGINIA

PALO ALTO • NEWPORT BEACH • CALIF.

CALENDAR OF DAM AND POOL ACTIVITY
MIDDLE FORK

PROJECT NO. 0700 DATE NOVEMBER 1972 FIGURE NO. C-3

TABLE C-1
CONSTRUCTION METHODS
MIDDLE FORK REFUSE BANK AND DAMS

FEATURE	SOURCE AND REPORTED (OR INFERRED) CONSTRUCTION METHOD
REFUSE BANK	<p>COMMISSION REPORT: TRUCK DUMPING</p> <p>U.S. CONGRESS, 1972a: NOT SPECIFICALLY MENTIONED</p> <p>DAVIES, 1967: TRUCK DUMPING</p> <p>DAVIES AND OTHERS, 1972: TRUCK DUMPING</p> <p>PARK AND OTHERS, 1972: DUMPING</p> <p>TASK FORCE PRELIMINARY REPORT 1972: TRUCK DUMPING</p> <p>WALKER, 1972: TRUCK DUMPING SPREAD INTO 20-FOOT LIFTS</p>
DAM NO. 1	<p>COMMISSION REPORT: NO DETAILS GIVEN</p> <p>U.S. CONGRESS, 1972a: NOT SPECIFICALLY COVERED. QUOTES PARK AND OTHERS (1972).</p> <p>DAVIES, 1966: TRUCK DUMPING</p> <p>DAVIES AND OTHERS, 1972: TRUCK DUMPING</p> <p>PARK AND OTHERS, 1972: "WAS CONSTRUCTED BY PLACING COAL REFUSE PARTIALLY ACROSS THE VALLEY AT A POINT UPSTREAM FROM THE THEN EXISTING REFUSE PILE. THIS REFUSE WAS APPARENTLY PLACED ON FIRM GROUND."</p> <p>TASK FORCE PRELIMINARY REPORT 1972: QUOTES PARK AND OTHERS, 1972 (SEE ABOVE).</p> <p>WALKER, 1972: "...BUILT BY END DUMPING FROM THE VALLEY SIDES IN ABOUT 20-FOOT LIFTS." (THIS DESCRIPTION MAY REFER MORE TO DAMS 2 AND 3 THAN TO DAM NO. 1.)</p>
DAM NO. 2	<p>COMMISSION REPORT: "DAM NO. 2... WAS CONSTRUCTED BY DUMPING REFUSE ACROSS THE WIDTH OF THE HOLLOW ON THE DEPOSITS REMAINING IN THE RESERVOIR BEHIND DAM NO. 1."</p> <p>U.S. CONGRESS, 1972a: "...CONSTRUCTED BY DUMPING REFUSE INTO AREAS OF IMPOUNDMENT WATER AND/OR PARTIALLY SETTLED COAL WASHINGS."</p> <p>DAVIES, 1966: TRUCK DUMPING</p> <p>DAVIES AND OTHERS, 1972: TRUCK DUMPING</p> <p>PARK AND OTHERS, 1972: "THE...DAM...(WAS) CONSTRUCTED BY HAULING REFUSE BY TRUCK...AND DUMPING IT INTO AN AREA WHICH CONTAINED SILT AND WATER IMPOUNDED EARLIER."</p> <p>TASK FORCE PRELIMINARY REPORT, 1972: QUOTES PARK AND OTHERS (1972). (SEE ABOVE).</p> <p>WALKER, 1972: "BUILT BY END DUMPING FROM THE VALLEY SIDES IN ABOUT 20-FOOT LIFTS."</p>

TABLE C-1 — CONTINUED
 CONSTRUCTION METHODS
 MIDDLE FORK REFUSE BANK AND DAMS

FEATURE	SOURCE AND REPORTED (OR INFERRED) CONSTRUCTION METHOD
DAM NO. 3	<p>COMMISSION REPORT: "DAM NO. 3 WAS CONSTRUCTED BY END DUMPING COAL WASTE FROM TRUCKS IN CLOSELY SPACED PILES FROM 4 TO 7 FEET HIGH AND THEN GRADED IN LAYERS 2 TO 4 FEET THICK. THE DUMPING WAS CARRIED ACROSS THE VALLEY FROM THE RIGHT ABUTMENT ON THE NO. 5 MINE ROAD TOWARD THE LEFT ABUTMENT... THE DUMPING WAS DONE IN THE FORM OF A SINGLE LIFT (LEVEL OF MATERIAL) WHICH RANGED UP TO 60 FEET THICK. ONCE THE DAM HAD BEEN COMPLETED ACROSS THE VALLEY, DUMPING WAS MAINLY ACROSS THE BACK SIDE OF THE DAM WHICH STEADILY GREW UPSTREAM."</p> <p>U.S. CONGRESS, 1972a: "AFTER THE EMBANKMENT FOR NO. 3 WAS COMPLETED ACROSS THE VALLEY BY DUMPING OVER THE END OF THE FILL, ADDITIONAL REFUSE WAS PLACED BY TRUCKS DUMPING OVER THE EDGE OF THE EMBANKMENT INTO THE IMPOUNDMENT OR ON TOP OF THE FILL. FOR THE LATTER, LEVELLING BY A DOZER AND BACKDRAGGING OF THE BLADE. TOGETHER WITH THE HAULING TRAFFIC, WAS THE ONLY COMPACTION THE REFUSE RECEIVED."</p> <p>DAVIES, 1966: (DAM NO. 3 NOT BUILT)</p> <p>DAVIES AND OTHERS, 1972: "IN CONSTRUCTING DAM NO. 3, THE COAL WASTE WAS DUMPED FROM TRUCKS IN CLOSELY SPACED PILES FROM 4 TO 7 FEET HIGH AND THEN GRADED IN LAYERS 2 TO 4 FEET THICK. THE DUMPING WAS CARRIED ACROSS THE DAM IN THE FORM OF "LIFTS" ON SUCCESSIVE LEVELS OF MATERIAL 10 TO 20 FEET THICK. ONCE THE DAM WAS CLOSED, DUMPING WAS MAINLY ACROSS THE BACK SIDE OF THE DAM, WHICH STEADILY GREW UPSTREAM. TREES IN THE PATH OF THE DAM CONSTRUCTION WERE NOT REMOVED BUT WERE COVERED BY DUMPING. THE POOL AREA ALSO WAS NOT CLEARED OF VEGETATION. THE SLUDGE ON WHICH THE WASTE WAS DUMPED WAS ONLY PARTIALLY DISPLACED AND MUCH OF IT FORMED THE FOUNDATION OF THE DAMS."</p> <p>PARK AND OTHERS, 1972: "THE ...DAM...(WAS) CONSTRUCTED BY HAULING REFUSE BY TRUCK, AND DUMPING IT INTO AN AREA WHICH CONTAINED SILT AND WATER IMPOUNDED EARLIER... RECENTLY, PLACING OF THE REFUSE WAS DONE BY TRUCKS DUMPING EITHER OVER THE ENDS OF THE DAM AND INTO THE IMPOUNDMENTS WHEN POSSIBLE, OR BY DUMPING THE LOADS ON THE TOP OF THE DAM FOR SPREADING. WHEN LOADS WERE DUMPED ON TOP, THIS MATERIAL HAD TO BE LEVELED PERIODICALLY TO PREVENT BLOCKING THE ACCESS FOR TRUCKS. THIS WAS DONE BY GRADING THE MATERIAL WITH A BULLDOZER AND THEN "BACK BLADING" OR SCRAPING THE MATERIAL WITH THE BACK OF THE BULLDOZER BLADE WHILE OPERATING IN A REVERSE DIRECTION. THIS PROVIDED A LEVEL SURFACE FOR HAULAGE. COMPACTION WAS DONE ONLY BY THE WEIGHT OF THE BULLDOZER AND TRUCKS AS THEY MOVED ACROSS THE MATERIAL."</p>

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 & ASSOCIATES

TABLE C-1 —CONTINUED
 CONSTRUCTION METHODS
 MIDDLE FORK REFUSE BANK AND DAMS

FEATURE	SOURCE AND REPORTED (OR INFERRED) CONSTRUCTION METHOD
DAM NO. 3 (CONTINUED)	TASK FORCE PRELIMINARY REPORT, 1972: QUOTES PARK AND OTHERS (1972). (SEE ABOVE). WALKER, 1972: "...BUILT BY END DUMPING FROM THE VALLEY SIDES IN ABOUT 20-FOOT LIFTS."
DAM NO. 4	COMMISSION REPORT: "DAM NO. 4 WAS CONSTRUCTED IN 1969 AND IS STILL IN PLACE...CONSTRUCTED MAINLY OF SHALE AND COAL WASTE." U.S. CONGRESS, 1972a: DAM NO. 4 MENTIONED ONLY AS "STILL IN PLACE." DAVIES, 1966: (DAM NO. 4 NOT BUILT) DAVIES AND OTHERS, 1972: "...CONSTRUCTED MAINLY OF SHALE WITH COAL WASTE..." PARK AND OTHERS, 1972: (DAM NO. 4 NOT MENTIONED) TASK FORCE PRELIMINARY REPORT, 1972: (DAM NO. 4 NOT MENTIONED). WALKER, 1972: MENTIONS "FOURTH BARRIER"; DOES NOT GIVE ANY CONSTRUCTION DATA.

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TABLE C-1
Sheet 3 of 3

TABLE C-2
DAILY WEATHER CONDITIONS JANUARY 1972
(WEST VIRGINIA)

["T" DENOTES TRACE OF PRECIPITATION. TEMPERATURES SHOWN ARE DEGREES FAHRENHEIT.
PRECIPITATION SHOWN IS IN INCHES.]

DATE	LOGAN			MADISON			PINEVILLE		
	MAX. TEMP.	MIN. TEMP.	PRECIP.	MAX. TEMP.	MIN. TEMP.	PRECIP.	MAX. TEMP.	MIN. TEMP.	PRECIP.
1	44	23	----	42	22	----	43	21	----
2	50	24	0.80	50	23	0.58	52	22	1.08
3	50	29	0.19	50	28	0.19	47	28	0.06
4	55	30	0.23	46	28	0.24	53	27	0.42
5	49	33	1.30	50	30	1.07	47	32	1.22
6	34	24	T	32	21	0.03	33	20	----
7	35	21	----	34	20	----	34	17	----
8	44	20	----	42	20	----	42	17	----
9	49	21	----	47	20	----	47	21	----
10	50	41	0.61	55	40	0.53	40	32	0.53
11	60	44	0.04	61	45	0.10	54	39	----
12	53	31	0.22	50	28	0.15	60	30	----
13	62	31	----	56	30	----	61	30	----
14	72	29	0.35	71	28	0.25	57	30	0.49
15	32	17	T	35	16	----	31	14	0.02
16	19	-5	----	23	-8	----	20	-7	T
17	15	2	----	15	-7	----	12	-7	----
18	44	11	----	40	12	----	40	5	----
19	59	17	0.10	53	18	0.08	50	13	0.05
20	48	39	0.05	52	38	0.09	42	34	0.10
21	57	40	0.65	58	40	0.39	46	36	1.37
22	51	45	0.02	48	41	T	59	38	0.06
23	67	43	0.04	65	40	0.03	63	42	0.04
24	58	46	0.30	62	48	0.34	57	43	0.03
25	76	41	0.33	72	38	0.29	72	38	0.24
26	43	19	----	40	17	----	41	19	----
27	50	19	----	45	17	----	48	18	----
28	42	26	0.85	37	23	0.60	46	19	1.00
29	39	26	T	37	23	----	42	26	T
30	35	26	----	36	23	----	46	26	----
31	35	20	----	34	20	T	34	21	T

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& ASSOCIATES

TABLE C-2
Sheet 1 of 2

TABLE C-2 —CONTINUED
DAILY WEATHER CONDITIONS FEBRUARY 1972
(WEST VIRGINIA)

[“T” DENOTES TRACE OF PRECIPITATION. TEMPERATURES SHOWN ARE DEGREES FAHRENHEIT.
PRECIPITATION SHOWN IS IN INCHES.]

DATE	LOGAN			MADISON			PINEVILLE		
	MAX. TEMP.	MIN. TEMP.	PRECIP.	MAX. TEMP.	MIN. TEMP.	PRECIP.	MAX. TEMP.	MIN. TEMP.	PRECIP.
1	38	18	----	37	17	----	36	17	----
2	42	18	----	42	17	----	43	18	T
3	55	31	0.06	54	29	0.04	45	29	0.12
4	45	18	0.52	44	17	0.42	42	15	0.29
5	22	11	----	22	10	T	21	11	----
6	35	11	----	33	11	----	31	12	----
7	39	27	0.32	40	24	0.22	35	24	0.32
8	28	10	T	25	7	T	29	3	----
9	32	12	----	30	7	----	29	4	0.30
10	37	24	----	34	17	----	37	16	----
11	45	23	----	41	18	----	41	10	----
12	57	12	----	51	23	----	52	20	----
13	40	28	0.92	59	25	0.81	58	24	0.78
14	57	30	0.29	40	32	0.28	38	31	0.34
15	45	32	----	53	32	----	53	23	----
16	49	28	----	54	25	----	45	27	----
17	50	25	0.06	47	26	0.09	46	26	0.18
18	43	31	0.10	40	31	0.10	41	32	0.70
19	41	24	0.34	42	23	0.30	41	22	0.22
20	28	19	0.04	27	16	0.10	25	15	0.14
21	36	18	----	33	16	----	29	9	----
22	55	18	0.14	56	18	0.16	49	9	0.15
23	45	28	----	42	22	----	42	25	----
24	49	27	1.41	51	24	1.27	47	26	1.33
25	*	*	0.41	53	39	0.52	49	40	0.86
26	68	40	1.90	65	40	1.87	68	41	1.54
27	50	29	0.05	46	28	0.08	56	26	0.03
28	57	28	----	57	28	----	56	28	----
29	71	31	----	69	36	----	65	29	----

* NOT REPORTED.

ORIGINAL SOURCE: CLIMATOLOGICAL DATA, WEST VIRGINIA
VOL. 80, NOS. 1 AND 2, JANUARY AND FEBRUARY, 1972
U.S. DEPARTMENT OF COMMERCE
NATIONAL OCEANIC AND ATMOSPHERIC ADMINISTRATION
ENVIRONMENTAL DATA SERVICE.

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TABLE C-3
SUMMARY
WEATHER CONDITIONS JANUARY 1 - FEBRUARY 29, 1972

[PRECIPITATION AND SNOW LEVEL RECORDS ARE GIVEN IN INCHES]

DESCRIPTION	LOGAN	HADISON	PINEVILLE
JANUARY (1-31)			
AVERAGE MAXIMUM TEMPERATURE	47.6	46.5	45.8
AVERAGE MINIMUM TEMPERATURE	26.9	25.2	24.0
AVERAGE DAILY TEMPERATURE	37.3	35.9	34.9
PRECIPITATION, TOTAL	6.08	4.96	6.55
PRECIPITATION, NORMAL	3.76	(1)	(1)
SNOW, TOTAL	-----	1.00	0.50
FEBRUARY (1-29)			
AVERAGE MAXIMUM TEMPERATURE	45.0	44.4	43.1
AVERAGE MINIMUM TEMPERATURE	23.7	22.7	21.1
AVERAGE DAILY TEMPERATURE	34.4	33.6	32.1
PRECIPITATION, TOTAL	6.56	6.26	7.30
PRECIPITATION, NORMAL	3.50	(1)	(1)
SNOW, TOTAL	2.50	3.20	10.60
FEBRUARY (11-25)			
AVERAGE MAXIMUM TEMPERATURE	45.7 *	45.9	43.7
AVERAGE MINIMUM TEMPERATURE	24.5 *	23.3	22.6
AVERAGE DAILY TEMPERATURE	35.1 *	34.6	33.2
PRECIPITATION, TOTAL	3.51	3.43	4.70
DAYS WITH MEASURABLE RAIN	9	9	9
FEBRUARY (24-25)			
AVERAGE MAXIMUM TEMPERATURE	49.0 *	52.0	48.0
AVERAGE MINIMUM TEMPERATURE	27.0 *	31.5	33.0
AVERAGE DAILY TEMPERATURE	38.0 *	41.8	40.5
PRECIPITATION, TOTAL	1.82	1.79	2.19
FEBRUARY (24-26)			
PRECIPITATION, TOTAL	1.82	1.79	2.19

*FEBRUARY 25 TEMPERATURE DATA MISSING AT LOGAN COUNTY.

(1) NOT DETERMINED

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TABLE C-4
CHRONOLOGICAL LISTING OF VISITS TO REFUSE DAM NO. 3
PRIOR TO FAILURE

DAY	DATE	TIME	NAME	REFERENCE*	OBSERVATION LISTED IN TESTIMONY
TUESDAY	2/22/72	EARLY MORNING	DANIEL S. DASOVICH	VOL. III, p.40	DOVE ON IMPOUNDMENT. WATER SEVERAL FEET BELOW 24 INCH PIPE
TUESDAY	2/22/72	MORNING	EARL G. REEDY	VOL. VII, p.165	NONE
WEDNESDAY	2/23/72	MORNING	EARL G. REEDY	VOL. VII, p.165	NONE
WEDNESDAY	2/23/72	MORNING	MARIO VARASSI	VOL. III, p.184	NONE
THURSDAY	2/24/72	MORNING	EARL G. REEDY	VOL. VII, p.169	DAM LOOKED OKAY TO HIM
THURSDAY	2/24/72	MORNING	MARIO VARASSI	VOL. III, p.184	NONE
THURSDAY	2/24/72	AFTERNOON	DANIEL S. DASOVICH	VOL. III, p.41	WATER COMING THROUGH 24 INCH PIPE.
THURSDAY	2/24/72	4:00 P.M.	JACK KENT	VOL. I, p.129	PLACED MEASURING STICK IN DAM NEAR DRAIN PIPE.
THURSDAY	2/24/72	---	BEN TUDOR	VOL. III, p.135	NONE
THURSDAY	2/24/72	PERIODICALLY UNTIL 11:30 P.M.	JACK KENT	VOL. I, p.128	WATER RAISED AN INCH PER HOUR.
FRIDAY	2/25/72	EARLY MORNING	DANIEL S. DASOVICH	VOL. I, p.128	WATER LEVEL A FEW INCHES BELOW TOP OF DRAIN PIPE.
FRIDAY	2/25/72	4:00 P.M.	JACK KENT	VOL. I, p.128	LEVEL HAD RISEN 18 INCHES IN 36 HOURS.
FRIDAY	2/25/72	5:30 P.M.	BEN TUDOR	VOL. III, p.135	INSPECTED WATER LEVEL
FRIDAY	2/25/72	9:00 P.M.	JACK KENT	VOL. I, p.133	WATER LEVEL HAD BEEN CHECKED BY MR. KENT AT REGULAR INTERVALS BETWEEN 4:00 P.M. AND 9:00 P.M.
FRIDAY	2/25/72	9:00 P.M.	ELMER ELSWICK	VOL. I, p.133	NONE
FRIDAY	2/25/72	10:00-11:00 P.M.	EDGAR PIERSON	VOL. II, p.84	SAW CRACK SIX TO EIGHT INCHES WIDE NEAR RIGHT OF DAM, EXTENDING THREE QUARTERS OF WAY ACROSS. WATER WAS TEN TO FIFTEEN INCHES FROM CREST. NO PIPES IN DAM. CREST WAS SOFT. SOME BLACK WATER SEEPING INTO POOL 2 AT TOE OF DAM NO. 3.

* REFERENCES GIVING VOLUME NUMBERS REFER TO THE HEARING TRANSCRIPT OF THE AD HOC COMMISSION REPORT.
REFERENCES GIVING APPENDICES REFER TO THE HEARINGS BEFORE THE SUBCOMMITTEE ON LABOR, U.S. CONGRESS, 1972B.

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TABLE C-4 — CONTINUED
CHRONOLOGICAL LISTING OF VISITS TO REFUSE DAM NO. 3
PRIOR TO FAILURE

DAY	DATE	TIME	NAME	REFERENCE*	OBSERVATION LISTED IN TESTIMONY
FRIDAY	2/25/72	10:00-11:00 P.M.	MR. CHANDLER (ACCOMPANIED EDGAR PIER- SON)	VOL. II, p.85	---
SATURDAY	2/26/72	12:30 A.M.	DENNY GIBSON, JACK KENT, AND HARVEY PIERSON	VOL. I, p.192	ALL THREE VISITED THE DAM SITES, OBSERVED A SLIDE IN THE RIGHT SIDE OF THE VALLEY BETWEEN DAMS 1 AND 2 WHICH WAS DIVERTING WATER INTO POOL 1.
SATURDAY	2/26/72	2:00 A.M.	HARVEY PIERSON	VOL. II, p.71	SAW NO PIPES ON DAM
SATURDAY	2/26/72	3:30 A.M.	JACK KENT	VOL. I, p.134	WATER LEVEL RISE INCREASED TO TWO INCHES AN HOUR.
SATURDAY	2/26/72	4:00 A.M.	KENNETH OSBORNE	VOL. I, p.134	DIDN'T SEE ANY PIPE
SATURDAY	2/26/72	4:30 A.M.	JACK KENT	VOL. I, p.134	WATER LEVEL HAD RISEN THREE INCHES IN AN HOUR.
SATURDAY	2/26/72	4:30 A.M.	DENNY GIBSON	VOL. II, p.71	MESSRS. KENT AND GIBSON REMOVED A TIRE FROM ONE OF THE DRAINPIPES ON DAM NO. 1.
SATURDAY	2/26/72	4:30 A.M.	HARVEY PIERSON	VOL. II, p.71	SURFACE OF DAM NO. 3 WAS SOFT, SAW NO PIPES ON TOP OF DAM. SAW NO WORKMEN AT DAM.
SATURDAY	2/26/72	6:00 A.M.	DENNY GIBSON	VOL. VIII, p.113	SAW PIPES ON DAM
SATURDAY	2/26/72	6:00 A.M.	KENNETH OSBORNE	VOL. II, pp.23, 34, 35, 36 AND 44.	TWO SECTIONS OF 24 INCH CORRUGATED STEEL PIPE LAID END TO END TO FORM 40 TO 60 FOOT SECTION ON CREST OF DAM. PART OF PIPE TOWARDS REAR OF DAM PARTLY BURIED. SMALL FLOW OF WATER OUT OF PIPE, SAW CRACK 10 FEET WIDE, 30 FEET LONG, ON LEFT FRONT OF DAM. WALKED ON DAM, FELT NO MOVEMENT.

* REFERENCES GIVING VOLUME NUMBERS REFER TO THE HEARING TRANSCRIPT OF THE AD HOC COMMISSION REPORT.
REFERENCES GIVING APPENDICES REFER TO THE HEARINGS BEFORE THE SUBCOMMITTEE ON LABOR, U.S. CONGRESS, 1972B.

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TABLE C-4 — CONTINUED
CHRONOLOGICAL LISTING OF VISITS TO REFUSE DAM NO. 3
PRIOR TO FAILURE

DAY	DATE	TIME	NAME	REFERENCE*	OBSESSION LISTED IN TESTIMONY
SATURDAY	2/26/72	6:30 A.M.	DANIEL S. DASOVICH	VOL. III, p.12	WATER COMING THROUGH OVERFLOW PIPE. DAM LOOKED STABLE. COULD HAVE DRIVEN ACROSS DAM. CRACKS IN LEFT FRONT FACE OF DAM. CONTEMPORATED ANOTHER PIPE ON DAM.
SATURDAY	2/26/72	6:30 A.M.	JACK KENT	VOL. III, p. 12	WATER ONE FOOT FROM TOP OF COMPAKTED DAM. 24 INCH PIPE IN DAM NO. 3 ABOUT 4 FEET FROM CREST RUNNING HALF FULL. CREST FIRM. WALKED COMPLETELY ACROSS DAM.
SATURDAY	2/26/72	6:30 A.M.	WALDON MULLINS	VOL. III, p.195	WALKED ON DAM, NOT SOGGY. WATER LEVEL 4 TO 6 FEET BELOW COMPAKTED DAM.
SATURDAY	2/26/72	6:30 A.M.	WALDON MULLINS	APPENDIX A, p.1287	WATER COMING OUT OF DRAIN PIPE.
SATURDAY	2/26/72	6:30 A.M.	MELVIN DUBA	VOL. III, p.201	NONE
SATURDAY	2/26/72	6:45 A.M.	BEN TUDOR	APPENDIX A, p.308	"DAM HOLDING ITS OWN"
SATURDAY	2/26/72	7:00 A.M.	BEN TUDOR	VOL. III, p.152, 153	WATER LEVEL 8 FEET BELOW COMPAKTED DAM. SURFACE FIRM. NO CRACKS.
SATURDAY	2/26/72	7:00-7:30 A.M.	MASON BLANKENSHIP, JR.	VOL.II, p.177	WATER HAD NOT REACHED TOP OF DAM.
SATURDAY	2/26/72	7:15 A.M.	LEONARD LANKAS	VOL. II, p.151	WATER AT CREST ON LOW SIDE. TRASH BAGS CIRCLING LIKE A WHIRLPOOL ON RIGHT HAND SIDE OF POOL BEHIND DAM.
SATURDAY	2/26/72	7:30 A.M.	BEN TUDOR	VOL. III, p.153	NO DIFFERENCE IN LEVEL FROM 7:00 A.M.

* REFERENCES GIVING VOLUME NUMBERS REFER TO THE HEARING TRANSCRIPT OF THE AD HOC COMMISSION REPORT.
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TABLE C-4 — CONTINUED
CHRONOLOGICAL LISTING OF VISITS TO REFUSE DAM NO. 3
PRIOR TO FAILURE

DAY	DATE	TIME	NAME	REFERENCE *	OBSERVATION LISTED IN TESTIMONY
SATURDAY	2/26/72	7:45 A.M.	WAYNE GOODMAN	VOL. III, p.232	SURFACE WET BUT FIRM. WATER 6 TO 8 FEET BELOW. OVERFLOW PIPES FLOWING.
SATURDAY	2/26/72	7:50 A.M.	DENNY GIBSON	VOL. I, p.193	SAW LARGE CRACKS AND SLUMPS ON DOWNSTREAM FACE OF DAM NO. 3 NEAR CENTER. ABOUT 20 FEET SLUMPED INTO POOL 2. TOP OF DAM NO. 3 SOFT AND SOGGY. WATER "OOZ- ING" THROUGH LOOSE RE- FUSE. MR. KENT'S MEAS- URING STICK SUBMERGED.
SATURDAY	2/26/72	8:10 A.M.	WILLIAM PEYTON	VOL. IV, pp.226-231	SAW 75-100 FEET OF RIGHT SIDE OF DAM HAD FAILED. REMAINDER OF DAM SLID- ING INTO BREACH.

* REFERENCES GIVING VOLUME NUMBERS REFER TO THE HEARING TRANSCRIPT OF THE AD HOC COMMISSION REPORT.
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