

## Study and Fabrication of Thermoelectric Air Cooling and Heating System

Prof. N. B. Totala<sup>1</sup>, Prof. V. P. Desai<sup>2</sup>, Rahul K. N. Singh<sup>3</sup>,

Debarshi Gangopadhyay<sup>4</sup>, Mohd. Salman Mohd. Yaqub<sup>5</sup>, Nikhil Sharad Jane<sup>6</sup>

<sup>1,2</sup>(Assistant Professor, Department of Mechanical Engineering, MIT Academy of Engineering, Alandi (D), Pune, Maharashtra, 412105)

<sup>3,4,5,6</sup>(Department of Mechanical Engineering, MIT Academy of Engineering, Alandi(D), Pune, Maharashtra, 412105)

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**Abstract:** In present scenario, HVAC system (commonly used in the air conditioners) is very efficient and reliable but it has some demerits. It has been observed during the last two decades that the O<sub>3</sub> layer is slowly destroyed because of the refrigerant (CFC and HFC) used for the refrigeration and air-conditioning purposes. The common refrigerant used is HFC's which are leaked and slowly ascend into the atmosphere. When they reach to O<sub>3</sub> layer they act on O<sub>3</sub> molecules and the layer of O<sub>3</sub> is destroyed. A single molecule of HFC can destroy thousands of O<sub>3</sub> molecules and that's why it has created a threat for the not only to maintain earth eco system stable but also to existence of earth. Even the percentage of HFCs are emitted into the atmosphere compared to CO<sub>2</sub> is negligible but its global warming effect is few thousand times of CO<sub>2</sub>. The effect of 100 gm of HFC can destroy 0.5 tons of O<sub>3</sub> molecules. These HFCs once destroy O<sub>3</sub> layer; it takes hundreds of years to recover its thickness as it is formed by complex reactions. This is because as HFCs comes in environment, they remain in atmosphere for 18 years. The capacity of HFCs to increase in earth temperature 10% is contributed by HFC's only. That leads to the emergence of finding an alternative of the conventional HVAC system, i.e. thermo-electric cooling and heating system.

**Keywords:** Peltier effect, Thermoelectric module, Cooling load, Thermal resistance, COP.

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### NOMENCLATURE

A - Cross section area (m<sup>2</sup>)  
A<sub>b</sub> - Effective base Area of a heat sink (m<sup>2</sup>)  
A<sub>fin</sub> - Area of a Fin (m<sup>2</sup>)  
C<sub>p</sub> - Specific heat of air (J/kgK)  
D - Diameter of the channel (m)  
f - Darcy friction factor (N/A)  
h - Heat transfer coefficient W/m<sup>2</sup>K  
H - Height of a channel (m)  
I - Operating Current (A)  
L - Length of a fin or channel (m)  
L<sub>c</sub> - Corrected length for a rectangular fin (m)  
m - Mass flow rate of air (kg/s)  
N - Number of channels (N/A)  
P<sub>c</sub> - Pressure drop in the circular duct (N/m<sup>2</sup>)  
P<sub>e</sub> - Electrical input power (W)  
P<sub>r</sub> - Pressure drop in the rectangular channel (N/m<sup>2</sup>)  
P<sub>t</sub> - Total pressure drop (N/m<sup>2</sup>)  
Q - Air flow rate (f<sup>3</sup>/min)  
Q<sub>c</sub> - Heat load absorbed by the cold side of TEC (W)  
Q<sub>h</sub> - Amount of heat dissipated at the hot side of TEC (W)  
R - Thermal resistance (K/W)  
R<sub>b</sub> - Base thermal resistance (K/W)  
R<sub>f</sub> - Fin thermal resistance (K/W)  
R<sub>t</sub> - Total Thermal resistance (K/W)  
r - Radius (m)  
t - Thickness of a fin (m)  
T - Temperature (°C)  
T<sub>c</sub> - Cold side temperature (°C)  
T<sub>h</sub> - Hot side temperature (°C)

$T_{in}$  - Inlet temperature (°C)  
 $T_{out}$  - Outlet temperature (°C)  
 $T_{\infty}$  - Ambient temperature (°C)  
 $\Delta T$  - Temperature difference (K)  
 $v$  - Velocity of the air (m/s)

## I. Introduction

Although thermoelectric (TE) phenomena was discovered more than 150 years ago, thermoelectric devices (TE coolers) have only been applied commercially during recent decades. For some time, commercial TECs have been developing in parallel with two mainstream directions of technical progress – electronics and photonics, particularly optoelectronics and laser techniques. Lately, a dramatic increase in the application of TE solutions in optoelectronic devices has been observed, such as diode lasers, super-luminescent diodes (SLD), various photo-detectors, diode pumped solid state lasers (DPSS), charge-coupled devices (CCDs), focal plane arrays (FPA) and others. The effect of heating or cooling at the junctions of two different conductors exposed to the current was named in honor of the French watchmaker Jean Peltier (1785–1845) who discovered it in 1834. It was found that if a current passes through the contacts of two dissimilar conductors in a circuit, a temperature differential appears between them. This briefly described phenomenon is the basis of thermoelectricity and is applied actively in the so-called thermoelectric cooling modules. Thermoelectric devices (thermoelectric modules) can convert electrical energy into a temperature gradient—this phenomena was discovered by Peltier in 1834. The application of this cooling or heating effect remained minimal until the development of semiconductor materials. With the advent of semiconductor materials came the capability for a wide variety of practical thermoelectric refrigeration applications. Thermoelectric refrigeration is achieved when a direct current is passed through one or more pairs of n and p-type semiconductor materials. In the cooling mode, direct current passes from the n to p-type semiconductor material. The temperature of the interconnecting conductor decreases and heat is absorbed from the environment. This heat absorption from the environment (cooling) occurs when electrons pass from a low energy level in the p-type material through the interconnecting conductor to a higher energy level in the n-type material. The absorbed heat is transferred through the semiconductor materials by electron transport to the other end of the junction TH and liberated as the electrons return to a lower energy level in the p-type material. This phenomenon is called the Peltier effect. 1) "Refrigeration and Air conditioning" book by Mr. Ambatkar S.D.-From this book we got information about the principle of refrigeration and air conditioning. We came to learn the domestic refrigeration system. We came to learn the domestic refrigeration system. We studied calculation related to refrigeration, refrigerants, principle of load estimation etc. 2)"Automotive Air Conditioning" book by Mr. Dwiggins B.H.-From this book we gathered information about the history of domestic and automotive air conditioning system. We studied the principle, construction and working and servicing of today's HVAC system.3)"Heat and Thermodynamic" book by Mr. Subramanyam B.N.-In this book we gathered the information about the basic laws of thermodynamics and the role of thermodynamic in the HVAC system.4)"Refrigeration and Air conditioning" book by Mr. Domkundwar:-This book proved to be really helpful, especially in areas of duct design and heat load calculation.5)"Automotive Technology" book by Mr. Jack Erajavec:-We learned mathematical calculation of refrigeration and thermodynamics. We studied working system of HVAC system and observe temperature and pressure in this system.

Our aim is to introduce the new HVAC system using thermoelectric couple which shall overcome all the disadvantages of existing HVAC system. If this system comes in present HVAC system, then revolution will occur in the automotive sector. With population and pollution increasing at an alarming rate TEC (thermoelectric couple) system have come to rescue as these are environment friendly, compact and affordable. Conventional compressor run cooling devices have many drawbacks pertaining to energy efficiency and the use of CFC refrigerants. Both these factors indirectly point to the impending scenario of global warming. As most of the electricity generation relies on the coal power plants, which add greenhouse gases to the atmosphere is the major cause of global warming. Although researches are going on, better alternatives for the CFC refrigerants is still on the hunt. So instead of using conventional air conditioning systems, other products which can efficiently cool a person are to be devised. By using other efficient cooling mechanisms we can save the electricity bills and also control the greenhouse gases that are currently released into the atmosphere. Although Thermoelectric (TE) property was discovered about two centuries ago thermoelectric devices have only been commercialised during recent years. The applications of TE vary from small refrigerators and electronics package cooling to Avionic instrumentation illumination control and thermal imaging cameras. Lately a dramatic increase in the applications of TE coolers in the industry has been observed. It includes water chillers, cold plates, portable insulin coolers, portable beverage containers and etc.

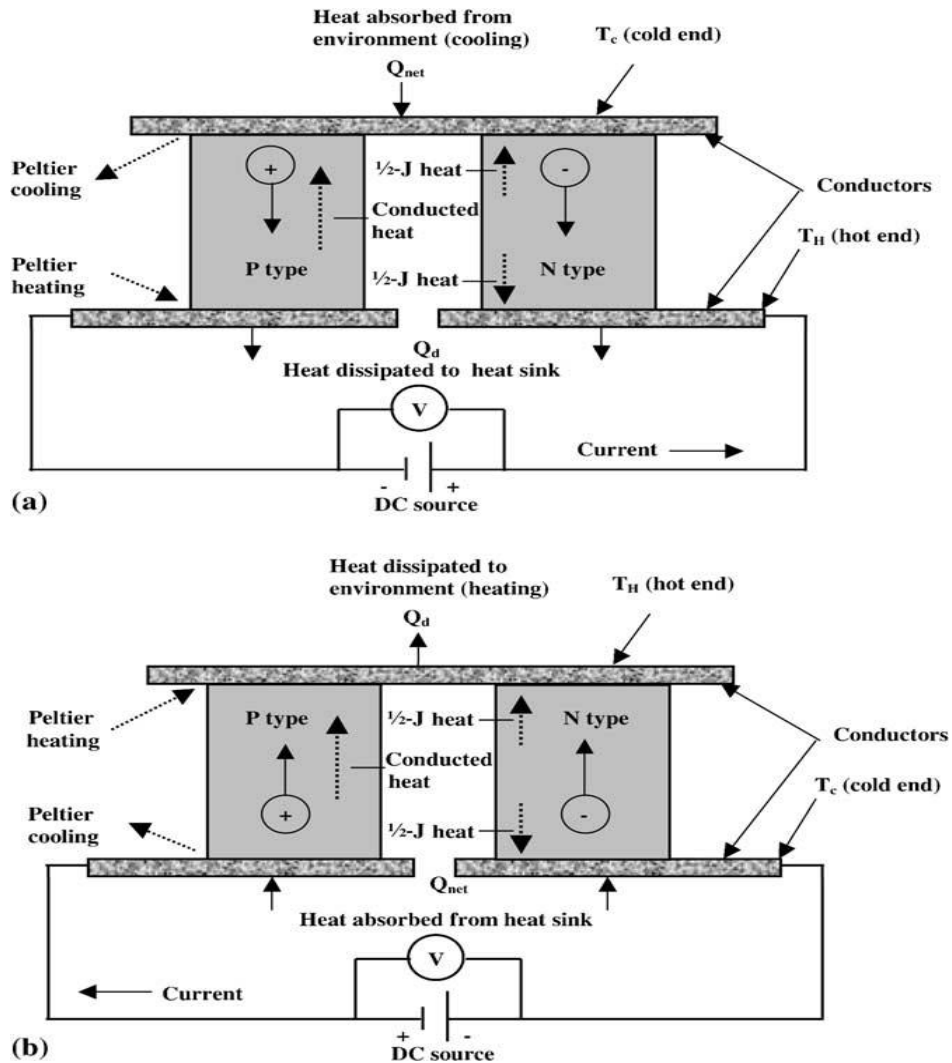


Fig. 1 Schematic of thermoelectric module operation (a) cooling mode (b) heating mode

## II. Methodology and Experimentation

### 2.1 Thermoelectric Module:

A standard module consists of any number of thermocouples connected in series and sandwiched between two ceramic plates (See Figure 3). By applying a current to the module one ceramic plate is heated while the other is cooled. The direction of the current determines which plate is cooled. The number and size of the thermocouples as well as the materials used in the manufacturing determine the cooling capacity. Cooling capacity varies from fractions of Watts up to many hundreds. Different types of TEC modules are single stage, two stage, three stage, four stage, centre hole modules etc.

A typical single stage is shown in Figure 2.



Fig. 2 A typical single stage thermoelectric module.

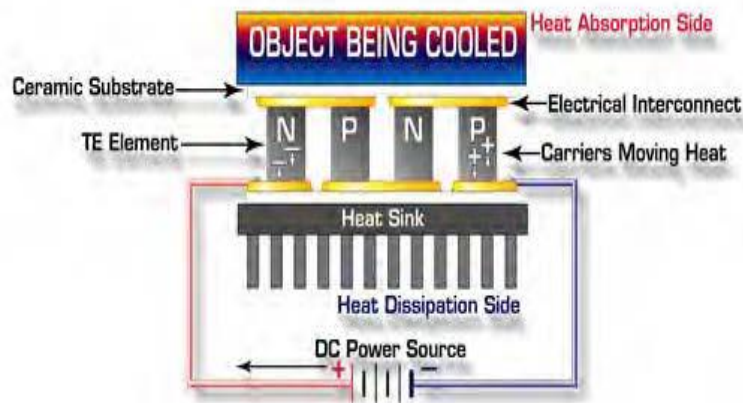


Fig. 3 A Classic TE Module Assembly

Before starting to design a TEC cooling system the designer have to take note the following into consideration.

1. Temperature to be maintained for the object that is to be cooled.
2. Heat to be removed from the cooled object.
3. Time required to attain the cooling after a DC power is applied.
4. Expected ambient temperature.
5. Space available for the module and hot side heat sink.
6. Expected temperature of hot side heat sink.
7. Power available for the TEC.
8. Controlling the temperature of the cooled object if necessary

## 2.2 Parameters of a Thermoelectric Module

Once it is decided that thermoelectric cooler is to be considered for cooling system, the next step is to select the thermoelectric module or cooler that can satisfy a particular set of requirements. Modules are available in great variety of sizes, shapes, operating currents, operating voltages and ranges of heat pumping capacity. The minimum specifications for finding an appropriate TEC by the designer must be based on the following parameters. The cutaway of a TEC is shown in Fig4.

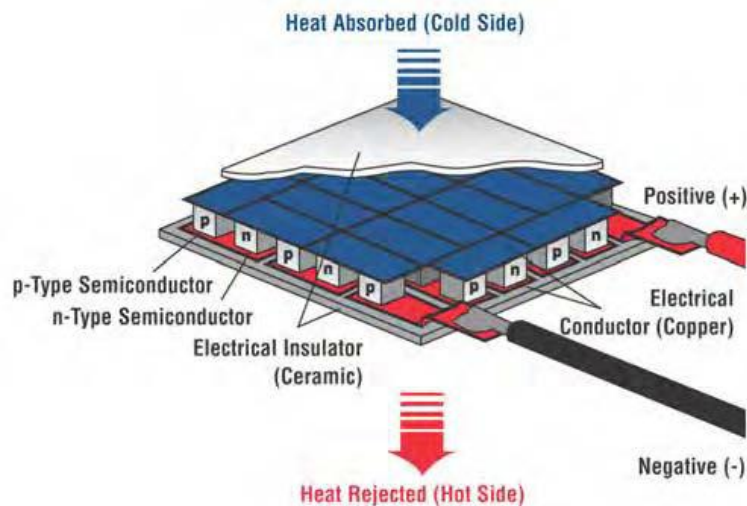


Fig. 4 A Cutaway of Thermoelectric Module

- Cold side temperature ( $T_c$ )
- Hot side temperature ( $T_h$ )
- Operating temperature difference, which is the temperature difference between  $T_h$  and  $T_c$ .
- Amount of heat to be absorbed at the TEC's cold surface. This can also be termed as heat load. It is represented as ( $Q_c$ ) and the unit is Watts.
- Operating current (I) and operating voltage (V) of the TEC.

### Cold side temperature

If the object to be cooled is in direct contact with the cold surface of the TEC, the required temperature can be considered the temperature of the cold side of TEC ( $T_c$ ). Here in this project the object is air inside the car, which has to be cooled when passed through a cluster of four Aluminium heat sinks. It is discussed in detail in the next chapter. The aim is to cool the air flowing through the heat sinks. When this type of system is employed the cold side temperature of the TEC is needed to be several time colder than the ultimate desired temperature of the air.

### Hot side temperature

The hot side temperature ( $T_h$ ) is mainly based on the two factors. First parameter is the temperature of the ambient air in environment to which the heat is been rejected. Second factor is the efficiency of the heat sink that is between the hot side of TEC and the ambient.

### Temperature difference

The two temperatures  $T_c$  and  $T_h$  and the difference between them  $\Delta T$  is a very important factor.  $\Delta T$  has to be accurately determined if the cooling system is expected to be operating as desired. The following equation shows the actual  $\Delta T$ .

$$\Delta T = T_h - T_c$$

Actual  $\Delta T$  is not same as the system  $\Delta T$ . Actual  $\Delta T$  is the difference between the hot and cold side of the TEC. On the other hand system  $\Delta T$  is the temperature difference between the ambient temperature and temperature of the load to be cooled.

### Cooling Load

The most difficult and important factor to be accurately calculated for a TEC is the amount of heat to be removed or absorbed ( $Q_c$ ) by the cold side of the TEC. In this project  $Q_c$  was calculated by finding the product of mass flow rate of air, specific heat of air and temperature difference. Here the temperature difference system  $\Delta T$  in the difference between the inlet temperature and outlet temperature of the cooling system. The mathematical equation for  $Q_c$  is as shown below.

$$Q_c = m C_p \Delta T$$

### Thermoelectric Assembly - Heat Sinks

Thermoelectric Assemblies (TEAs) are cooling or heating systems attached to the hot side of the TEC to transfer heat by air, liquid or conduction. TEAs which dissipate heat from the hot side use heat exchangers. TEC requires heat exchangers or heat sinks and will be damaged if operated without one. The two  $\Delta T$  s, actual  $\Delta T$  and system  $\Delta T$  depend on the heat sinks fitted at the hot sides or cold sides of TEC. The thermal resistances of the heat sinks could vary the  $\Delta T$  across the TEC for a set ambient temperature and cooling load temperature. Therefore the thermal resistance of the heat sinks could increase the current flowing through the TEC. The three basic types of heat sinks are: forced convective, natural convective and liquid cooled, where liquid cooled is the most effective. The typical allowances for  $\Delta T$  at the hot side heat sink of a TEC are

1. 10 to 15 °C for a forced air cooling system with fins - Forced convection
2. 20 to 40 °C for cooling using free convection - Natural convection.
3. 2 to 5 °C for cooling using liquid heat exchangers - Liquid cooled.

There are several different types of heat exchangers available in the market. As far this project is concerned a forced convection type of heat sink was be used based on the  $\Delta T$ .

The main heat sink parameter for the selection process is its thermal resistance. Heat sink resistance can be termed as the measure of the capability of the sink to dissipate the applied heat. The equation is as follows.

$$R = (T_h - T_\infty) / Q_h$$

$R$  is the thermal resistance (in °C /W or K/W) and  $T_h$ , the hot side temperature and  $T_\infty$  ambient temperature respectively.  $Q_h$  is the heat load into the heat sink which is the sum of TEC power  $P_e$  and heat absorbed.

$$Q_h = Q_c + P_e$$

The goal of a heat sink design is to lessen the thermal resistance. It can be attained through exposed surface area of the heat sink. It may also require forced air or liquid cooling.

### Power Supply and Temperature Control

Power supply and temperature control are two added items that must be considered wisely for a successful TE system. TEC is a direct current device. The quality of the DC current is important. Current and voltage of a TEC can be determined by the charts provided by the manufacturer. TEC's power is the product of required voltage and current. ( $P = IV$ ).

Temperature control is generally categorized into two groups. One is open loop or manual and the other is closed loop or automatic. For cooling systems normally cold side is used as basis of control. The controlled temperature is compared to the ambient temperature. An on-off or a control using thermostat is the simplest and easiest techniques to control the temperature of a TEC.

### 2.3 Thermoelectric Air Cooling For 1m<sup>3</sup> Wooden box

The thermoelectric cooling fan design was preformed based on certain mechanical and electrical calculations. The prototype assembly starts with a main fan which is used to blow the ambient air through an aluminum duct. The duct is attached to the blower fan and leads towards a group of four heat sinks. The air which is passed through the duct goes into the cluster of four heat sinks which are united together. These heat sinks acts as a channel for the air to pass through. There are four TECs that are sandwiched between a long black heat sink and the bunch of four heat sinks. TEC cold side or the bottom side rests on the group of four heat sinks. The hot side or the top sides of the TECs are fastened together with the long heat sink. The TECs were installed between the heat sinks using thermal grease, which increases the thermal conductivity by balancing irregular surface of the heat sinks. When the TECs are in operation cold side of the TEC cools down the heat sink channel. Air which is coming out from the channel (i.e. cold side heat sinks H1, H2, H3, H4) is chilled air which is lower than the ambient. The cold side heat sinks rests on a wooden base. There are two fans fitted on top of the hot side heat sink. They blow air towards the hot heat sink to cool it down when the TECs are in operation. The hot air is channeled away from the user using panels. The whole assembly of the cold side heat sinks, hot side heat sink, TECs and the wooden base are fitted tightly with the help of metal clips. These metal clips are tightened together with screws and nuts. The whole assembly is enclosed with sheets or panels.



Fig. 5 Thermoelectric cooling in a 1m<sup>3</sup> wooden box

### 2.4 Computation of cooling power

The amount of heat removed or the cooling power was determined before selection of the TEC.  $Q_c$  which is the amount of heat absorbed was calculated using the equation

$$Q_c = m C_p \Delta T$$

Mass flow rate ( $m$ ) of air is the product of density of air ( $\rho$ ) and volume flow rate ( $Q$ ). Density of air at 30 °C was taken as 1.164 kg / m<sup>3</sup>.  $Q$  was obtained by multiplying velocity of air pass through the rectangular duct of heat sinks and the cross section area of a heat sink. It is denoted by the equation ( $Q = V \times A$ ). Velocity of the air passing through the duct was measured using an anemometer and resulted in a reading of 5m /s. Cross sectional area of the rectangular duct ( $W \times H$ ) was calculated as 0.0054128m<sup>2</sup> and the volume flow rate was 0.02706m<sup>3</sup> / s . Specific heat of air ( $C$ ) at 30 °C was taken as 1007 J / kgK. The system  $\Delta T$  is the difference between the ambient temperature and the temperature of the load to be cooled. It had been targeted to attain a temp of 23°C form the ambient temperature (30 °C). In other words the input temperature from the blower fan is 30 °C and the expected output is 23°C

$$\Delta T = T_{in} - T_{out} = 30^\circ C - 23^\circ C = 7K$$

The amount of heat load for cooling the air through the rectangular duct was calculated as 222W.

### 2.5 TEC Selection

The TEC was selected considering few factors such as dimensions,  $Q_c$ , power supply and etc. The model of TECs used in this project was manufactured in China by Hebei I.T (Shangai) Co. Ltd. The model no. of the module is TEC1-12706. The idea was to select a TEC which has a cooling power greater than the calculated TEC. TEC1-12706 operates with an optimum voltage of 12V. It has maximum voltage of 15.4V. At

12V it draws and maximum DC current of 4 A. The minimum power rating or the cooling power is 37.7 W. The maximum power is 48W. It has a maximum operating temperature of 200°C of the TEC are 68 when hot side temperature is 25 °C. The charts from the TEC manufacture were also analyzed while choosing the TEC. It had been decided to choose 4 TECs of the same model so that when the power of all the 4 TECs is higher than the calculated cooling load. The minimum power rating for 4 TECs added together was more than the cooling load calculated.

$$37.7W \times 4 = 150.8W > 122W$$

The electrical power supplied to the TEC must be higher than the combined power rating of the four TECs and it also depends on the arrangement of the TEC.

## 2.6 TEC Arrangement

The ambient air blown from the blower is channeled into a group of four heat sinks which acts as a rectangular duct as discussed earlier. It was decided to remove maximum amount of heat from the point when the air started to enter the first heat sink. Keeping that in mind the first heat sink was installed with two TECs in series and the second one also was installed with another two TECs in series. This will help to remove more heat from of the air when air enters the duct. The third and fourth heat sinks were installed with one TEC each and they were connected in series also. All the two series connected TECs were connected in parallel.

## 2.7 Selection of Heat sink

There were two different types of heat sink used for this project. One was for the cold side and another for hot side. The initial idea of the project was to use a hollow cylinder as duct to channel air, instead of heat sink on the cold side of the TEC. Initial testing after the proposal stage with hollow cylinder, did not work out well. This was because there of less heat transfer within the cylinder and the air coming out was not cold enough. So the decision was made to use to heat sinks which acts a rectangular duct to channel air. A total of four similar kinds of heat sinks (9Y692 A00-00) were used. Each heat sinks have 20 fins which helped to dissipate coldness fast enough from TECs cold side. In this project heat sinks (hot side and cold side) operate by conducting heat or coldness from the TEC to the heat sink and then radiating to air. A better the transfer of coldness between the two surfaces, the better the cooling will be. When the heat sinks were attached the TECs, there will be uneven surfaces or gaps. The gap will cause for poor heat transfer, even if it is negligible. To improve the thermal connection between the TECs and the heat sinks a chemical compound was used. The heat sink compound, typically a white paste made form zinc oxide in a silicone base ensures a good transfer of heat between the modules and the heat sinks.

### Hot Side heat sink

The hot side heat sink used in the project was a single long one installed on the top side of the TECs. As discussed , thermal resistance of a heat sink is an important factor while designing a system.

$$R_t = (T_h - T_\infty) / Q_h = 0.038K / W$$

Therefore a forced convection heat sink had to be used. When selecting hot side heat sink for the project other factors such as dimension to fit into the whole assembly, budget and availability were also taken to consideration. The heat sink was bought from a local shop and there was no thermal resistance or datasheets available for the product. The alternative was to calculate  $R_t$  from the resistance of the unfinned area ( $R_b$ ) and the resistance offered by the fins ( $R_f$ ). Since both of these resistances are acting in parallel, total resistance was found using the equation

$$1 / R_t = 1 / R_b + 1 / R_f$$

The calculated value was 0.0145K /W. The calculated thermal resistance of the heat sink was lesser than the required. But when considered the dimensions of the cooling system the selected heat sink was very apt.

### Calculations

All calculations used in the project ,related to cooling load , selection of heat sinks, selection of fans, pressure drop calculations, surface area needed to cool the air etc. are mentioned below-

Cooling load-

$Q_c$  the amount heat load to be absorbed by the cold junction has to be calculated before the selection of TECs.

$$Q_c = m C_p \Delta T$$

$$m = p \cdot Q$$

$$p = 1.164 \text{ kg/m}^3 \text{ ( At } 30^\circ\text{C)}$$

$$Q = V \times A$$

$$\begin{aligned}
 A &= W \times H \\
 &= 0.098\text{m} \times 0.064\text{m} \\
 &= 0.006272\text{m}^2 \\
 V &= 2.5\text{m/s} \\
 Q &= 2.5 \times 0.006272 \\
 &= 0.01568\text{m}^3/\text{s} \\
 m &= 1.164 \text{ kg/m}^3 \times 0.01568\text{m}^3/\text{s} \\
 &= 0.018252\text{kg/s} \\
 C_p &= 1007\text{J/KgK} \text{ ( At } 30^\circ\text{C)} \\
 \Delta T &= 32.5 - 22.1 \\
 &= 10.4^\circ\text{C} \\
 Q_c &= 1007 \times 10.4 \times 0.018252 \\
 &= 191.149\text{W} \\
 &\approx 191\text{W} \\
 Q_h &\text{ was calculated by adding the electrical power input and the cooling load.} \\
 P_e &= 18\text{V} \times 13\text{amp} = 234\text{W} \\
 Q_h &= 191\text{W} + 234\text{W} \\
 &= 425\text{W} \\
 \text{COP} &= Q_c/P_e = 0.81624
 \end{aligned}$$

This was not the actual COP of the system. It can be higher, as the power input designed is higher than the calculated  $Q_c$ . A higher power input for TECs were selected in the project. The system was designed with a higher power input. Therefore the actual COP can even higher.

Thermal Resistance of the Hot side Heat Sink

Hot side heat sink has to be selected based on its Thermal resistance. The thermal resistance of the hot side heat sink is calculated below.

$$\begin{aligned}
 Q_h &= (T_h - T_\infty) / R_t \\
 Q_h &= 425\text{W} (Q_c + P_e) \\
 T_\infty &= 32.5^\circ\text{C} \\
 T_h &= 36.2^\circ\text{C} \\
 R_t &= (36.2 - 32.5) / 425 = 0.0087 \text{ K/W}
 \end{aligned}$$

Power of blower fan: The power of the fan will be equal to the product of total pressure drop ( $p_c$ ) and volume flow rate. The total pressure drop will be the sum of pressure drop in cold side heat sink channel (rectangular channel) and the circular duct.

To calculate the pressure drop using Darcy Law, the equation is as follows:

$$\text{The pressure drop} = 0.5 * (fL/D) * \rho * v^2$$

Pressure drop in the circular duct ( $p_c$ ) :-

For the circular duct, Darcy friction factor is value is taken as 0.03 for

$$f = 0.03$$

$$L = 0.22$$

$$D = 15.5$$

$$r = 0.0775$$

$$\rho = 1.164 \text{ kg/m}^3$$

$$Q = V A$$

$$V = Q/A$$

$$Q = 0.01568$$

$$A = \pi * r^2$$

$$= 3.14 * 0.07^2$$

$$= 0.01887 \text{ m}^2$$

$$v = 0.83098 \text{ m/s}$$

$$p_c = 0.5 * fL/D * \rho * v^2$$

$$= 0.5 * ((0.03 * 0.22) / 0.155) * 1.164 * 0.83098^2$$

$$p_c = 0.01711 \text{ N/m}^2$$

Surface area needed to cool the air



The calculations are computed below.

$$Q_c = m C_p \Delta T$$

$$Q_c = hA^* \Delta T$$

$$A = Q_c / (h \Delta T)$$

$$h = 100 \text{ w/m}^2 \text{ k}$$

$$\Delta T = T^* - T_c$$

$$T^* = (T_1 + T_2) / 2$$

$$T^* = (32.5^\circ\text{C} + 21.1^\circ\text{C}) / 2$$

$$T^* = 27.3^\circ\text{C}$$

$$T_c = 15^\circ\text{C}$$

$$\Delta T = 27.3^\circ\text{C} - 15^\circ\text{C}$$

$$\Delta T = 12.3 \text{ K}$$

$$A = 191 / (100 * 12.3)$$

$$A = 0.15528 \text{ m}^2$$

The velocity of hot side, the velocity of cold side, and the applied voltage is varied and different sets of readings are taken. The results of various combinations are plotted.

### III. Results

T<sub>1</sub>-Ambient temperature of air, T<sub>2</sub>-Cold side heat sink temperature.

T<sub>3</sub>-Hot side heat sink temperature, T<sub>4</sub>-Plywood box temperature.

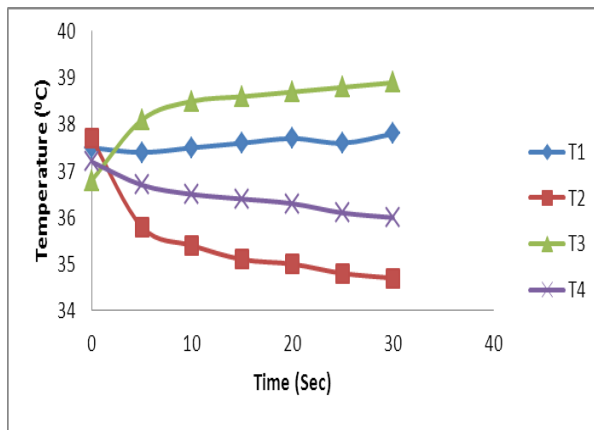


Fig. 6 Variation of temperature with time

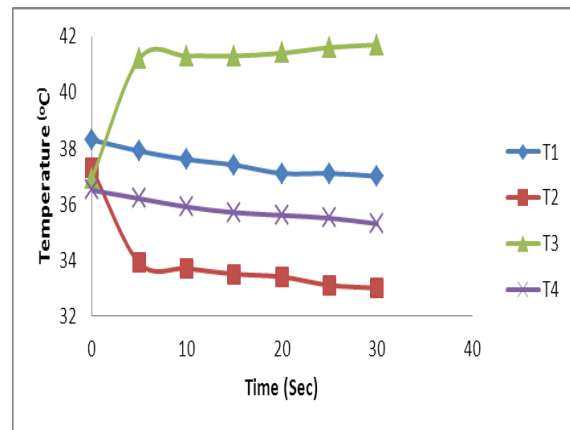


Fig.7 Variation of temperature with time

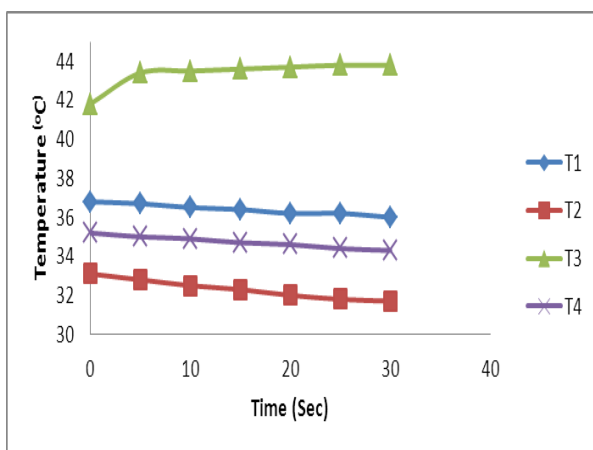


Fig.8 Variation of temperature with time

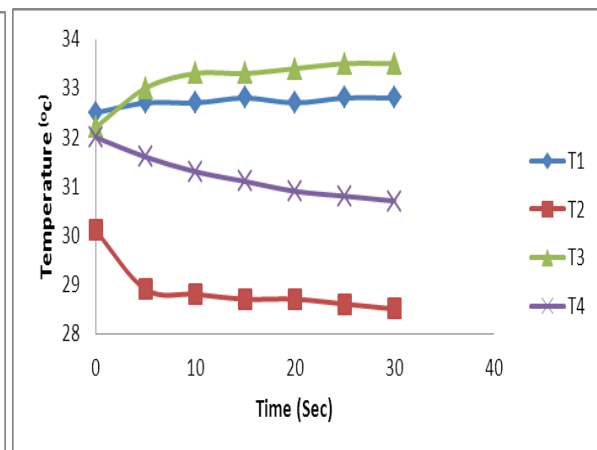


Fig.9 Variation of temperature with time

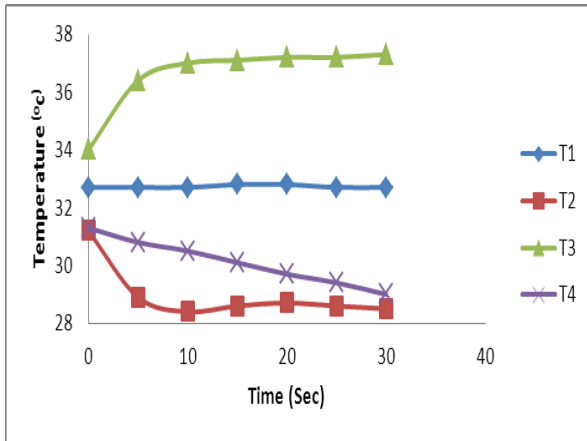


Fig.9 Variation of temperature with time

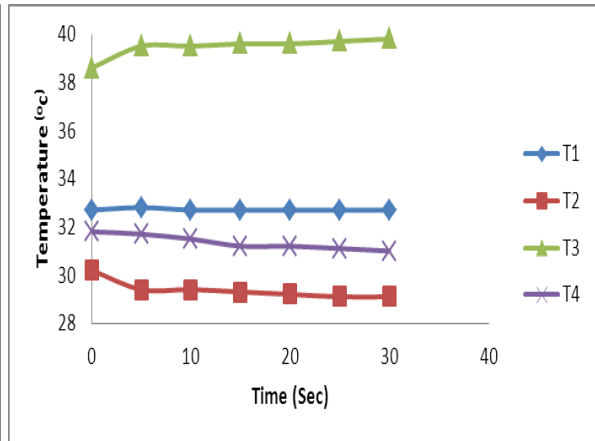


Fig.10 Variation of temperature with time

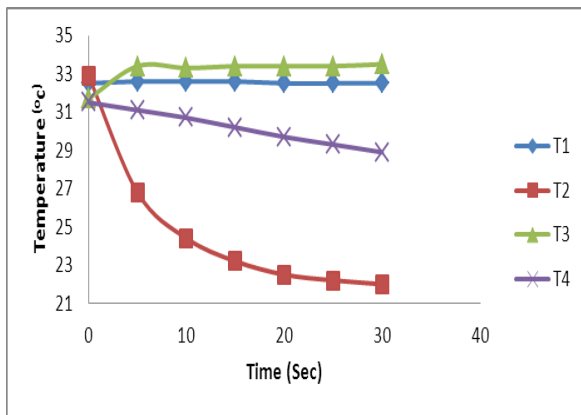


Fig.11 Variation of temperature with time

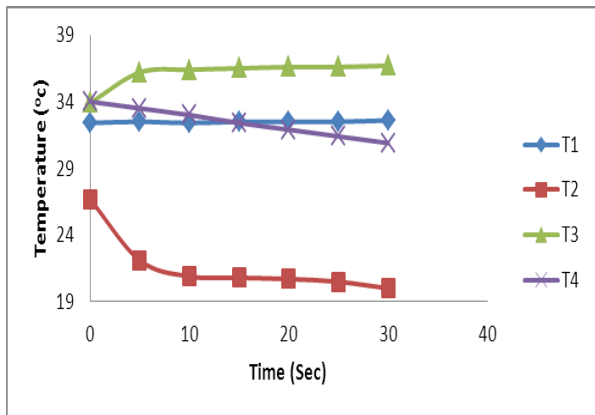


Fig.12 Variation of temperature with time

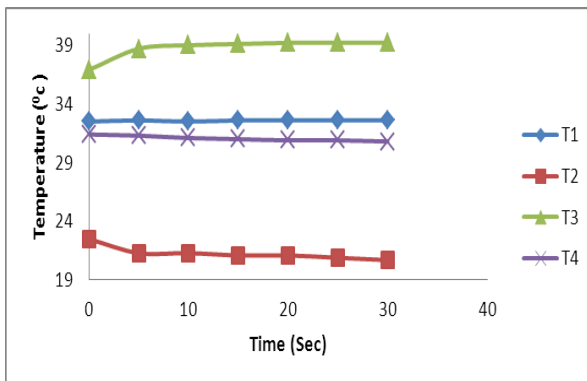


Fig.13 Variation of temperature with time

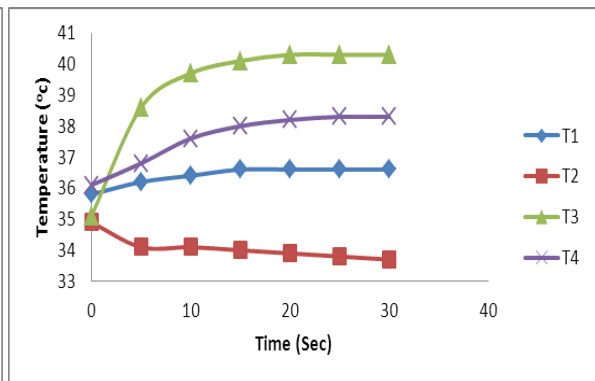


Fig.14 Variation of temperature with time

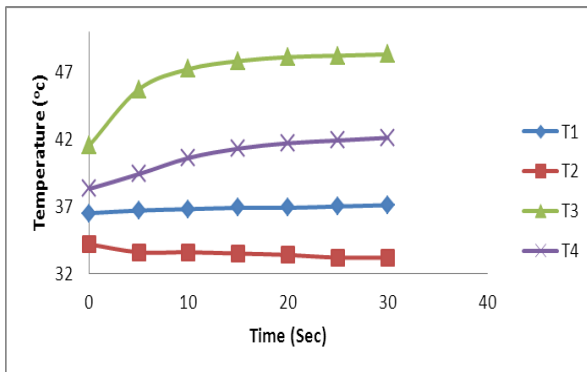


Fig.15 Variation of temperature with time

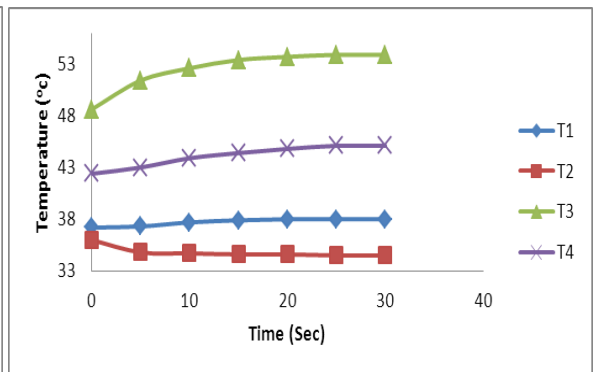


Fig.16 Variation of temperature with time

#### **IV. Conclusion**

A Thermoelectric Air cooling & heating system was designed and built which can be used for personal cooling & heating. Four TECs were used for achieving the cooling with a DC power supply through external power supply (dimmer stat). It had been shown from testing results that the cooling system is capable of cooling & heating the air when re circulating the air with the help of blower. TEC cooling designed was able to cool an ambient air temperature from 32.5°C to 22.1°C. Cooling stabilizes within ten minutes once the blower is turned ON (with a velocity of 2.5 m/s). The system can attain a temperature difference of set target which was 6°C. Accomplishing the set target establish the success of the project. All the components in the project had been tested individually and the results were found to be positive.

The prototype can be made compact by selecting as single TEC of higher power (i.e. of 200W or more). It can be done by choosing a better cold side heat sink that has twisted channels or pipes for circulating the air for a longer time. As an alternative for normal axial fan used in this project, if a blower fans is selected, the cooling system would provide better airflow. Even as shown in the appended figure we can mount no of TEC cooling in Well-known TEC brands (i.e. Melcor, Ferro TEC etc) must be chosen if there is only one high power TEC selected for the cooling system. Bigger hot side heat sink has to be selected accurately based its calculated thermal resistances for best cooling efficiency. With a single TEC, one hot side and a cold side heat sink a smaller personal TEC cooler which gives comfort can be fabricated and can be installed on roof for individual cooling by changing the airflow and some mechanical or electronics section modification, the TEC air cooling for car can be used for heating applications too.

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